# AM-10A 10 KILOWATT <br> AM-6A 6 KILOWATT AM BROADCAST TRANSMITTERS 

## IMPORTANT INFORMATION

## EQUIPMENT LOST OR DAMAGED IN TRANSIT.

When delivering the equipment to you, the truck driver or carrier's agent will present a receipt for your signature. Do not sign it until you have: 1) inspected the containers for visible signs of damage and 2) counted the containers and compared with the amount shown on the shipping papers. If a shortage or evidence of damage is noted, insist that notation to that effect be made on the shipping papers before you sign them.
Further, after receiving the equipment, unpack it and inspect thoroughly for concealed damage. If concealed damage is discovered, immediately notify the carrier, confirming the notification in writing, and secure an inspection report. This item should be unpacked and inspected for damage WITHIN 15 DAYS after receipt. Claims for loss or damage will not be honored without proper notification of inspection by the carrier.

## RF PRODUCT TECHNICAL ASSISTANCE - REPAIR SERVICE - REPLACEMENT PARTS.

Technical assistance is available from Broadcast Electronics by letter, prepaid telephone, fax, or E-mail. Equipment requiring repair or overhaul should be sent by common carrier, prepaid, insured, and well protected. If proper shipping materials are not available, contact the Customer Service Department for a shipping container. Do not the mail equipment. We can assume no liability for inbound damage, and necessary repairs become the obligation of the shipper. Prior arrangement is necessary. Contact the Customer Service Department for a Return Authorization.
Emergency and warranty replacement parts may be ordered from the following address. Be sure to include the equipment model number, serial number, part description, and part number. Non-emergency replacement parts may be ordered directly from the Broadcast Electronics stock room by fax at the number shown below.

## FACILITY CONTACTS -

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Quincy, Illinois 62305
Telephone: (217) 224-9600
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E-Mail: General - bdcast@bdcast.com
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RF PRODUCT TECHNICAL ASSISTANCE - REPAIR - EMERGENCY/WARRANTY REPLACEMENT PARTS -
Telephone: (217) 224-9600
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Fax: (217) 224-9607
NON-EMERGENCY REPLACEMENT PARTS -
Fax: (217) 224-9609

## RETURN, REPAIR, AND EXCHANGES.

Do not return any merchandise without our written approval and Return Authorization. We will provide special shipping instructions and a code number that will assure proper handling and prompt issuance of credit. Please furnish complete details as to circumstances and reasons when requesting return of merchandise. All returned merchandise must be sent freight prepaid and properly insured by the customer.

## WARRANTY ADJUSTMENT.

Broadcast Electronics, Inc. warranty is included in the Terms and Conditions of Sale. In the event of a warranty claim, replacement or repair parts will be supplied F.O.B. factory. At the discretion of Broadcast Electronics, the customer may be required to return the defective part or equipment to Broadcast Electronics, Inc. F.O.B. Quincy, Illinois. Warranty replacements of defective merchandise will be billed to your account. This billing will be cleared by a credit issued upon return of the defective item.

## PROPRIETARY NOTICE.

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## MODIFICATIONS.

Broadcast Electronics, Inc. reserves the right to modify the design and specifications of the equipment in this manual without notice. Any modifications shall not adversely affect performance of the equipment so modified.

ALL PERSONS WHO WORK WITH OR ARE EXPOSED TO POWER TRANSISTORS MUST TAKE PRECAUTIONS TO PROTECT THEMSELVES AGAINST POSSIBLE SERIOUS BODILY INJURY. EXERCISE EXTREME CARE AROUND SUCH PRODUCTS. UNINFORMED OR CARELESS OPERATION OF THESE DEVICES CAN RESULT IN POOR PERFORMANCE, DAMAGE TO THE DEVICE OR PROPERTY, SERIOUS BODILY INJURY, AND POSSIBLY DEATH.

## DANGEROUS HAZARDS EXIST IN THE OPERATION OF POWER TRANSISTORS

The operation of power tubes and power transistors involves one or more of the following hazards, any one of which, in the absence of safe operating practices and precautions, could result in serious harm to personnel.
A. HIGH VOLTAGE - Normal operating voltages can be deadly. Additional information follows.
B. RF RADIATION - Exposure to RF radiation may cause serious bodily injury possibly resulting in blindness or death. Cardiac pacemakers may be affected. Additional information follows.
C. BERYLLIUM - OXIDE POISONING - Dust or fumes from BeO ceramics used as thermal links with power transistors are highly toxic and can cause serious injury or death. Additional information follows.
D. HOT SURFACES - Surfaces of air-cooled heat sinks radiators can reach temperatures of 100 degrees centigrade and cause burns if touched. Additional information follows.
E. RF BURNS - Circuit boards with RF power transistors contain high RF potentials. Do not operate an RF power module with the cover removed.

## HIGH VOLTAGE

The transmitter operates at voltages high enough to kill through electrocution. Personnel should always break the primary circuits when access to the transmitter is required.

## RADIO FREQUENCY RADIATION

Exposure of personnel to RF radiation should be minimized, personnel should not be permitted in the vicinity of open energized RF generating circuits, or RF transmission systems (waveguides, cables, connectors, etc.), or energized antennas. It is generally accepted that exposure to "high levels" of radiation can result in severe bodily injury including blindness. Cardiac pacemakers may be affected.

The effect of prolonged exposure to "low level" RF radiation continues to be a subject of investigation and controversy. It is generally agreed that prolonged exposure of personnel to RF radiation should be limited to an absolute minimum. It is also generally agreed that exposure should be reduced in working areas where personnel heat load is above normal. A $10 \mathrm{~mW} / \mathrm{cm}^{2}$ per one tenth hour average level has been adopted by several U.S. Government agencies including the Occupational Safety and Health Administration (OSHA) as the standard protection guide for employee work environments. An even stricter standard is recommended by the American National Standards Institute which recommends a $1.0 \mathrm{~mW} / \mathrm{cm}^{2}$ per one tenth hour average level exposure between 30 Hz and 300 MHz as the standard employee protection guide (ANSI C95.1-1982).

RF energy must be contained properly by shielding and transmission lines. All input and output RF connections, such as cables, flanges and gaskets must be RF leakproof. Never operate a power tube without a properly matched RF energy absorbing load attached. Never look into or expose any part of the body to an antenna, open RF generating circuit, or RF transmission system while energized. Monitor the tube and RF system for RF radiation leakage at regular intervals and after servicing.

## DANGER - BERYLLIUM OXIDE CERAMICS (BeO) - AVOID BREATHING DUST OR FUMES

BeO ceramic material is used as a thermal link to carry heat from a transistor to the heat sink. Do not perform any operation on any BeO ceramic which might produce dust or fumes, such as grinding, grit blasting, or acid cleaning. Beryllium oxide dust or fumes are highly toxic and breathing them can result in serious personal injury or death. BeO ceramics must be disposed of only in a manner prescribed by the device manufacturer.

## HOT SURFACES

Heat sinks and reject loads are air-cooled or conduction-cooled. The air-cooled external surface can operate at a high temperature (up to $100^{\circ} \mathrm{C}$ ). All hot surfaces may remain hot for an extended time after the transmitter is operated to off. To prevent serious burns, take care to prevent and avoid any bodily contact with these surfaces both during and for a reasonable cooling down period after operation.

## TRANSMITTER WARRANTY VOID NOTICE

THE PRODUCT WARRANTY WILL BE VOID IF THE TRANSMITTER IS INSTALLED AT A SITE WITH INADEQUATE LIGHTNING PROTECTION AND A DEFECTIVE TRANSMISSION LINE SYSTEM.

The transmitter is covered by a two year limited product warranty from Broadcast Electronics. However, the transmitter must be properly installed at a site with adequate lightning protection and transmission line systems. TO ENSURE THE TRANSMITTER WARRANTY IS VALID, the transmitter must be installed: 1) as described by the INSTALLATION procedures presented in SECTION II of this manual, 2) at a transmitter site with a lightning protection system described in TRANSMITTER SITE LIGHTNING PROTECTION SYSTEM CHECKOUT (refer to SECTION II of this manual), and 3) at a transmitter site with a transmission line system described in TRANSMISSION LINE AND ANTENNA CHECKOUT (refer to SECTION II of this manual). FAILURE TO PROPERLY INSTALL THE TRANSMITTER, PROVIDE AN ADEQUATE LIGHTNING PROTECTION SYSTEM, OR PROVIDE AN ADEQUATE TRANSMISSION LINE SYSTEM WILL VOID THE WARRANTY ON THE TRANSMITTER. If any questions develop concerning the transmitter warranty and installation site systems, contact the Broadcast Electronics Customer Service Department.

## NOTICE TO THE EQUIPMENT USER

FCC Rule 73.1590 mandates the licensee of each AM station to make measurements for spurious and harmonic emissions to show compliance with the transmission system requirements of Section 73.44 of the Commission's Rules. It is the broadcast station's responsibility to ensure that the audio signal applied to a Broadcast Electronics A-Series AM transmitter conforms to the audio standard NRSC-1 (published as ANSI/EIA-549-1988). This is a mandatory requirement to ensure that the equipment complies to Section 73.44 and Section 73.128(C) of the Commission's Rules.

4 warning

## OPERATING HAZARDS

## 出 <br> WARNING <br> WARNING

> THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH PO-TENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

The Broadcast Electronics AM transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents.

In addition to high voltages and currents, the AM transmitters contain multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized if required.

## SCOPE OF MANUAL

This manual consists of two sections which provides the following information for the Broadcast Electronics AM-10A and AM-6A AM Broadcast Transmitters.
A. PART I - Contains information relative to installation, operation, and maintenance applicable to the overall transmitter.
B. PART II - Contains detailed information for the following transmitter modular units.

1. POWER SUPPLY ASSEMBLY
2. RF POWER MODULE
3. OUTPUT NETWORK
4. EXCITER/CONTROLLER UNIT (ECU)

## PART I - TABLE OF CONTENTS

## PARAGRAPH

## SECTION I

1-1
1-3
1-4
1-6
1-12
1-13
1-15
1-16
1-17
1-19
1-21

## SECTION II

2-1
2-3
2-6
2-8
2-12
2-13
2-16
2-17
2-19
2-22
2-25
2-26
2-27
2-28
2-29
2-31

## GENERAL INFORMATION

INTRODUCTION ..... 1-1
EQUIPMENT DESCRIPTION ..... 1-1
GENERAL ..... 1-1
EXCITER/CONTROL UNIT ..... 1-1
OUTPUT NETWORK ASSEMBLY ..... 1-4
RF POWER MODULE ..... 1-4
POWER SUPPLY ..... 1-4
COMBINER ASSEMBLY ..... 1-4
TRANSMITTER CONFIGURATIONS ..... 1-5
ACCESSORIES AND SPARE PARTS KITS ..... 1-5
EQUIPMENT SPECIFICATIONS ..... 1-5
INSTALLATION
INTRODUCTION ..... 2-1
UNPACKING ..... 2-1
ENVIRONMENTAL REQUIREMENTS ..... 2-1
COOLING AIR REQUIREMENTS ..... 2-1
PRIMARY POWER ..... 2-1
THREE-PHASE AM-10A/AM-6A ..... 2-1
SINGLE-PHASE AM-10A/AM-6A ..... 2-2
INSTALLATION ..... 2-2
EQUIPMENT PLACEMENT ..... 2-2
COMPONENT INSTALLATION ..... 2-2
ECU CIRCUIT BOARDS ..... 2-8
RF POWER MODULES ..... 2-8
POWER SUPPLY ..... 2-8
BATTERY INSTALLATION ..... 2-11
CIRCUIT BOARD PROGRAMMING ..... 2-11
EXCITER CIRCUIT BOARD ..... 2-11

PAGE NO.

2-40
2-45
2-58
2-61
2-62
2-87
2-89
2-91
2-92
2-93
2-94
2-95
2-96
2-101
2-102
2-104
2-108
2-109
2-110
2-116
2-117
2-119
2-120
2-121
2-122
2-124
2-126
2-132
2-144
2-155
SECTION III OPERATION
3-1
3-3
3-5
3-6
3-14
3-16
3-17
3-18
3-19
3-21
3-23
3-24
3-27
3-29
3-31
3-32

| STEREO CIRCUIT BOARD | $2-13$ |
| :--- | :---: |
| CONTROLLER CIRCUIT BOARD | $2-13$ |
| POWER SUPPLY CIRCUIT BOARD | $2-17$ |
| REMOTE CONTROL | $2-17$ |
| GENERAL | $2-17$ |
| WIRING | $2-20$ |
| AUDIO INPUT CONNECTION | $2-20$ |
| EXTERNAL STEREO RF INPUT | $2-20$ |
| AM-10A RF TRANSMISSION LINE CONNECTION | $2-20$ |
| AM-6A RF TRANSMISSION LINE CONNECTION | $2-21$ |
| EXTERNAL INTERLOCK | $2-23$ |
| MODULATION MONITOR | $2-23$ |
| AC POWER CONNECTIONS | $2-23$ |
| GROUND | $2-24$ |
| TRANSMITTER SITE LIGHTNING PROTECTION | $2-29$ |
| SYSTEM CHECKOUT |  |
| ANTENNA BALL-GAP LIGHTNING ARRESTOR | $2-29$ |
| ANTENNA-TUNING-UNIT SPARK-GAP | $2-29$ |
| LIGHTNING ARRESTOR |  |
| TRANSMITTER SITE GROUNDING SYSTEM | $2-31$ |
| CABLE PROTECTION | $2-31$ |
| ANTENNA RF FEED LINE | $2-31$ |
| TRANSMISSION LINE AND ANTENNA CHECKOUT | $2-31$ |
| ANTENNA VSWR | $2-32$ |
| COAXIAL SWITCH CONTROLLER | $2-32$ |
| ATU AND PHASOR CHECKOUT | $2-32$ |
| INITIAL CHECKOUT | $2-32$ |
| PRELIMINARY OPERATION AND ADJUSTMENT | $2-32$ |
| TUNING | $2-33$ |
| POWER LEVEL AND MODULATION MONITOR | $2-33$ |
| CALIBRATION ADJUSTMENTS | $2-35$ |
| STEREO ADJUSTMENT | $2-37$ |
| SINGLE CHANNEL LEVEL |  |

INTRODUCTION 3-1
CONTROLS AND INDICATORS 3-1
OPERATION 3-13
TURN-ON 3-13
TURN OFF 3-14
METERING 3-14
FORWARD POWER 3-14
REFLECTED POWER 3-14
POWER ADJUST 3-14
MONO/STEREO OPERATION 3-15
STEREO OPERATION 3-15
MONO OPERATION 3-15
PILOT CONTROL 3-15
EXCITER MONITOR OPERATION 3-15
MONO/STEREO INDICATIONS 3-15
INPUT SELECTION 3-15 electronics ing

PARAGRAPH
3-33
3-34
3-35
3-37
3-39
3-41
3-43
3-45
3-47
3-49
3-51
3-53
3-55
3-57
3-59
3-61
3-63

## SECTION IV

4-1
4-5
4-6
4-7
4-8
4-11
4-13
4-18
4-19
4-24
4-27
4-31
4-34
4-39
4-42
4-44
4-46
4-47
4-49
4-51
4-55
4-58
4-60
4-63
4-66
4-74
4-79
4-84
4-89
4-90
4-96
4-100

POLARITY SELECTION
PAGE NO.

X10 AUTORANGE INDICATIONS 3-16
FAULT RESET 3-16
POWER SUPPLY FAULT RESET 3-16
OVER-CYCLE OFF $3-16$
OVER-MODULATION PWM MUTE 3-16
TRANSMITTER MONITOR 3-16
BATTERY TEST $3-16$
CONTROLLER PWM MUTE INDICATOR 3-17
CONTROLLER REMOTE FAIL-SAFE INDICATOR 3-17
EXCITER LOCK INDICATOR 3-17
EXCITER $+5 \mathrm{~V} /+15 \mathrm{~V} /-15 \mathrm{~V}$ INDICATORS $3-17$
STEREO EQUALIZATION INDICATORS 3-17
RF POWER MODULE INDICATORS 3-17
POWER SUPPLY INDICATORS 3-17
EXCITER NEGATIVE LIMITER INDICATOR 3-17
HIGH AC LINE CONDITIONS 3-17

## THEORY OF OPERATION

INTRODUCTION 4-1
FUNCTIONAL DESCRIPTION 4-1
ECU 4-1
GENERAL 4-1
STEREO CIRCUIT BOARD 4-1
EXCITER CIRCUIT BOARD 4-1
CONTROLLER CIRCUIT BOARD 4-2
POWER SUPPLY 4-2
RF POWER MODULE 4-2
RF COMBINER 4-7
OUTPUT NETWORK 4-7
POWER SUPPLY 4-8
POWER SUPPLY CIRCUIT BOARD 4-8
METERING 4-8
COOLING FANS 4-9
INTERFACE CIRCUIT BOARD 4-9
DETAILED DESCRIPTION 4-9
POWER SUPPLIES 4-9
AC INPUT CIRCUITRY 4-9
ECU POWER SUPPLY ASSEMBLY 4-9
TRANSMITTER FLUSHING FANS 4-10
LOW-VOLTAGE POWER SUPPLY TRANSFORMER 4-10
POWER SUPPLY CIRCUIT BOARD 4-10
CONVENTIONAL RECTIFIER CIRCUITRY 4-10
SWITCHING POWER SUPPLY CIRCUIT 4-13
MODULATOR CIRCUIT BOARD 4-14
POWER AMPLIFIER CIRCUIT BOARDS 4-14
SEQUENCE OF OPERATION 4-15
RF CIRCUITRY 4-15
EXCITER CIRCUIT BOARD 4-15
STEREO CIRCUIT BOARD 4-19
RF POWER MODULE 4-20

PARAGRAPH
4-107
4-108
4-109
4-113
4-114
4-115
4-117

## SECTION V

5-1
5-3
5-6
5-8
5-9
5-10
5-11
5-12
5-14
5-15
5-18
5-20
5-22
5-24
5-25
5-26
5-27
5-28
5-34

SECTION VI
6-1

SECTION VII
7-1

TABLE
1-1
1-2

3-1
3-2
3-3
5-1
5-2
6-1

RF COMBINER
PAGE NO.
4-21
HARMONIC BAND-PASS FILTER 4-21
DIRECTIONAL COUPLER CIRCUIT BOARD 4-21
T-MATCHING NETWORK 4-22
LIGHTNING PROTECTION CIRCUIT BOARD 4-22
LIGHTNING DETECTION CIRCUIT BOARD 4-22
RF OUTPUT POWER CONTROL CIRCUITRY 4-22

MAINTENANCE
INTRODUCTION $\quad 5-1$
SAFETY CONSIDERATIONS $5-1$
FIRST LEVEL MAINTENANCE $5-1$
ROUTINE MAINTENANCE $5-1$
INSPECTION AND CLEANING 5-2
CONTROLLER BATTERY 5-2
AIR FILTERS 5-2
FLUSHING FANS 5-2
SPARK GAP 5-2
SECOND LEVEL MAINTENANCE $5-2$
ELECTRICAL ADJUSTMENTS 5-4
TRANSMITTER FREQUENCY RE-PROGRAMMING 5-4
TROUBLESHOOTING $5-4$
TRANSMITTER INDICATORS 5-5
RF POWER MODULE REMOVAL 5-8
TRANSMITTER TROUBLESHOOTING 5-9
PROCEDURES
TRANSMITTER COMPONENT LOCATIONS 5-9
COMPONENT REPLACEMENT PROCEDURE 5-13
INTEGRATED CIRCUITS 5-14

PARTS LIST
INTRODUCTION 6-1

DRAWINGS
INTRODUCTION 7-1

## LIST OF TABLES

DESCRIPTION
ELECTRICAL CHARACTERISTICS
PHYSICAL AND ENVIRONMENTAL
CHARACTERISTICS
AM-10A/AM-6A CONTROLS AND INDICATORS 3-1
ECU CONTROLS AND INDICATORS $3-5$
POWER MODULE CONTROLS AND INDICATORS 3-12
AM-10A INDICATORS 5-5
AM-10A/AM-6A TROUBLESHOOTING $5-9$
AM-10/AM-6A REPLACEABLE PARTS LIST INDEX 6-1

PAGE NO.
1-6
1-9

## LIST OF ILLUSTRATIONS

## FIGURE

1-1
1-2
2-1
2-2
2-3
2-4
2-5
2-6
2-7
2-8
2-9
2-10
2-11
2-12
2-13
2-14
2-15
2-16
2-17

2-18
2-19
3-1
3-2
3-3
4-1
4-2
4-3

4-4

5-1
5-2
5-3
5-4

DESCRIPTION
AM-10A TRANSMITTER 1-2
AM-6A TRANSMITTER 1-3
AM-10A TRANSMITTER INSTALLATION 2-3
AM-6A TRANSMITTER INSTALLATION 2-5
ACCEPTABLE AC POWER INPUT CONFIGURATIONS $2-7$
TRANSMITTER MOVING 2-8
COMPONENT INSTALLATION 2-9
EXCITER CIRCUIT BOARD PROGRAMMING 2-12
STEREO CIRCUIT BOARD PROGRAMMING $2-14$
CONTROLLER CIRCUIT BOARD PROGRAMMING $2-15$
REMOTE CONTROL AND AUDIO CONNECTIONS $2-18$
AM-10A RF OUTPUT CONNECTIONS 2-21
AM-6A RF OUTPUT CONNECTIONS $2-22$
AM-10A THREE-PHASE PRIMARY AC WIRING $2-25$
AM-10A SINGLE-PHASE PRIMARY AC WIRING $2-26$
AM-6A THREE-PHASE PRIMARY AC WIRING $2-27$
AM-6A SINGLE-PHASE PRIMARY AC WIRING $2-28$
ANTENNA LIGHTNING PROTECTION SYSTEM $2-30$
TEST EQUIPMENT CONNECTIONS, POWER LEVEL 2-34
CALIBRATION
TEST EQUIPMENT CONNECTIONS, SEPARATION 2-35
EQUALIZATION LISSAJOUS PATTERNS 2-39
AM-10A CONTROLS AND INDICATORS 3-2
ECU CONTROLS AND INDICATORS 3-7
POWER MODULE CONTROLS AND INDICATORS 3-12
AM-10A BLOCK DIAGRAM 4-3
AM-6A BLOCK DIAGRAM 4-5
AM-10A/AM-6A POWER SUPPLY SIMPLIFIED 4-11
SCHEMATIC
AM-10A/AM-6A RF CIRCUITRY SIMPLIFIED 4-16 SCHEMATIC
REMOVING THE AIR FILTER 5-3
AM-10A COMPONENT LOCATOR 5-15
AM-6A COMPONENT LOCATOR 5-19
ECU/POWER BLOCK COMPONENT LOCATOR 5-23

## PART II - TABLE OF CONTENTS

I - POWER SUPPLY ASSEMBLY
II - RF POWER MODULE
III - OUTPUT NETWORK
IV - EXCITER/CONTROLLER UNIT (ECU)

# SECTION I GENERAL INFORMATION 

## 1-1. INTRODUCTION.

1-2. Information presented by this section provides a general description of the Broadcast Electronics AM-10A and AM-6A transmitters and lists equipment specifications.

## 1-3. EQUIPMENT DESCRIPTION.

## 1-4. GENERAL.

1-5. The Broadcast Electronics AM-10A transmitter is a 10 kW solid-state C-QUAM ${ }^{\text {™ }}$ stereo AM transmitter designed for continuous operation in the 522 kHz to 1705 kHz broadcast band (refer to Figure 1-1). The Broadcast Electronics AM-6A transmitter is a 6 kW solidstate C-QUAM ${ }^{T M}$ stereo AM transmitter designed for continuous operation in the 522 kHz to 1705 kHz broadcast band (refer to Figure 1-2). The AM-10A and AM-6A consist of modular components assembled in a single cabinet. The modular components include: 1) an exciter/control unit, 2) an output network assembly, 3) power block assemblies containing two RF power modules and a star combiner assembly, 4) power supply panel assemblies, and 5) an AC distribution panel assembly. Specific AM-10A and AM-6A features include:

1. Built-in C-QUAM ${ }^{\text {™ }}$ AM stereo circuitry.
2. High efficiency Class E solid-state RF power amplifier modules.
3. A high efficiency switching power supply.
4. Star combiner assembly. Each star combiner allows the removal of RF power modules without the use of dummy modules or bypass switches.
5. A built-in output matching network.
6. A CMOS digital controller with extensive VSWR detection and foldback circuitry which reduces carrier interruptions by weather conditions.

1-6. EXCITER/CONTROL UNIT. The transmitter exciter/control unit (ECU) is a modular assembly containing plug-in stereo, exciter, and controller circuit boards. In addition to the circuit boards, the ECU is equipped with forward and reflected power meters to provide transmitter output power status indications.

1-7. Stereo Circuit Board. The ECU stereo circuit board is a modular plug-in assembly containing C-QUAM ${ }^{\text {™ }}$ AM stereo circuitry. The C-QUAM ${ }^{\text {™ }}$ stereo system is a mode of $A M$ stereo transmission utilizing amplitude modulated monaural $(\mathrm{L}+\mathrm{R})$ information and independently quadrature modulated stereo ( $\mathrm{L}-\mathrm{R}$ ) information. The results produce a stereo transmission system compatible with mono receivers.

1-8. The stereo circuit board is designed with remote/local controlled mono left, mono right, mono $\mathrm{L}+\mathrm{R}$, and stereo modes of operation. Two equalization circuits are provided to allow the transmitter to be configured for operation into two different antennas.

C-QUAM ${ }^{\text {TM }}$ is a registered trademark of Motorola Inc.


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597-1113-1
FIGURE 1-1. AM-10A TRANSMITTER


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FIGURE 1-2. AM-6A TRANSMITTER

1-9. Exciter Circuit Board. The ECU exciter circuit board is a modular plug-in exciter assembly. Instrumentation amplifiers provide balanced left and right channel transformerless audio inputs. The exciter carrier frequency is established by a digital frequency synthesizer. The synthesizer is a phase-locked-loop circuit which provides extremely accurate and reliable carrier frequency operation. A PWM (pulse-width-modulation) circuit is used to generate an RF drive signal for application to a modulator circuit board in an RF power module. If a stereo circuit board failure is encountered or when the stereo circuit board is removed from the ECU chassis, the exciter circuitry is designed to automatically configure to monophonic operation.

1-10. Controller Circuit Board. All transmitter control operations are directed by the ECU controller circuit board. The controller circuit board consists of CMOS logic control and monitoring circuitry. The circuitry is designed to interface to all popular remote control systems such as the Broadcast Electronics VMC-16 remote control system.

1-11. The transmitter power is controlled by a power control circuit. The circuit allows the transmitter to be operated at five power levels. A power trim circuit allows the transmitter output power to be adjusted to a precise level. An antenna interlock circuit is provided to prevent the transmitter from operating into an incorrect antenna. A reflected power detection circuit operates in association with the power control circuit to foldback the transmitter power during high VSWR conditions. In addition to the reflected power detector, a lightning detector circuit is provided to mute the transmitter when high voltage is present at the transmitter output during a lightning storm.

1-12. OUTPUT NETWORK ASSEMBLY. Matching of the transmitter impedance to the antenna is accomplished by the output network assembly. The assembly is equipped with an LC T network to match the transmitter output to the antenna. A bandpass filter is provided to attenuate all harmonic frequencies to FCC, DOC, and CCIR levels. The assembly also contains the lightning detection circuit board, a lightning protection circuit board, and a directional coupler assembly.

1-13. RF POWER MODULE. The AM-10A and AM-6A transmitters are equipped with RF power modules. A power module is a modular plug-in assembly containing two RF power amplifier circuit boards and one modulator circuit board. Each power module is equipped with MOSFET transistors to produce 1100 watts of RF power.

1-14. The RF power modules are designed using Class E amplifier technology. A Class E amplifier exhibits high efficiency and provides superior audio performance. In addition to the superior efficiency and audio performance, the power modules are designed to be removed from the chassis for maintenance. The remaining power modules will provide full power to maintain on-air operation.

1-15. POWER SUPPLY. A modular switching power supply provides operating potentials for two RF power modules. The power supply design uses an SCR controlled bridge to rectify the ac line voltage into a dc potential. The supply is filtered and routed to the RF power modules for control and regulation. A fault detection circuit monitors power supply activity for failure conditions. A separate modular switching power supply provides operating potentials for the ECU circuitry.

1-16. COMBINER ASSEMBLY. The AM-10A and AM-6A are equipped with a star combining system. The system combines the outputs of the RF power modules to provide: 1) a 10 kW output in AM-10A models and 2) a 6 kW output in AM-6A models. If a power module is removed from the chassis, the remaining power modules will continue operation to maintain on-air operation.

## 1-17. TRANSMITTER CONFIGURATIONS.

1-18. The AM-10A and AM-6A transmitters can be ordered in the following configurations:
$\mathbf{P} / \mathbf{N}$
907-1010-001

907-1010-041

907-1010-011

907-6000

907-6000-030

907-6000-040

DESCRIPTION
AM-10A 10 kW AM Transmitter for operation in the 522 kHz to 1705 kHz broadcast band, 10 kHz spacing, $196 \mathrm{~V}-256 \mathrm{~V}$ ac three phase supply.

AM-10A 339 V to 437 V ac three phase supply option.

AM-10A 10 kW AM Transmitter for operation in the 522 kHz to 1705 kHz broadcast band, 10 kHz spacing, $196 \mathrm{~V}-256 \mathrm{~V}$ ac single phase supply.

AM-6A 6 kW AM Transmitter for operation in the 522 kHz to 1705 kHz broadcast band, 10 kHz spacing, $196 \mathrm{~V}-256 \mathrm{~V}$ ac single phase supply.

AM-6A 10 kW AM Transmitter for operation in the 522 kHz to 1705 kHz broadcast band, 10 kHz spacing, $196 \mathrm{~V}-256 \mathrm{~V}$ ac three phase supply.

AM-6A 339 V to 437 V ac three phase supply option.

## 1-19. ACCESSORIES AND SPARE PARTS KITS.

1-20. The following text presents accessories and spare parts kits available for use with the AM-10A and AM-6A transmitters.

## $\mathbf{P} / \mathbf{N}$

977-0030
977-0031
977-0032

977-0033
977-0034
977-0035

907-0016-110

977-0037

## DESCRIPTION

AM-10A recommended semi-conductor kit.
AM-10A 100\% semi-conductor kit.
AM-10A recommended spare parts kit. Includes selected meters, switches, fuses, filters, etc. Does not include semi-conductors.

AM-6A recommended semi-conductor kit.
AM-6A 100\% semi-conductor kit.
AM-6A recommended spare parts kit. Includes selected meters, switches, fuses, filters, etc. Does not include semi-conductors.

VMC-16 Voice Remote Control Unit, AM-10A/ AM-6A

Basic semi-conductor kit, AM-10A/AM-6A/ AM-1A.

## 1-21. EQUIPMENT SPECIFICATIONS.

1-22. Refer to Table 1-1 for electrical specifications or Table 1-2 for physical specifications of the $\mathrm{AM}-10 \mathrm{~A}$ and AM-6A transmitters.

TABLE 1-1. ELECTRICAL CHARACTERISTICS
(Sheet 1 of 4)

| PARAMETER | SPECIFICATION |
| :---: | :---: |
| RF POWER OUTPUT |  |
| AM-10A | 50 W to 10.8 kW . Five preset power levels available by local or remote control. Will operate at a reduced power output (20-35\% typical) with one-half of the power modules. |
| AM-6A | 25 W to 6.6 kW . Five preset power levels available by local or remote control. Will operate at a reduced power output ( $20-35 \%$ typical) with one-half of the power modules. |
| OUTPUT POWER REGULATION | Less than $1 \%$ change in output power with variation of ac line input voltage from 196 V to 252 V ac. |
| RF CARRIER FREQUENCY RANGE | 522 kHz to 1705 kHz (as ordered). Accommodates 9 kHz or 10 kHz channel spacing ( 9 kHz spacing requires an optional crystal). |
| RF OUTPUT IMPEDANCE |  |
| AM-10A | optimize VSWR of $1.4: 1$ at any phase angle and carrier frequency. <br> 50 Ohms, unbalanced. Matching network to optimize VSWR of $1.5: 1$ at any phase angle and carrier frequency. |
| $\begin{aligned} & \text { OUTPUT CONNECTOR } \\ & \text { AM-10A } \\ & \text { AM-6A } \end{aligned}$ | $15 / 8$ inch EIA flange. <br> Clamp and lug type. Accommodates $7 / 8$ inch (2.2 $\mathrm{cm})$ transmission line. |
| LOAD VSWR |  |
| AM-10A AM-6A | 1.4:1 at full carrier power. Will operate into a higher VSWR with automatic power reduction. Open and short circuit protected. <br> 1.5:1 at full carrier power. Will operate into a higher VSWR with automatic power reduction. Open and short circuit protected. |
| HARMONIC AND SPURIOUS SUPPRESSION | Meets or exceeds FCC, DOC, and CCIR requirements when preceded by external NRSC-1 compatible audio low-pass filters. |
| CARRIER FREQUENCY STABILITY | $\pm 3 \mathrm{ppm}, 0^{\circ}$ to $50^{\circ} \mathrm{C}\left(+32^{\circ}\right.$ to $\left.+122^{\circ} \mathrm{F}\right)$. |
| CARRIER SHIFT | Less than $1 \%$ at $95 \%$ negative modulation at 1 kHz . |

# TABLE 1-1. ELECTRICAL CHARACTERISTICS 

## (Sheet 2 of 4)

| PARAMETER | SPECIFICATION |
| :---: | :---: |
| TYPE OF MODULATION | Pulse Width Modulation of $L+R$ envelope with integrated C-QUAM AM stereo. An RF input connector is also provided for an external stereo exciter. |
| OPERATING MODES | Stereo, mono L+R, mono L, mono R, by local or remote control. |
| MODULATION CAPABILITY |  |
| AM-10A | Greater than $145 \%$ peak positive capability at 10.8 kW . $130 \%$ into 1.4:1 VSWR. |
| AM-6A | Greater than $145 \%$ peak positive capability at 6.6 kW . $130 \%$ into 1.5:1 VSWR. |
| MODULATION INPUT INDICATION | Peak reading, color coded, LED bar graph display with an autorange feature for monitoring positive or negative input levels of four different audio channels ( $\mathrm{L} / \mathrm{R}$ or $\mathrm{L}+\mathrm{R} / \mathrm{L}-\mathrm{R}$ ). |
| AUDIO INPUT LEVEL | $+10 \mathrm{dBm}, \pm 1 \mathrm{~dB}, \mathrm{~L}=\mathrm{R}$ (or mono) to produce $100 \%$ $\mathrm{L}+\mathrm{R}$ envelope modulation. Other input levels can be accommodated. |
| AUDIO INPUT IMPEDANCE | 600 Ohms. Inputs are balanced, transformerless, and resistive with passive RFI filtering. Other impedances can be accommodated. |
| AUDIO FREQUENCY RESPONSE (MONOPHONIC) | $\pm 0.5 \mathrm{~dB}, 20 \mathrm{~Hz}$ to 10 kHz at $90 \%$ negative modulation (linear phase mode). +0.1 dB $-3 \mathrm{~dB}, 20 \mathrm{~Hz}$ to 10 kHz at $90 \%$ negative modulation, standard configuration. |
| AUDIO HARMONIC DISTORTION |  |
| Mono | Less than $0.8 \%, 20 \mathrm{~Hz}$ to 10 kHz at rated power. Less than $1.5 \%, 20 \mathrm{~Hz}$ to 10 kHz at 5000 W . Less than $2.0 \%, 20 \mathrm{~Hz}$ to 10 kHz at 2500 W . Less than $3.0 \%, 20 \mathrm{~Hz}$ to 10 kHz at 1000 W . All mono audio harmonic distortion specifications are referenced to an audio input level which generates $90 \%$ modulation at $1 \mathrm{kHz}(9 \mathrm{dBm})$. |
| Stereo | Less than $1.5 \%$ at $50 \%$ single channel modulation, 50 Hz to 10 kHz at rated power. |
| INTERMODULATION DISTORTION (MONO) | $1.2 \%$ or less at $1: 1$ ratio. $1.7 \%$ or less at $4: 1$ ratio. $60 / 7000 \mathrm{~Hz}$ SMPTE standards with $85 \%$ modulation at rated power. |

TABLE 1-1. ELECTRICAL CHARACTERISTICS
(Sheet 3 of 4)

| PARAMETER | SPECIFICATION |
| :---: | :---: |
| CCIF INTERMODULATION DISTORTION (MONO) | $1.0 \%$ or less at $1: 1$ ratio. $4 \mathrm{kHz} / 5 \mathrm{kHz}$ with $85 \%$ modulation at rated power. <br> $1.0 \%$ or less at $4: 1$ ratio. 2.96 kHz square wave 8 kHz sinewave with $85 \%$ modulation at rated power. <br> Less than 2.0 degrees ( 0.035 radians) average or 30 dB ( 40 dB typical) below equivalent $100 \% \mathrm{~L}-\mathrm{R}$ $\mathrm{C}-\mathrm{QUAM}$ modulation, 50 Hz to 10 kHz at rated power. Measured with an audio input level which generates $95 \%$ negative $L+R$ envelope modulation at $1 \mathrm{kHz}(9.5 \mathrm{dBm})$. <br> -30 dB or greater, 50 Hz to 10 kHz . Measured with $50 \%$ single channel modulation into a 50 ohm resistive load at rated power. <br> $0.1 \%$ or less at $400 \mathrm{~Hz}, 90 \%$ modulation with high frequency boost disabled. <br> $1.0 \%$ or less at $400 \mathrm{~Hz}, 50 \%$ single channel modulation with high frequency boost disabled. <br> $1.0 \%$ or less at $40 \mathrm{~Hz} .1 .5 \%$ or less at 20 Hz . Measured with $90 \%$ negative modulation. <br> Greater than 65 dB below a reference level equivalent to $100 \%$ negative modulation in a 22 Hz to 30 kHz bandwidth, unweighted. <br> Greater than 55 dB below a reference level equivalent to $100 \%$ negative modulation of either left or right channel in a 22 Hz to 30 kHz bandwidth, unweighted. <br> 196V to 252 V Delta/Wye or 339 V to 437 V Wye, $50 / 60 \mathrm{~Hz}$, three-phase. Includes built-in MOVs for surge suppression. <br> 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$, single phase. Includes built-in MOVs for surge suppression. <br> 13.3 kW , no modulation of 10 kW carrier. $20 \mathrm{~kW}, 100 \%$ modulation of 10 kW carrier. Measured at 10 kW into a 50 ohm resistive load at 220 V ac. <br> 8 kW , no modulation of 6 kW carrier. $12 \mathrm{~kW}, 100 \%$ modulation of 6 kW carrier. Measured at 6 kW into a 50 ohm resistive load at 220 V ac. |
| TRANSIENT INTERMODULATION DISTORTION (MONO) |  |
| INCIDENTAL PHASE MODULATION (STEREOPHONIC) |  |
| STEREO SEPARATION |  |
| SQUAREWAVE OVERSHOOT Mono |  |
| Stereo |  |
| SQUAREWAVE TILT |  |
| NOISE |  |
| Mono |  |
| Stereo |  |
| AC INPUT VOLTAGE <br> Three-Phase Models Single-Phase Models |  |
| AC POWER CONSUMPTION AM-10A $\mathrm{AM}-6 \mathrm{~A}$ |  |

TABLE 1-1. ELECTRICAL CHARACTERISTICS
(Sheet 4 of 4)

| PARAMETER | SPECIFICATION |
| :---: | :---: |
| OVERALL EFFICIENCY |  |
| AM-10A | $75 \%$ or greater, $100 \%$ sinusoidal modulation of carrier, ac line to RF output. Measured at 10 kW into a 50 ohm resistive load at 220 V ac. |
| AM-6A | $75 \%$ or greater, $100 \%$ sinusoidal modulation of carrier, ac line to RF output. Measured at 6 kW into a 50 ohm resistive load at 220 V ac. |
| SAFETY | Meets IEC 215 specifications. |
| METERING |  |
| AM-10A | Output Forward Power. High scale -0 kW to 12 kW . Low scale - 0 W to 3 kW . |
|  | Output reflected power. High scale - 0 to 1200 watts. Low scale -0 to 300 watts. Ac line voltage. Scale - 150 to 300 volts. AM-10A Forward Power Meter complies with FCC rule 73.1215(A) within the 600 watt to 10.8 kW range. |
| AM-6A | Output Forward Power. High scale -0 kW to 7 kW . Low scale - 0 W to 1750 watts. Output reflected power. High scale -0 to 600 watts. Low scale -0 to 150 watts. Ac line voltage. Scale - 150 to 300 volts. AM-6A Forward Power Meter complies with FCC rule 73.1215(A) within the 360 watt to 6.6 kW range. |
| RF MONITORING PROVISIONS | 2 volts RMS nominal RF output sample into a 50 Ohm input. Adjustable from the transmitter front panel for each of the five power levels. |
| REMOTE INTERFACE | Built-in interface for most control and monitoring systems. |

TABLE 1-2. PHYSICAL AND ENVIRONMENTAL CHARACTERISTICS
(Sheet 1 of 2)

| PARAMETER | SPECIFICATION |
| :--- | :--- |
| PHYSICAL |  |
| DIMENSIONS | Width: 27.3 Inches $(69.3 \mathrm{~cm})$. |
|  | Height: 73.5 Inches $(186.7 \mathrm{~cm})$ |
| WEIGHT | Depth: 37.0 Inches 94.0 cm$)$ |
| AM-10A | 635 Pounds $(288 \mathrm{~kg})$, unpacked. |
| AM-6A | 442 Pounds $(200 \mathrm{~kg})$, unpacked. |
| CUBAGE | $42.5 \mathrm{Ft}^{3}\left(1.2 \mathrm{~m}^{3}\right)$. |

TABLE 1-2. PHYSICAL AND ENVIRONMENTAL CHARACTERISTICS (Sheet 2 of 2)

| PARAMETER | SPECIFICATION |
| :--- | :--- |
| ENVIRONMENTAL |  |
| COOLING | Low velocity air with disposable filters. |
| Type | 1200 Cubic Feet Per Minute ( $34.0 \mathrm{~m}^{3} / \mathrm{min}$ ). |
| Requirements | 720 Cubic Feet Per Minute $\left(20.4 \mathrm{~m}^{3} / \mathrm{min}\right)$ |
| AM-10A | $0^{\circ}$ to $50^{\circ} \mathrm{C}$ ( $+32^{\circ}$ to $+122^{\circ} \mathrm{F}$ ) |
| AM-6A | 0 TO $95 \%$ ( non-condensing) |
| OPERATING TEMPERATURE | 0 to 10,000 feet above sea level ( 0 to 3048 Meters). |
| OPERATING HUMIDITY | 0 to 7,500 feet above sea level ( 0 to 2286 Meters). |
| MAXIMUM ALTITUDE |  |
| 60 Hz Models |  |
| 50 Hz Models |  |
| NOTE - For AM-10A, All specifications measured at 10 kW into a 50 ohm resistive load using |  |
| Broadcast Electronics AS-10 modulation monitor. |  |
| For AM-6A, All specifications measured at 6 kW into a 50 ohm resistive load using |  |
| Broadcast Electronics AS-10 modulation monitor. |  |

# SECTION II INSTALLATION 

## 2-1. INTRODUCTION.

2-2. This section contains information required for the installation and preliminary checkout of the Broadcast Electronics AM-10A and AM-6A transmitters.

## 2-3. UNPACKING.

$2-4$. The equipment becomes the property of the customer when the equipment is delivered to the carrier. Carefully unpack the transmitter. Perform a visual inspection to determine that no apparent damage has been incurred during shipment. All shipping materials should be retained until it is determined that the unit has not been damaged. Claims for damaged equipment must be promptly filed with the carrier or the carrier may not accept the claim.
$2-5$. The contents of the shipment should be as indicated on the packing list. If the contents are incomplete, or if the unit is damaged electrically or mechanically, notify both the carrier and Broadcast Electronics.

2-6. ENVIRONMENTAL REQUIREMENTS.
2-7. Table 1-2 provides environmental conditions which must be considered prior to transmitter installation. Refer to Table 1-2 in SECTION I, INTRODUCTION and ensure the transmitter is to be installed in an acceptable environment.
$2-8$. COOLING AIR REQUIREMENTS.
$2-9$. If outside air is to be used to cool the transmitter, the air inlet duct must be sized to allow adequate air flow. The air must be dry and well filtered. If intake louvers are used, operation of the louvers must be electrically interlocked with the transmitter operation.
$2-10$. If the heated transmitter air is to be ducted from the room, the duct system must not introduce any back-pressure on the equipment. Proper allowances for air flow will ensure that only a limited amount of heat is dissipated into the equipment interior. The duct system must allow for a minimum air flow of: 1) 1200 cubic feet of air per minute for AM-10A models and 2) 720 cubic feet of air per minute for AM-6A models.

2-11. As a minimum requirement, any duct work must have a cross-sectional area equal to the exhaust area of the cabinet (refer to Figure 2-1 and 2-2). Sharp bends in the duct system will introduce back pressure and are not permissible. A radius bend must be used if a right angle turn is required. An exhaust fan may be used to overcome duct losses or overcome wind pressures if the duct is vented to the outside.

2-12. PRIMARY POWER.
2-13. THREE-PHASE AM-10A/AM-6A. The three-phase AM-10A and AM-6A transmitters are designed for operation from a closed-delta or wye connected three-phase power source. Operation from an unsatisfactory power source will void the warranty on the transmitter as any resultant damage is beyond the control of the manufacturer. Before attempting installation of the transmitter, assure that the proper power source is installed. Acceptable power input configurations are shown in Figure 2-3.

2-14. An open-delta, V to V, T to T, T to L, or Scott connected power source will provide unsatisfactory transmitter performance as transients and unstable power can damage components of the transmitter and provide degraded specifications. Any of these systems will develop a considerable imbalance between phases in voltage, phase angle, or both voltage and phase angle. These problems can result in premature failure of power supply and RF circuit components.
2-15. It is important that the local electric utility be consulted to ensure that the correct service is provided before connection of the transmitter to a primary power source. The proper power source can be readily identified by the use of three transformers with one winding each or one transformer with three windings instead of the use of two transformers as required for the unacceptable configurations.
2-16. SINGLE-PHASE AM-10A/AM-6A. The single phase AM-10A and AM-6A transmitters are designed for operation from a 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ single phase power source. Consult the local electric utility company to ensure that the correct service is provided before connection of the transmitter to the primary power source.
2-17. INSTALLATION.
2-18. Each transmitter is wired, operated, tested, and inspected at the factory prior to shipment and is ready for installation when received. Prior to installation, this publication should be studied to obtain an understanding of the operation, circuitry, nomenclature, and installation requirements. Installation is accomplished as follows: 1) placement, 2) component installation, 3) circuit board programming, 4) remote control connections, 5) wiring, 6) initial checkout, and 7) preliminary operation and tuning.
2-19. EQUIPMENT PLACEMENT.
$2-20$. The transmitter is designed with access holes in the top of the cabinet to allow for the over-head ducting of ac power, RF transmission line, and ground strap wiring (refer to Figure $2-1 / 2-2$ ). The floor must be capable of supporting the total transmitter weight of approximately 90 pounds per square foot. The floor support should be more than marginal to maintain proper cabinet alignment and reduce vibration.
2-21. Evaluate the installation site and determine the location of the transmitter. Once the location is determined, refer to Figure 2-4 and use a forklift to move the transmitter to the desired location. After the transmitter is placed in the desired location, remove the shipping skid as follows:

1. Refer to Figure $2-4$ and remove the $5 / 16$ inch shipping bolts securing the transmitter to the skid.
2. Once the bolts are removed, slide the transmitter off the skid.
3. Slide the transmitter to the exact location.

2-22. COMPONENT INSTALLATION.
WARNING
ENSURE NO PRIMARY POWER IS CONNECTED TO THE TRANSMITTER BEFORE PROCEEDING.
WARNING

2-23. Selected components of the AM-10A and AM-6A transmitters have been removed to prevent damage during shipment. The components removed from the transmitter are shipped in separate containers.
2-24. Remove all tape, wire ties, string, and packing material used for shipment. In addition, locate the component containers. To install the components, perform the following procedures.


NOTES

1. AIR INLET AT REAR CF CABINETS, $1200 \mathrm{cfm}\left(34.0 \mathrm{~m}^{3} / \mathrm{MIN}\right.$.)
2. AIR $\operatorname{ZUTLET}$ AT TDP CF CABINETS, $15.69 " \times 24.38^{\prime \prime}(39.85 \mathrm{~cm} \times 61.93 \mathrm{~cm})$
3. ACCESS FDR aC POWER THROUGH CABINET TIP ACCESS HILES.
4. GROUND STRAP ENTRY POINT IN LIWER LEFT CIRNER AT REAR DF DUTPUT NETWIRK CABINET (SEE DETAIL "A")

5. ZUTPUT RF CINNECTIUN IS $1-5 / 8^{\prime \prime}$ FEMALE EIA FLANGE

ACCESS FIR MIDULATION MQNITUR RF SAMPLE
6. HEAT DISSIPATIUN: 6000 WATTS MAXIMLM ( 20,525 BTU/HR.) FDR 10.8 KW RF QUTPUT e 125\% AUDID TINE MIDULATIUN
7. WEIGHT: 635 LBS ( 288 KGS) UNPACKED.
8. PACKED CUBAGE: DIMESTIC $38.2 \mathrm{FT}^{3}\left(1,08 \mathrm{~m}^{3}\right)$

AC PAWER CINSUMPTIDN: 23 kW AT $125 \%$ SINUSOIDAL MIDULATIIN DF 10.8 KW CARRIER.
12. AC PQWER INPUT: $196-252$ QR $339-437$ VAC THREE PHASE AT 100 AMPS MAXIMUM; 196-252
VAC SINGLE PHASE AT 150 AMPS MAXIMUM; $50 / 60$ Hz, FUSED DISCDNNECT SWITCH RECDMMENDED. FDR PRDPER SIZING DF FUSES, REFER TD INSTRUCTION MANUAL AND NATIDNAL ELECTRICAL CIDEE OR LICAL CIDES
13. PRIMARY AC FUSED SERVICE DISCDNNECT:

THREE-PHASE
FUSE SIZE: 150A
WIRE SIZE: $2 / 0$ CDPPER
THHN QR EDUAL
THHN QR EDUAL
SINGLE PHASE
FUSE SIZE: 225A
WIRE SIZE: 250 MLM CIPPER
THHN IR EDLIAL



NDTES:

1. AIR INLET AT REAR aF CABINETS, $720 \mathrm{cfm}(20.4 \mathrm{~m} 3 \mathrm{MIN}$.
2. AIR DUTLET AT TIP पF CABINETS, $15.69^{\prime \prime} \times 24.38^{\prime \prime}(39.85 \mathrm{~cm} \times 61.93 \mathrm{~cm}$ )
3. ACCESS FIR AC PGWER THROUGH CABINET TIP ACCESS HDLES.
4. GRDUND STRAP ENTRY PDINT IN LIWER LEFT CDRNER AT REAR DF OUTPUT NETWDRK CABINET.
5. (SEE DETAIL "A")
6. ZUTPUT RF CDNNECTIDN IS 7/8" SEMI-RIGID FDAM CDAXIAL CABLE,

SEE CINNECTIDN INSTRUCTIUNS QN REAR PANEL DF OUTPUT NETWIRK
7. ACCESS FIR MIDULATIUN MINITDR RF SAMPLE
8. HEAT DISSIPATIDN: 4200 WATTS MAXIMLM ( $14,360 \mathrm{BTL} / \mathrm{HR}$.) FGR 6.6 KW RF OUTPUT e $100 \%$ AUDID TONE MDDULATIIN
9. WEIGHT: 442 LBS ( 200 KGS ) UNPACKED.
10. PACKED CLBBAGE: DOMESTIC $38.2 \mathrm{FT}^{3}\left(1.08 \mathrm{~m}^{3}\right)$
11. AC PDWER CONSUMPTIUN: 13.2 KW AT $100 \%$ SINUSOIDAL MIDULATICN DF 6.6 kW CARRIER.
12. AC PEWER INPUT: 196-252 पR 339-437 VAL THREE PHASE AT 52 AMPS MAXIMUM; 196-252 VAC SINGLE PHASE AT 90 AMPS MAXIMLM: $50 / 60 \mathrm{~Hz}$, FUSED DISCDNNECT SWITCH RECIMMENDED. FDR PRDPER SIZING GF FUSES, REFER TI INSTRUCTIDN MANUAL AND NATIUNAL ELECTRICAL CDDE aR LICAL CDDES.
13. PRIMARY aC FUSED SERVICE DISCDNNECT.

THREE-PHASE
FUSE SIZE: 75A
WIRE SIZE: ND. 4 CIPPER
THHN OR EDUAL
THHN DR EDUAL
SINGLE PHASE
FUSE SIZE: 125A
WIRE SIZE: ND. 1 CIPPER
THHN $\quad$ R ERUAL



## FIGURE 2-3. ACCEPTABLE AC POWER INPUT CONFIGURATIONS ${ }^{\text {597-0220-3 }}$



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## FIGURE 2-4. TRANSMITTER MOVING

597-1113-36
2-25. ECU CIRCUIT BOARDS. The ECU circuit boards are removed for shipment. Locate the circuit board shipping container. To re-install the circuit boards, proceed as follows:

CAUTION
THE TRANSMITTER MAY BE DAMAGED
IF THE ECU CIRCUIT BOARDS ARE NOT CAUTION SECURELY SEATED INTO THE CONNECTORS.

1. Refer to Figure 2-5 to determine the circuit board location.
2. Insert the circuit board in the appropriate location.
3. Firmly press the circuit board into the connector.
4. Firmly press the circuit board into the connector again to ensure the circuit board is seated.
5. Repeat the procedure for each ECU circuit board.


## CAUTION <br> REMOVING OR INSTALLING AN RF POWER MODULE WITH THE TRANSMITTER ENERGIZED MAY RESULT CAUTION IN DAMAGE TO THE MODULE.

2-26. RF POWER MODULES. Each RF power module is removed for shipment. Locate the RF power module shipping containers. Refer to Figure 2-5 and re-install the modules.
2-27. POWER SUPPLY. The transmitter power supply circuit boards may be removed for shipment. If the power supply circuit boards have been removed, locate the shipping container. Install each circuit board as follows:


597-1113-25
FIGURE 2-5. COMPONENT INSTALLATION
(2-9/2-10)


# THE TRANSMITTER MAY BE DAMAGED IF THE POWER SUPPLY CONNECTORS ARE NOT SECURELY SEATED INTO THE POWER SUPPLY CIRCUIT BOARD RECEPTACLES. 


#### Abstract

TO PREVENT DAMAGE TO THE POWER SUPPLY CIRCUIT BOARD, ENSURE THE CIRCUIT BOARD IS INSERTED INTO THE MOUNTING PINS AND THE CAPACITORS ON THE CIRCUIT SIDE OF THE BOARD ARE PLACED INTO THE PANEL CUTOUT PRIOR TO SLIDING THE CIRCUIT BOARD TO SEAT THE MOUNTING SLOTS INTO THE PINS.


1. Locate the mounting slots in the power supply circuit board and insert the board into the power supply mounting pins on the power supply panel. Ensure the circuit board is inserted with the capacitors on the circuit side of the board placed into the panel cutout prior to seating the circuit board in the mounting pins.
2. Slide the circuit board in a position to seat the circuit board slots in the mounting pins.
3. Secure the power supply circuit board mounting hardware.
4. Connect the power supply circuit board cables as follows:
A. Securely connect 12 -pin connector P 1 to J 1 on the power supply circuit board.
B. Securely connect 12-pin connector P2 to J2 on the power supply circuit board.
C. Securely connect 24 -pin connector P3 to J3 on the power supply circuit board.
5. Repeat the procedure for each power supply circuit board.

2-28. BATTERY INSTALLATION. The ECU is equipped with a battery system. Refer to Figure $2-5$ and install the battery in the battery receptacle.
2-29. CIRCUIT BOARD PROGRAMMING.
2-30. The AM-10A and AM-6A transmitters are designed with programmable transmitter operating characteristics. The operating characteristics are determined by the programmable circuitry on the ECU circuit boards (refer to Figure 2-5). Refer to the following text and program the circuitry for the desired operating characteristics.

2-31. EXCITER CIRCUIT BOARD. Exciter circuit board programming is presented in Figure 2-6. Refer to Figure 2-6 and program the circuit board as required.
2-32. External Stereo Generator Select. Programmable header J7 programs the circuitry if: 1) an external stereo generator is to be used with the transmitter or 2) the internal stereo circuit board is to be used with the transmitter. The transmitter is shipped with the circuit programmed for the internal stereo circuit board operation.
2-33. Carrier Frequency Programming. Eight position switch S2 programs the exciter carrier frequency. The switch is programmed for the station frequency at the factory. Refer to the factory test data sheets to check the programming of the switch. If the switch programming is not identical to programming recorded in the factory test data sheets, contact the Broadcast Electronics Customer Service Department.
2-34. PWM Frequency Programming. Four position switch S1 programs the PWM frequency. Refer to the factory test data sheets to check the programming of the switch.


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597-1111-11

FIGURE 2-6. EXCITER CIRCUIT BOARD PROGRAMMING

2-35. Frequency Synthesizer Programming. Programmable header J6 determines the frequency synthesizer band of operation. Refer to the factory test data sheets to check the programming of the header.
$2-36$. Pilot Tone Programming. Programmable header J5 establishes the pilot tone frequency for 10 kHz carrier frequency operation and 9 kHz carrier frequency operation. Refer to the factory test data sheets to check the programming of the header.
2-37. High-Pass Filter Defeat. Left channel programmable header J12 and right channel programmable header J13 control an exciter second order 10 Hz high-pass filter. The highpass filter is provided to remove low frequency residual products from specific audio processing units. The filter is shipped from the factory in the enabled position. Evaluate the audio processor and determine if low frequency residual products are present at the output of the audio processing unit. If no low frequency residual products are present, refer to Figure 2-6 and disable the high pass filter.
2-38. High Frequency Boost Defeat. Left channel programmable header J2 and right channel programmable header J3 control an exciter high frequency boost circuit. The high frequency boost circuit provides increased high frequency response to compensate for a Bessel filter in the PWM modulator. If the high frequency boost circuit is enabled to compensate for the filter, the circuit will result in a compromise between the frequency and transient response performance. If the high frequency boost circuit is enabled, the transmitter frequency response will increase approximately 2 dB at 10 kHz and the transient response will degrade. If the high frequency boost circuit is disabled, the transmitter frequency response will decrease approximately 2 dB at 10 kHz and the transient response will improve. The high frequency boost circuit is shipped from the factory in the disabled position.
2-39. Monophonic Transmitter Operation Channel Select. Programmable header J4 selects either the left or right audio channel when the transmitter is operating in the monophonic mode with the stereo circuit board removed. The transmitter is shipped with the left channel audio selected for monophonic operations.
2-40. STEREO CIRCUIT BOARD. Stereo circuit board programming is presented in Figure 2-7. Refer to Figure 2-7 and program the circuit board as required.
2-41. Antenna C Equalization Select. Programmable header J6 selects equalization circuit 1 or equalization circuit 2 for operation with antenna C. The transmitter is shipped with equalization circuit 2 configured for operation with antenna C.
2-42. Bandpass Filter Alignment. Programmable header J5 configures the bandpass filter for alignment. The jumper must be installed in position 1-2.
2-43. Bandpass Filter Programming. Four position switches S2 through S4 program the bandpass filter. Refer to the factory test data sheets to check the programming of the switches.
2-44. Equalization Control Select. Programmable header J7 configures the equalization circuitry for either a momentary or constant antenna status signal. The transmitter is shipped with equalization control circuitry configured for a constant status signal.
$2-45$. CONTROLLER CIRCUIT BOARD. Controller circuit board programming is presented in Figure 2-8. Refer to Figure 2-8 and program the circuit board as required.
2-46. Power Level Trim Reset Select. Programmable header J12 determines if the power level control circuit is to reset when a power level switch/indicator is depressed. If the circuit is programmed to reset, the previous raise/lower information will be deleted and the transmitter will operate at the selected power level. If the circuit is programmed to retain the previous raise/lower information, the transmitter will operate above or below the selected power level as determined by previous raise/lower operations. For example, the transmitter is operating at power level 4 with the power level raised $5 \%$ by the power level raise/ lower circuit. When power level 5 switch/indicator is depressed, the transmitter will operate at $5 \%$ above the power level 5 output due to the previously retained raise/lower information. The transmitter is shipped with power level trim reset circuit configured to reset.


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FIGURE 2-7. STEREO CIRCUIT BOARD PROGRAMMING


FIGURE 2-8. CONTROLLER CIRCUIT BOARD PROGRAMMING

2-47. Antenna Power Level Programming. Switches S1, S2, and S3 assign power levels to a specific antenna. This programs the antenna interlock circuit to the station antenna system to prevent the transmitter from operating into an antenna at an incorrect power level. Switch S1 programs the power levels for antenna A. Switch S2 programs the power levels for antenna B. Switch S3 programs the power levels for antenna C. Power level 2 is assigned to an antenna by switch 1 on S1, S2, and S3. Power level 3 is assigned to an antenna by switch 2 on S1, S2, and S3. Power level 4 is assigned to an antenna by switch 3 on S1, S2, and S3. Power level 5 is assigned to an antenna by switch 4 on S1, S2, and S3. Power level 1 is assigned to each antenna. Evaluate the antenna system and program the circuit as required.
2-48. AC Power Failure Automatic Transmitter Shutdown Time. Programmable headers J4, J5, J6, and J7 program the transmitter ac power failure automatic transmitter shutdown timer circuit. The circuit is designed to automatically operate the transmitter to off during a power failure after a specific time delay programmed by headers J 4 , J 5 , J6, and J7. J4 programs the circuit for a 1 minute shutdown time. J5 programs the circuit for a 4.5 min ute shutdown time. J6 programs the circuit for a 17 minute shutdown time. J7 programs the circuit for a 68 minute shutdown time. The transmitter is shipped from the factory for a 1 minute shutdown time.
2-49. Antenna Interlock Control Select. Programmable header J1 controls the antenna interlock circuit. The circuit can be disabled if the transmitter is to operate into only one antenna. The transmitter is shipped from the factory with the antenna interlock circuit disabled.
2-50. Power Level Reference. Programmable headers J10 and J19 provide a reference for the power level circuit. For the AM-10A transmitter, ensure jumper P10 is removed and jumper P19 is installed. For the AM-6A transmitter, ensure jumpers P10 and P19 are removed.
2-51. Power Level 3 Assignment. Programmable header J8 and J9 control the assignment for the power level 3 switch/indicator. For the AM-10A, the power level 3 switch/indicator can be programmed to control power from: 1) 3 kW to 10.8 kW or 2) 50 watts to 5 kW . For the AM-6A, the power level 3 switch/indicator can be programmed to control power from: 1) 25 watts to 3 kW or 2$) 2 \mathrm{~kW}$ to 6.6 kW . The power level 3 switch/indicator is shipped from the factory to control power from: 1) 50 watts to 5 kW on AM-10A models and 2) 25 watts to 3 kW on AM-6A models. Program jumpers P8 and P9 as required.
$2-52$. Remote Reflected Power Sample Voltage Programming. Programmable header J3 controls the remote reflected power meter sample voltage. The remote reflected power sample can be programmed for a +5.0 volt dc or +2.5 volt dc full-scale meter indications. The transmitter is shipped from the factory programmed for +5.0 volt dc full-scale remote reflected power meter indications.
2-53. Remote Forward Power Sample Voltage Programming. Programmable header J2 controls the remote forward power meter sample voltage. The remote forward power sample can be programmed for a +5.0 volt dc or +2.5 volt dc full-scale meter indications. The transmitter is shipped from the factory programmed for +5.0 volt dc full-scale remote forward power meter indications.
2-54. High Forward Power Defeat. Programmable header J11 controls the high forward power detector circuit. Ensure jumper P11 is removed.
$2-55$. Reflected/Forward Power Sample Programming. Programmable headers J15, J16, J17, and J18 control the reflected and forward power sample levels. Headers J15 and J17 control the forward power sample. Headers J16 and J18 control the reflected power sample. For AM-10A models, jumpers P15, P16, P17 and P18 must be removed. For AM-6A models: 1) install jumpers P15 and P16 and 2) remove jumpers P17 and P18.
2-56. Forward Power Reference Voltage Programming. Programmable headers J13 and J14 establish the forward power reference level for a comparator circuit. Jumpers P13 and P14 must be installed in the AM-10A and AM-6A transmitters. Ensure jumpers P13 and P14 are installed.

2－57．Temperature Sense．Header J20 controls the temperature sense sample voltage．Ensure P20 is removed for all models．
$2-58$ ．POWER SUPPLY CIRCUIT BOARD．The power supply circuit board programming is pre－ sented in the following text．Refer to the following text to check the power supply circuit board programming．
2－59．Future Corrector Circuit．Programmable headers J9 and J10 establish parameters for a future corrector circuit．Ensure jumper P9 is removed and P10 is installed．
2－60．Model Programming．Programmable headers J5 through J8 establish parameters for dif－ ferent AM A－Series transmitters．Refer to the following text for the programming infor－ mation．

| TRANSMITTER | J5 | J6 | J7 | J8 |
| :--- | :--- | :--- | :--- | :--- |
| AM－6A | Not Used | Not Used | Not Used | Not Used |
| AM－10A | Not Used | Not Used | Not Used | Not Used |

2－61．REMOTE CONTROL．

## ENSURE PRIMARY POWER IS DISCONNECTED BE－ FORE PROCEEDING．

2－62．GENERAL．The AM－10A and AM－6A transmitters are designed for complete remote con－ trol operations（refer to Figure 2－9 ）．The transmitters will interface with almost any re－ mote control unit such as the Broadcast Electronics model VMC－16 voice remote control system．The following text presents a description of the transmitter remote control func－ tions and indications．The remote control functions are activated using a +5 to +15 volt dc signal．The remote indication functions：1）require current limiting resistors and 2）pro－ vide up to 100 mA for indicators．A +5 volt supply is provided on the ECU rear－panel for remote control operations．The remote control connections are located on the rear－panel of the ECU．
2－63．Power Level Controls／Indicators．The transmitter is designed with five customer adjust－ able operating power controls．The controls are located at TB1－1 through TB1－5．A +5 to +15 volt de signal is required to activate the desired function．
2－64．Indications of power level control operations are located at TB1－7 through TB1－11．The power level status indicators will go LOW（ 0 volts dc）when activated．
2－65．Transmitter Off Control／Indicator．The transmitter off control is located at TB1－6．A +5 to +15 volt dc signal is required to operate the transmitter to off．The indicator for the trans－ mitter off control is located at TB1－12．The off indicator will go LOW（ 0 volts dc）when ac－ tivated．
2－66．Power Level Raise／Lower Controls．The transmitter is designed with raise and lower con－ trols to adjust the transmitter output power level．The controls are equipped with ability to raise／lower power from $10 \%$ to $15 \%$ of the selected output power level．The controls are located at TB1－16 and TB1－17．A +5 to +15 volt dc signal is required to activate the de－ sired function．
2－67．Antenna Interlock Input．The antenna interlock inputs are designed for the connection of the status signals from antenna A，B，and C．The inputs are located at TB1－24 through TB1－26．The inputs require $\mathrm{a}+5$ to +15 volt dc signal to indicate an antenna ready status．
2－68．Transmitter Mute Input．The transmitter mute input is designed to mute the transmitter when activated．The input is located at TB1－27．The input requires a +5 to +15 volt dc signal to mute the transmitter．


FIGURE 2-9. REMOTE CONTROL AND AUDIO CONNECTIONS

2-69. Remote Failsafe Input. The remote failsafe input is designed for the remote control unit failsafe control line. The input is located at TB1-28. The input requires a +5 to +15 volt dc signal to indicate an enabled remote control unit.
2-70. External Interlock Input. The external interlock input is for the connection of an interlock external to the transmitter. The input is located at TB1-29. The input requires a +5 to +15 volt dc signal to indicate a closed interlock.
2-71. Interlock +5 V . The interlock +5 volt supply is provided for the external interlock. The +5 volt supply is located at TB1-30.
2-72. Exciter Mode Controls/Indicators. The transmitter exciter is designed to be operated in the mono left, mono right, mono L+R, or stereo modes of operation. The controls are located at TB2-1 through TB2-4. A +5 to +15 volt de signal is required to activate the desired function.

2-73. Indications of exciter modes of operations are located at TB2-5 though TB2-8. The exciter mode indicators will go LOW when activated.

2-74. Remote Forward/Reflected Power Meter Indications. Remote reflected power meter indications are located at TB2-9 and TB2-10. The indications are designed to be programmed for +5 volt dc full-scale meter indications or +2.5 volt dc full-scale meter indications.

2-75. Remote Enabled Indications. The remote enabled indicator provides a signal to indicate the status of transmitter remote control operations. The remote enabled indicator is located at TB2-11. The indicator will go LOW to indicate when remote control operations are enabled.

2-76. Antenna Conflict Indications. The antenna conflict indicator provides a signal to indicate when the transmitter is configured to operate into an incorrect antenna. The antenna conflict indicator is located at TB2-12. The indicator will go LOW ( 0 volts dc) to indicate when the transmitter is configured for operation into an incorrect antenna.
2-77. Maintenance Indications. The maintenance indicator provides a signal to indicate when a transmitter power supply or an RF power module is removed from the transmitter for maintenance. The maintenance indicator is located at TB2-13. The indicator will go LOW ( 0 volts dc) to indicate when a power supply is removed for maintenance.

2-78. Lightning Indications. The lightning indicator provides a signal to indicate when a greater than: 1) 2700 volt potential is present at the output for AM-10A models or 2) 2100 volt potential is present at the output for AM-6A models. The lightning indicator is located at TB2-14. The indicator will go LOW ( 0 volts dc) to indicate when a lightning potential is present at the transmitter output.

2-79. $1.2: 1$ VSWR Indications. The 1.2:1 VSWR indicator provides a signal to indicate when a greater than $1.2: 1$ VSWR condition is present at the transmitter output. The $1.2: 1$ indicator is located at TB2-15. The indicator will go LOW ( 0 volts dc) to indicate when a $1.2: 1$ VSWR condition is present at the transmitter output.
2-80. Exciter/PWR Supply/PWR Module Fault Indications. The exciter, power supply, and power module fault indicators provide signals to indicate when an exciter, power supply, or a power module fault has occurred. The exciter, power supply, and power module fault indicators are located at TB2-16 through TB2-18. The indicators will go LOW ( 0 volts dc) to indicate when an exciter, power supply, or a power module fault has occurred.
2-81. RFL PWR High Indications. The reflected power high indicator provides a signal to indicate when: 1) 400 watts of reflected power is present at the transmitter output for AM-10A models or 2) 240 watts of reflected power is present at the transmitter output for AM-6A models. The high reflected power indicator is located at TB2-19. The indicator will go LOW ( 0 volts dc) to indicate when a reflected power high condition is present at the transmitter output.

2-82. RFL PWR Emergency Indications. The reflected power emergency indicator provides a signal to indicate when greater than: 1) 2000 watts of reflected power is present at the output of the AM-10A transmitter or 2) 1200 watts of reflected power is present at the output of the AM-6A transmitter. The reflected power emergency indicator is located at TB2-20. The indicator will go LOW ( 0 volts dc) to indicate when a reflected power emergency condition is present at the transmitter output.
2-83. Overtemp Indications. The overtemp indicator provides a signal to indicate when the transmitter temperature is greater than $70^{\circ} \mathrm{C}$. The overtemp indicator is located at TB2-21. The indicator will go LOW ( 0 volts dc) to indicate when the transmitter temperature is greater than $70^{\circ} \mathrm{C}$.
$2-84$. Foldback Indications. The transmitter is designed to automatically reduce power when one of the following fault condition occurs: 1) high reflected power, 2) high forward power, 3) high temperature, or 4) detection of a high voltage by the lightning circuit. The foldback indicator is located at TB2-22. The indicator will go LOW ( 0 volts dc) to indicate when the transmitter is in a foldback condition.
2-85. Alarm Status Indications. The alarm status provides a signal to indicate when a fault or foldback condition occurs. The alarm status indicator is located at TB2-23. The indicator will go LOW ( 0 volts dc) to indicate when the transmitter is in a fault or foldback condition.
$2-86$. Alarm Reset Control. The alarm reset control is designed to reset the fault detection circuitry. The alarm reset control is located at TB2-24. A +5 to +15 volt dc signal is required to activate the function.

## $2-87$. WIRING.

2-88. Wiring consists of connecting audio, the RF transmission line, and ac power to the transmitter. Refer to the following text and connect the wiring to the transmitter.
2-89. AUDIO INPUT CONNECTION. The AM-10A and AM-6A transmitters are equipped with electronically balanced 600 Ohm left and right channel audio inputs. The audio inputs are located on the ECU rear-panel (refer to Figure 2-9). The inputs are designed to accept a +10 dBm signal at 600 Ohms.

## I WARNING ENSURE PRIMARY POWER IS DISCONNECTED BEFORE PROCEEDING.

WARNING
2-90. Audio is interfaced to the transmitter by: 1) selecting the appropriate cable and 2) connecting the cable to the terminals on the ECU rear-panel. To interface audio to the transmitter: 1) use Belden 8760 cable or equivalent and 2) refer to Figure 2-9 and connect the audio to the transmitter as follows:

1. Connect the plus signal line to the + terminal.
2. Connect the minus signal line to the terminal.
3. Connect the shield to ground.

2-91. EXTERNAL STEREO RF INPUT. The transmitter is equipped with an external stereo RF input on the ECU rear-panel. The input is designed for the connection of an external stereo generator or reference oscillator with a signal level from 5 to 15 volts peak-topeak. If an external stereo signal/reference is to be applied to the transmitter, connect the signal to the J1 EXTERNAL STEREO RF INPUT connector on the ECU rearpanel and program jumper P7 on the exciter circuit board in position 1-2.
2-92. AM-10A RF TRANSMISSION LINE CONNECTION. The AM-10A RF output connection is a $15 / 8$ inch EIA flange. The connector is located on the output network assembly rearpanel (refer to Figure 2-10). To connect the RF transmission line to the transmitter, refer to Figure 2-10 and route the transmission line to the transmitter RF output connection. Connect the transmission line to the EIA flange. The flange is secured with four bolts.


FIGURE 2-10. AM-10A RF OUTPUT CONNECTIONS
2-93. AM-6A RF TRANSMISSION LINE CONNECTION. The AM-6A transmitter RF output connection is located on the output network assembly rear-panel (refer to Figure 2-11). The connection is designed for 7/8 inch transmission line. To connect the RF transmission line to the transmitter, refer Figure 2-11 and proceed as follows:

1. Remove the RF transmission line clamp from the bracket.
2. Prepare the RF transmission line for connection as follows:
A. Refer to Figure 2-11 and strip the transmission line as shown.
B. Use a hammer to flatten the end of the cable to the dimensions shown.


FIGURE 2-11. AM-6A RF OUTPUT CONNECTIONS
C. Locate a .281 drill and bore a hole in the end of the cable as shown.
3. Route the transmission line cable to the output network assembly as shown.
4. Attach the cable as follows:
A. Attach the transmission line to the RF output connector as shown.
B. Insert and secure the RF transmission line clamp to the bracket as shown.

2-94. EXTERNAL INTERLOCK. The AM-10A/AM-6A is equipped with an external interlock such as for a test load. The interlock will turn off the transmitter RF output when opened. The interlock is located at TB1-29 and TB1-30 on the rear-panel of the ECU unit. Refer to External Interlock Input and Interlock +5v in the REMOTE CONTROL section of the preceding text and perform the procedures to connect equipment to the transmitter external interlock.

2-95. MODULATION MONITOR. The modulation monitor connection is located on the output network rear-panel. Refer to Figure 2-10 and connect the modulation monitor to the modulation monitor receptacle.

## ENSURE PRIMARY POWER IS DISCONNECTED BEFORE PROCEEDING.

## 4 <br> WARNING <br> WARNING

## ENSURE AN EARTH GROUND CONDUCTOR IS SECURELY CONNECTED TO THE TRANSMITTER AC GROUND LUG.

2-96. AC POWER CONNECTIONS. The AM-10A transmitter requires: 1) a Delta/Wye threephase source of 196 V to $252 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ at 150 amperes, 2) a Wye three-phase source of 339 V to 437 V ac $50 / 60 \mathrm{~Hz}$ at 150 amperes, or 3 ) a single phase source of 196 V to 252 V ac $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ at 225 amperes. The AM-6A transmitter requires: 1) a Delta/Wye threephase source of 196 V to $252 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ at 75 amperes, 2 ) a Wye three-phase source of 339 V to 437 V ac $50 / 60 \mathrm{~Hz}$ at 75 amperes, or 3 ) a single phase source of 196 V to 252 V ac $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ at 125 amperes. For operating safety, the power source must be routed to the transmitter through a fused power disconnect (refer to Figures 2-12 through 2-15). The transmitter ac input configuration can be verified by checking the ac distribution panel part number. Ensure the transmitter is configured for the proper ac power configuration using the following ac distribution panel part numbers.

| AM-10A TRANSMITTER |  |
| :--- | :--- |
| AC DIST. PANEL <br> PART NUMBER | DESCRIPTION |
| $957-0021-001$ | 196 V to $252 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ Delta/Wye three-phase <br> ac input. <br> $957-0021-041$ <br> 339 V to $437 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ Wye three-phase ac in- <br> put. <br> $957-0021-011$ |


| AM-6A TRANSMITTER |  |
| :--- | :--- |
| AC DIST. PANEL <br> PART NUMBER | DESCRIPTION |
| $957-6000-030$ | 196 V to $252 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ Delta/Wye three-phase <br>  <br> $957-6000-040$ <br> $957-6000$ |
| 339 V to $437 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ Wye three-phase ac in- <br> put. <br> 196 V to $252 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ single-phase ac input. |  |

## $4 W^{\text {WARNING }}$

## ENSURE PRIMARY POWER IS DISCONNECTED BEFORE PROCEEDING.

2-97. Three-Phase Main ac Input - AM-10A - Refer to Figure 2-12 and connect the 150 Ampere service to ac input/control device CB1 through a fused service disconnect as shown. Ensure a utility company ground conductor is securely connected to the transmitter common ground system and the ac service ground wire is securely connected to the ac ground lug as shown.

2-98. Single-Phase Main ac Input - AM-10A - Refer to Figure 2-13 and connect the 225 Ampere service to ac input/control device CB1 through a fused service disconnect as shown. Ensure a utility company ground conductor is securely connected to the transmitter common ground system and the ac service ground wire is securely connected to the ac ground lug as shown.

2-99. Three-Phase Main ac Input - AM-6A - Refer to Figure 2-14 and connect the 75 Ampere service to ac input/control device CB1 through a fused service disconnect as shown. Ensure a utility company ground conductor is securely connected to the transmitter common ground system and the ac service ground wire is securely connected to the ac ground lug as shown.

2-100. Single-Phase Main ac Input - AM-6A - Refer to Figure 2-15 and connect the 125 Ampere service to ac input/control device CB1 through a fused service disconnect as shown. Ensure a utility company ground conductor is securely connected to the transmitter common ground system and the ac service ground wire is securely connected to the ac ground lug as shown. BEFORE PROCEEDING.

## ENSURE AN EARTH GROUND CONDUCTOR IS SECURELY CONNECTED TO THE TRANSMITTER GROUND LUG.

2-101. GROUND. The transmitter is equipped with a cabinet ground system for operating safety. The ground system requires the connection of an earth ground. Refer to Figures 2-12 through 2-15 to connect an earth ground to the cabinet ground lug as shown using a 2 inch ( 5.08 cm ) wide copper strap.






FIGURE 2-15. AM-6A SINGLE-PHASE PRIMARY AC WIRING

2-102. TRANSMITTER SITE LIGHTNING PROTECTION SYSTEM CHECKOUT.
CAUTION
CAUTION

## THE TRANSMITTER SITE LIGHTNING PROTECTION SYSTEM MUST BE INSPECTED AND IN PROPER WORKING CONDITION FOR RELIABLE TRANSMITTER OPERATION.

$2-103$. For reliable transmitter operation, the transmitter site lightning protection system must be inspected and in proper working condition. Due to the solid-state design of the transmitter, high voltage potentials from lightning activity can cause severe damage to the transmitter circuitry. Therefore, perform the following procedures to inspect and improve the lightning protection system at the transmitter site. Refer to the NAB Radio Handbook for additional transmitter site lightning protection system information.

2-104. ANTENNA BALL-GAP LIGHTNING ARRESTOR. Each tower in the antenna system must be equipped with a ball-gap lightning arrestor (refer to Figure 2-16). The ball-gap arrestor is designed to safely conduct lightning potentials to ground. Inspect the ball-gap arrestors by performing the following procedures.

2-105. Ball-Gap Position. The antenna ball-gap lightning arrestor must be aligned horizontally. Do not align the ball-gaps vertically. Vertical alignment allows rain water to collect on the balls. This reduces the gap separation and results in arcing during rain activity.
$2-106$. Ball-Gap Separation. The antenna ball-gap lightning arrestor must be adjusted for the proper separation. If the ball-gap separation is too wide, the arrestor will not function. If the ball-gap separation is too narrow, the arrestor will arc during normal transmitter operation. As a general rule: 1) a separation of approximately 0.020 in . for each peak kilovolt at the transmitter tower is required or 2) 0.125 inch for each 9.4 peak kilovolt at the transmitter tower is required.
$2-107$. The recommended method for ball-gap separation adjustment is to adjust the gap to prevent arcing during peak modulation activity. To adjust the separation, proceed as follows:

1. Adjust the ball-gap separation using the general rule presented in the preceding text.
2. Operate the transmitter at peak modulation and check the ball-gap for arcing activity.

WARNING DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.
WARNING
3. Operate the transmitter to off.
4. Adjust the ball-gap separation as follows:
A. If no arcing activity is detected, reduce the ball-gap separation.
B. If arcing activity is detected, increase the ball-gap separation.
5. Repeat the procedure until the ball-gap separation is adjusted for the smallest gap possible without arcing during peak modulation activity.

2-108. ANTENNA-TUNING-UNIT SPARK-GAP LIGHTNING ARRESTOR. The antenna-tuningunit (ATU) must be equipped with a spark-gap lightning arrestor (refer to Figure 2-16). The spark-gap arrestor can be: 1) a ball-gap type or 2) a horn type. Adjust the spark-gap for the smallest possible gap without arcing during peak modulation activity.


DETAIL "A"
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FIGURE 2-16. ANTENNA LIGHTNING PROTECTION SYSTEM

2-109. TRANSMITTER SITE GROUNDING SYSTEM. The transmitter site grounding system must be properly connected for reliable transmitter operation. A typical transmitter site grounding system is shown in Figure 2-16. Perform the following procedures to ensure the grounding system connections are secure.

1. Ensure the antenna base ground strap is securely connected to the antenna ground plane radials.
2. Ensure the antenna ball-gap lightning arrestor is securely connected to the lightning ground rod system and to the antenna ground plane radials.
3. Ensure the ATU ground and the station RF ground is securely connected to the antenna ground plane radials.

2-110. CABLE PROTECTION. The ac line cable, audio/control cables, and the RF output transmission line require a combination of MOV and ferrite core protection to prevent the entry of lightning potentials (refer to Figure 2-16). Refer to the following text to install MOV and ferrite cores on the cables to prevent the conductance of lightning potentials. Ensure MOVs are connected from the ac line and audio/control cable conductors to the station RF ground as shown. The MOVs should be rated for 20,000 Ampere surges.
(BE P/N 140-0032)
2-111. Ferrite Core. The ac line cable, the audio/control cables, and the RF output transmission line also require the placement of ferrite cores. The cores are designed to create a high impedance for undesired current paths such as lightning. Ferrite cores for placement on ac line audio/control and RF output transmission line cables are located in the accessory parts kit. Locate the ferrite cores and install the cores by performing the following procedures.

2-112. Modulation Monitor Core. One 375-0009 ferrite core is designed to be installed on the modulation monitor cable. Install the core on the modulation monitor cable by: 1) routing the cable through the core and 2) wrapping the cable to create one cable loop around the core. The core can be installed at any location on the cable.

2-113. Audio/Remote Control/Status Core. A second 375-0009 ferrite core is designed to be installed on the audio and remote control/status cables. Install the core on the audio and remote control/status cables by: 1) routing the cables through the core and 2 ) if possible, wrapping the cables to create one cable loop cable around the core. The core can be installed at any location on the cables.

2-114. Ac Input Core. A ferrite core is shipped with the unit for installation on the transmitter ac input cable. A 360-0099 ferrite core is provided for AM-10A models. A 375-0007-001 ferrite core is provided for AM-6A models. Install the core by routing: 1) all ac line phase cables through the core or 2) all ac line phase cables and ground cable through the core. Place the core at any location between the wall mounted fused disconnect and the transmitter ac input switch.
2-115. RF Output Core. A second ferrite core is designed to be installed on the transmitter RF output transmission line cable. A 360-0099 ferrite core is provided for AM-10A models. A 375-0007-001 ferrite core is provided for AM-6A models. Install the core by routing the RF output cable through the core. Place the core at any location between the transmitter RF output connector and the next equipment connection in the RF output system such as the antenna phasing system. It is recommended the core be placed outside the transmitter cabinet.
$2-116$. ANTENNA RF FEED LINE. Check the antenna RF feed line between the ATU and the tower. Ensure the line contains one or more one foot diameter loops. The loops function as a series inductance and increase the impedance of the line.

## $2-117$. TRANSMISSION LINE AND ANTENNA CHECKOUT.

CAUTION CAUTION

2-118. The transmission line and antenna must be inspected and in proper working condition for reliable transmitter operation. Perform the following procedures to inspect the transmission line and antenna.

2-119. ANTENNA VSWR. The AM-10A is designed to operate into an antenna with a maximum VSWR of $1.4: 1$. The AM-6A is designed to operate into an antenna with a maximum VSWR of $1.5: 1$. Check the antenna VSWR. If the VSWR is greater than $1.4: 1$ for AM-10A models or 1.5:1 for AM-6A models, contact the Broadcast Electronics Customer Service Department. Typically, the antenna will require the installation of an additional tuning unit to reduce the antenna VSWR.

2-120. COAXIAL SWITCH CONTROLLER. To prevent damage to the transmitter, the transmitter must be muted during any antenna change sequence. Inspect the motorized coaxial switch controller and ensure the unit outputs a +5 volt to +15 volt mute signal. Ensure the mute signal is applied to the transmitter.

2-121. ATU AND PHASOR CHECKOUT. Inspect the ATU and the antenna phasor unit (if installed in the system) for arcing activity during peak modulation periods. Repair or replace any devices to prevent arcing during peak modulation periods.
$2-122$. INITIAL CHECKOUT.

## $4 \begin{aligned} & \text { WARNING } \\ & 4 \varnothing\end{aligned}$

## ENSURE PRIMARY POWER IS DISCONNECTED BEFORE PROCEEDING.

2-123. Prior to performing the preliminary operating procedures, the transmitter should be checked to ensure all installation and connection procedures have been performed. To check the transmitter, proceed as follows:
A. Ensure all ECU circuit boards, RF power modules, and power supply circuit boards are installed.
B. Ensure the RF output transmission line is connected to the transmitter output network.
C. Ensure the station earth ground is connected to the transmitter ground terminal.
D. Ensure all audio and control cables are connected to the transmitter.
E. Ensure the modulation monitor is connected to the transmitter.
F. Ensure all ac power connections are secure.
G. Ensure the station RF output transmission line system and antenna are in proper working condition.
H. Ensure the antenna lightning protection system is in proper working condition.
$2-124$. PRELIMINARY OPERATION AND ADJUSTMENT.
2-125. Adjust the transmitter for operation with the equipment at the installation site as follows:

WARNING
WARNING
THE TRANSMITTER POWER SUPPLY OPERATES FROM A HIGH FLOATING GROUND POTENTIAL. NEVER OPERATE THE TRANSMITTER WITH THE REAR-DOOR OPEN.
$2-126$. TUNING. The transmitter must be adjusted to operate into the station antenna. To tune the transmitter, proceed as follows:

2-127. Operate the rear-door ac on/off switch to ON. The ECU and power module front-panel indicators will illuminate.

2-128. Depress the power level 1 switch/indicator to illuminate the switch/indicator.
2-129. Operate the FORWARD POWER meter switch to LOW and observe the forward power indication.

2-130. Operate the REFLECTED POWER meter switch to LOW and observe the reflected power indication.

2-131. Tune the transmitter by adjusting the TUNING and LOADING controls as required for a minimum reflected power indication on the REFLECTED POWER meter.

2-132. POWER LEVEL AND MODULATION MONITOR CALIBRATION ADJUSTMENTS. The transmitter power levels are adjusted to the levels specified in the sales order at the factory. If no power levels are specified, the levels are adjusted as follows:

| AM-10A | AM-6A |
| :--- | :--- |
| Power level $1=2 \mathrm{~kW}$ | Power level $1=1 \mathrm{~kW}$ |
| Power level $2=4 \mathrm{~kW}$ | Power level $2=2 \mathrm{~kW}$ |
| Power level $3=6 \mathrm{~kW}$ | Power level $3=3 \mathrm{~kW}$ |
| Power level $4=8 \mathrm{~kW}$ | Power level $4=4 \mathrm{~kW}$ |
| Power level $5=10 \mathrm{~kW}$ | Power level $5=6 \mathrm{~kW}$ |

$2-133$. If desired, the transmitter power levels can be changed at any time. If the transmitter power levels are adjusted, the modulation monitor output must also be re-calibrated. To change the power level and re-calibrate the modulation monitor output, proceed as follows:

DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.
WARNING
2-134. Operate the transmitter rear-door ac on/off control switch to OFF and open the rear-door.
2-135. Refer to Figure 2-17 and connect the test equipment to the transmitter modulation connector as shown.

2-136. Operate the transmitter rear-door ac on/off control switch to ON.
2-137. Depress power level control 1 switch/indicator to illuminate the switch/indicator.
2-138. Operate the FORWARD POWER meter switch to LOW or HIGH as required and observe the forward power indication.
2-139. Refer to Figure 2-8 and adjust the power level 1 control to obtain the desired indication on the FORWARD POWER meter. The control range is from: 1) 50 W to 5 kW on AM-10A models and 2) 25 W to 3 kW on AM-6A models.

2-140. Refer to Figure 3-1 in SECTION III, OPERATION and adjust the power level 1 modulation monitor calibration control for a 5.7 volt peak-to-peak signal on the oscilloscope.
$2-141$. Repeat the procedure for power levels 2 through 5 . The power level control ranges are as follows:

AM-10A

1. Power level 2 - 50 W to 5 kW .
2. Power level $3-50 \mathrm{~W}$ to 5 kW or 3 kW to 10.8 kW as programmed by a jumper on the controller circuit board.
3. Power level $4-3 \mathrm{~kW}$ to 10.8 kW .
4. Power level $5-3 \mathrm{~kW}$ to 10.8 kW .

AM-6A

1. Power level 2 - 25 W to 3 kW .
2. Power level 3 - 25 W to 3 kW or 2 kW to 6.6 kW as programmed by a jumper on the controller circuit board.
3. Power level $4-2 \mathrm{~kW}$ to 6.6 kW .
4. Power level $5-2 \mathrm{~kW}$ to 6.6 kW .


AM-10A SHDWN
AM-6A IS IDENTICAL

## FIGURE 2-17. TEST EQUIPMENT CONNECTIONS, POWER LEVEL CALIBRATION

## $4 \begin{aligned} & \text { WARNING } \\ & 4 \varnothing \text { WARNING }\end{aligned}$

## DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.

2-142. Operate the transmitter rear-door ac on/off control switch to OFF.
2-143. Disconnect the cable from the transmitter modulation monitor connector.
2-144. STEREO ADJUSTMENT. If the transmitter is operated in the stereo mode, the transmitter stereo circuitry must be adjusted to compensate for antenna system variances. The primary objective in the adjustment of the transmitter is to configure the stereo circuitry to minimize distortion and maximize separation across the entire audio band. A proof of performance sheet is provided at the end of this section to record performance measurements. To adjust the stereo circuitry, perform the following procedures and record the measurements on the proof of performance sheet at the end of this section.

## 4 WARNING

2-145. Operate the transmitter rear-door ac on/off control switch to OFF.
2-146. Refer to Figure 2-18 and connect the test equipment as shown.


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FIGURE 2-18. TEST EQUIPMENT CONNECTIONS, SEPARATION
$2-147$. Operate the oscilloscope for: 1) $200 \mathrm{mV} /$ div sensitivity and 2) dc coupled.
2-148. Refer to Figure 2-9 and connect an audio generator to the audio input terminals on the ECU rear-panel.

2-149. Operate the transmitter rear-door ac on/off control switch to ON.
2-150. Select the antenna which is configured for equalization circuit 1 operation (refer to STEREO CIRCUIT BOARD PROGRAMMING in the preceding text if required) and determine a power level.
$2-151$. Depress the desired power level switch/indicator to illuminate the switch/indicator.
$2-152$. Refer to SECTION III, OPERATION and perform the following:

1. Operate the stereo circuit board mode control switch to illuminate the stereo indicator. When power is applied to the transmitter, the stereo circuit board will automatically be configured to the stereo mode.
2. Operate the stereo circuit board pilot switch to off.
3. Ensure the equalization circuit 1 indicator on the stereo circuit board is illuminated.

2-153. Adjust equalization circuit 1 as follows:

1. Adjust the audio generator for a 1 KHz left channel output at +10 dBm and observe the lissajous pattern displayed on the oscilloscope.
2. Refer to Figure 2-7 and adjust the left channel level control to obtain a horizontal lissajous pattern (refer to Figure 2-19).
3. Adjust the group delay as follows:
A. Configure the group delay circuitry for adjustment as follows:
4. Refer to Figure 2-7 and configure the left channel 4 microsecond and 8 microsecond sections to in.
5. Refer to Figure 2-7 and operate the left channel delay control fully counterclockwise.
B. Refer to Figure 2-7 and adjust the left channel delay control to close the oscilloscope display and obtain a straight-line lissajous display as shown in the maximum left channel separation lissajous pattern (refer to Figure 2-19). If the display will not close, proceed as follows:
6. Refer to Figure 2-7 and: 1) configure only the 8 microsecond delay section to in and 2) adjust the left channel delay control to close the oscilloscope display.
7. If the display will not close refer to Figure 2-7 and: 1) configure only the 4 microsecond delay section to in and 2) adjust the left channel delay control to close the oscilloscope display.
8. Adjust the separation at 7 kHz as follows:
A. Adjust the audio generator for a 7 kHz left channel output at +10 dBm .
B. Refer to Figure 2-7 and adjust the left channel cutoff and peak controls to obtain a maximum left channel separation lissajous pattern as shown in Figure 2-19.
C. If a maximum left channel lissajous pattern can not be obtained, refer to Figure 2-7 and adjust the left channel delay control to close the oscilloscope display and obtain a straight-line lissajous pattern (refer to Figure 2-19).
9. Repeat the entire procedure for the right channel. Adjust the right channel level, cutoff, peak, and delay controls as required to obtain optimum separation and distortion from the right channel.
10. Repeat the entire procedure for equalization circuit 2 . Adjust the equalization circuit 2 using the equalization 2 left/right channel level, cutoff, peak, delay, controls and the equalization 2 group delay sections to obtain optimum separation and distortion.

2-154. Once the stereo adjustment is complete: 1) refer to SECTION III, OPERATION and operate the pilot switch on the stereo circuit board to ON and 2) remove the test equipment.
$2-155$. SINGLE CHANNEL LEVEL. The transmitter is equipped with a single channel level control. When the transmitter is operating in the stereo mode, the level control is designed to boost a remaining audio channel level in the event of a failure in one channel. For transmitters operating in the stereo mode, adjust the single channel level control as follows:

## $4 \begin{aligned} & \text { WARNING } \\ & \text { H }\end{aligned}$

## DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.

2-156. Operate the transmitter rear-door ac on/off control switch to OFF.
$2-157$. If an audio processor is used with the transmitter, ensure the processor is connected as follows:

1. Ensure normal program audio is connected to the processor input.
2. Ensure the audio processor output is connected to the transmitter audio input.

2-158. Operate the transmitter rear-door ac on/off control switch to ON.
2-159. Depress a desired power level switch/indicator to illuminate the switch/indicator.
$2-160$. Refer to SECTION III, OPERATION and operate the stereo circuit board mode control switch to illuminate the stereo indicator.

2-161. Disable one channel applied to the transmitter.
$2-162$. If an audio processor is used with the transmitter, refer to the audio processor manual and adjust the processor single channel limiter as described in the procedure.
$2-163$. Refer to SECTION III, OPERATION and operate the stereo circuit board mode control switch to illuminate the mono left or mono right indicator as determined by the remaining operating audio channel applied to the transmitter.

2-164. Refer to Figure 2-6 and adjust the single channel level control on the exciter circuit board as required to obtain an approximate $100 \%$ modulation indication on the modulation monitor.

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PAGE


MAXIMUM SEPARATION LISSAJOUS PATTERNS

 INCORRECT PHASE
EQUALIZATION


INCORRECT PHASE INCORRECT PHASE
EQUALI ZATION


I NCORRECT AMPLI TUDE EQUALIZATION

LEFT CHANNEL


COMBINATION


INCORRECT AMPLI TUDE EQUALI ZATION

RIGHT CHANNEL


POOR SEPARATION LISSAJOUS PATTERNS

## SECTION III OPERATION

## 3-1. INTRODUCTION.

3-2. This section identifies all controls and indicators associated with the AM-10A/AM-6A transmitters and provides standard operating procedures.

3-3. CONTROLS AND INDICATORS.
3-4. Figures 3-1, 3-2, and 3-3 present the location of all controls and indicators associated with normal operation of the AM-10A and AM-6A transmitters. Tables 3-1, 3-2, and 3-3 present the functions of each control or indicator. Refer to Figures 3-1 through 3-3 and Tables 3-1 through 3-3 for a description of the controls and indicators associated with the AM-10A/AM-6A transmitters.

TABLE 3-1. AM-10A/AM-6A CONTROLS AND INDICATORS
(Sheet 1 of 2)

| $\begin{aligned} & \text { INDEX } \\ & \text { NO. } \end{aligned}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 1 | FORWARD POWER <br> Meter | Displays the transmitter forward power output in watts as selected by the FORWARD POWER Meter LOW/HIGH/OFF switch. |
| 2 | FORWARD POWER <br> Meter HIGH/LOW/OFF Switch | Configures the FORWARD POWER meter: 1) to display forward power information on the HIGH scale, 2) to display forward power information on the LOW scale, or 3) to off. In the AM-10A: 1) the HIGH scale is from 0 W to 12 kW and 2) the LOW scale is from 0 kW to 3 kW . In the AM-6A: 1) the HIGH scale is from 0 W to 7 kW and 2) the LOW scale is from 0 kW to 1750 watts. |
| 3 | REFLECTED POWER <br> Meter | Displays the transmitter reflected power output in watts or the ac input voltage in volts as selected by the REFLECTED POWER HIGH/LOW/VAC Switch. |
| 4 | REFLECTED POWER Meter HIGH/LOW/VAC Switch | Configures the REFLECTED POWER Meter to display: 1) reflected power information on the HIGH scale, 2) reflected power information on the LOW scale, or 3) the ac input voltage. In the AM-10A: 1) the HIGH scale is from 0 to 1200 watts and 2) the LOW scale is from 0 to 300 watts. In the AM-6A: 1) the HIGH scale is from 0 to 600 watts and 2) the LOW scale is from 0 to 150 watts. |



FIGURE 3-1. AM-10A CONTROLS AND INDICATORS (SHEET 1 OF 2)


TABLE 3-1. AM-10A/AM-6A CONTROLS AND INDICATORS
(Sheet 2 of 2)

| $\begin{aligned} & \text { INDEX } \\ & \text { NO. } \end{aligned}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 5 | RF POWER MODULE | A modular plug-in assembly containing two RF power amplifier circuit boards and one modulator circuit board. The AM-10A is equipped with 10 power modules. The AM-6A is equipped with 6 power modules. Each power module is designed to output 1100 watts of RF power. |
| 6 | POWER BLOCK | An RF power amplifier assembly containing two $R F$ power modules and a combiner unit. |
| 7 | LOAD Control | Operates in association with the TUNE control to match the transmitter output impedance to the antenna. |
| 8 | TUNE Control | Operates in association with the LOAD control to match the transmitter output impedance to the antenna. |
| 9 | AC ON/OFF <br> Switch | Controls the application of ac power to the transmitter. |
| 10 | Modulation Monitor Calibration Controls | Calibrates the modulation monitor sample to power levels 1 through 5. |
| 11 | POWER SUPPLY 1-2 <br> Fault Indicator | Illuminates to indicate a failure in the 1-2 power supply. The supply provides power for RF power modules 1-2. |
| 12 | POWER SUPPLY 3-4 <br> Fault Indicator | Illuminates to indicate a failure in the 3-4 power supply. The supply provides power for RF power modules 3-4. |
| 13 | POWER SUPPLY 5-6 <br> Fault Indicator | Illuminates to indicate a failure in the 5-6 power supply. The supply provides power for RF power modules 5-6. |
| 14 | POWER SUPPLY 7-8 <br> Fault Indicator (AM-10A Only) | Illuminates to indicate a failure in the $7-8$ power supply. The supply provides power for RF power modules 7-8. |
| 15 | POWER SUPPLY 9-10 <br> Fault Indicator (AM-10A Only) | Illuminates to indicate a failure in the 9-10 power supply. The supply provides power for RF power modules 9 and 10 . |

TABLE 3-2. ECU CONTROLS AND INDICATORS (Sheet 1 of 5)


TABLE 3-2. ECU CONTROLS AND INDICATORS
(Sheet 2 of 5)

| $\begin{gathered} \text { INDEX } \\ \text { NO. } \end{gathered}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 5 | POWER CONTROL <br> Switch/Indicators | SWITCHES - A group of five switches designed to select five customer adjustable transmitter operating output power levels. |
|  |  | In the AM-10A, switches 1 and 2 can be adjusted to obtain output power levels from 50 W to 5 kW . Switches 4 and 5 can be adjusted to obtain output power levels from 3 kW to 10.8 kW . Switch 3 is designed to be customer assigned to control power in the 50 W to 5 kW range or the 3 kW to 10.8 kW range. |
|  |  | In the AM-6A, switches 1 and 2 can be adjusted to obtain output power levels from 25 W to 3 kW . Switches 4 and 5 can be adjusted to obtain output power levels from 2 kW to 6.6 kW . Switch 3 is designed to be customer assigned to control power in the 25 W to 3 kW range or the 2 kW to 6.6 kW range. |
|  |  | INDICATORS - Illuminates to indicate an associated power control switch has been selected. |
| 6 | OFF Switch/Indicator | SWITCH - Deenergizes the transmitter RF output power and configures the unit to off. |
|  |  | INDICATOR - Illuminates to indicate the OFF switch has been selected. |
| 7 | POWER $\boldsymbol{A}$ Switch/ <br> Indicator | SWITCH - Instructs the system controller to raise the transmitter output power. The switch is designed with the ability to raise power from $10 \%$ to $15 \%$ of the selected output power level. |
|  |  | INDICATOR - During manual operating conditions, illuminates to indicate the POWER $\boldsymbol{\Delta}_{\text {switch }}$ is selected. During automatic raise conditions, the indicator will illuminate to indicate the rate of automatic power increase. |
| 8 | POWER $\nabla$ Switch/ <br> Indicator | SWITCH - Instructs the system controller to lower the transmitter output power. The switch is designed with the ability to lower power from $10 \%$ to $15 \%$ of the selected output power level. |
|  |  | INDICATOR - During manual operating conditions, illuminates to indicate the POWER $\nabla_{\text {switch }}$ is selected. During automatic lower conditions, the indicator will illuminate to indicate the rate of automatic power decrease. |




TABLE 3-2. ECU CONTROLS AND INDICATORS
(Sheet 3 of 5)

| $\begin{array}{\|c} \mid \text { INDEX } \\ \text { NO. } \end{array}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 9 | RESET Switch/ <br> Indicator | SWITCH - Clears the transmitter fault circuitry when: 1) the switch is depressed and 2) if the fault condition is removed. <br> INDICATOR - Illuminates to indicate a fault has been encountered. |
| 10 | EXCITER MONITOR STEREO Indicator | Illuminates to indicate the exciter is configured to the stereo mode. |
| 11 | EXCITER MONITOR MODE Switch/ Indicator | SWITCH - Selects either left/right channel or $L-R / L+R$ information for presentation on the EXCITER MONITOR LED bar-graph display. <br> INDICATOR - Indicates the type of information selected for display on the exciter monitor. The $\mathbf{L} / \mathbf{R}$ indicator will illuminate to indicate the display of left/right channel information. The $\mathbf{L}+\mathbf{R} / \mathbf{L}-\mathbf{R}$ indicator will illuminate to indicate the display of $\mathrm{L}+\mathrm{R} /$ $\mathrm{L}-\mathrm{R}$ information. |
| 12 | EXCITER MONITOR +/- POLARITY Switch/Indicator | SWITCH - Selects either positive or negative peak audio for application to the EXCITER MONITOR LED bar-graph display. <br> INDICATOR - Indicates the signal polarity selected for display on the exciter monitor. The + indicator will illuminate to indicate the display of positive information. The - indicator will illuminate to indicate the display of negative information. |
| 13 | EXCITER MONITOR <br> LED Bar-Graph Display | Displays left, right, L+R, or L-R audio channel peak levels as selected by the EXCITER MONITOR MODE and POLARITY switches. Each indicator will illuminate at the level indicated on the display. In addition, the display is equipped with an autorange feature to allow the monitoring of signals in the $0.5 \%$ to $14.5 \%$ range. Indications of autorange operation are provided by the $\mathbf{R} / \mathbf{L}-\mathbf{R}$ and $\mathbf{L} / \mathbf{L}+\mathbf{R} \mathbf{~ X 1 0}$ indicators. |
| 14 | EXCITER MONITOR <br> MONO Indicator | Illuminates to indicate the exciter is configured to the mono L , mono R , or mono $\mathrm{L}+\mathrm{R}$ mode of operation. |
| 15 | R/L-R Display X10 Indicator | Illuminates to indicate the autorange feature is enabled to expand the $\mathbf{R} / \mathbf{L}-\mathbf{R}$ display by 10 to provide the resolution required for low level audio monitoring. |

TABLE 3-2. ECU CONTROLS AND INDICATORS
(Sheet 4 of 5)

| $\begin{aligned} & \text { INDEX } \\ & \text { NO. } \end{aligned}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 16 | L/L+R Display X10 Indicator | Illuminates to indicate the autorange feature is enabled to expand the $\mathbf{L} / \mathbf{L}+\mathbf{R}$ display by 10 to provide the resolution required for low level audio monitoring. |
| 17 | OVERTEMP Indicator | Illuminates to indicate when the transmitter operating temperature exceeds $70^{\circ} \mathrm{C}\left(158^{\circ} \mathrm{F}\right)$. |
| 18 | FOLDBACK Indicator | Illuminates to indicate when the transmitter is in a foldback condition. Foldback is when the transmitter output power is automatically reduced in response to one of the following fault conditions: 1) high reflected power, 2) high forward power, 3) high temperature, or 4) detection of a lightning potential. |
| 19 | INTERLOCK <br> Indicator | Illuminates to indicate the internal interlock, external interlock, and the remote fail-safe are closed. The remote control fail-safe must be closed only when the transmitter is configured for remote control operation. |
| 20 | REMOTE Indicator | Illuminates to indicate transmitter remote control operations are enabled. |
| 21 | CONFLICT Indicator | Illuminates to indicate an incorrect power level is selected for operation into the antenna connected to the transmitter. |
| 22 | LIGHTNING Indicator | In the AM-10A, illuminates to indicate a 2700 volt or greater potential is present at the transmitter output. In the AM-6A, illuminates to indicate a 2100 volt or greater potential is present at the transmitter output. |
| 23 | PWM Mute Indicator | Illuminates to indicate the power control PWM signal is muted in response to a fault such as lightning, an exciter fault, a reflected power emergency, an open remote control fail-safe, or an external transmitter mute. |
| 24 | Remote Fail-safe Indicator | Illuminates to indicate the remote control unit is enabled. |
| 25 | Remote/Local Switch | Controls the transmitter remote control operations. When the switch is operated to remote, remote control operations are enabled. When the switch is operated to local, remote control operations are disabled. |

TABLE 3-2. ECU CONTROLS AND INDICATORS
(Sheet 5 of 5)
(Sheet 5 of 5)

| $\begin{aligned} & \text { INDEX } \\ & \text { NO. } \end{aligned}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 26 | Battery OK Indicator | When the battery test switch is depressed, the indicator will: 1) illuminate to indicate the battery is operational or 2) not illuminate to indicate the battery is to be replaced. |
| 27 | Battery Test Switch | When depressed, evaluates the controller battery status. The status is displayed by the battery OK indicator. |
| 28 | Pilot On/Off Switch | Enables and disables the stereo pilot signal. |
| 29 | Stereo Indicator | Illuminates to indicate the exciter is configured to the stereo mode. |
| 30 | Mono L+R Indicator | Illuminates to indicate the exciter is configured to the mono L+R mode. |
| 31 | Mono Right Indicator | Illuminates to indicate the exciter is configured to the mono right mode. |
| 32 | Mono Left Indicator | Illuminates to indicate the exciter is configured to the mono left mode. |
| 33 | Exciter Mode Control Switch | Configures the exciter for stereo, mono $\mathrm{L}+\mathrm{R}$, mono left, or mono right operation. The switch is designed to configure the exciter to a different mode of operation each time the switch is depressed. The switch will advance to a mode of operation in the following order: 1) mono left, 2) mono right, 3) mono $\mathrm{L}+\mathrm{R}$, and 4) stereo. |
| 34 | Stereo Equalization 1 Indicator | Illuminates to indicate the exciter stereo equalization 1 circuit is active. |
| 35 | Stereo Equalization 2 Indicator | Illuminates to indicate the exciter stereo equalization 2 circuit is active. |
| 36 | Lock Indicator | Illuminates to indicate the exciter is locked to the programmed carrier frequency. |
| 37 | Exciter +5 V Indicator | Illuminates to indicate the ECU +5 V supply is operational. |
| 38 | Exciter +15 V Indicator | Illuminates to indicate the $\mathrm{ECU}+15 \mathrm{~V}$ supply is operational. |
| 39 | Exciter -15V Indicator | Illuminates to indicate the ECU -15 V supply is operational. |
| 40 | Negative Limiter Indicator | Illuminates to indicate the negative limiter circuit is enabled. Factory adjusted to illuminate at approximately $94 \%$ negative modulation. | ELECTRONICS INC

TABLE 3-3. POWER MODULE CONTROLS AND INDICATORS
(Sheet 1 of 2)

| $\begin{gathered} \text { INDEX } \\ \text { NO. } \end{gathered}$ | NOMENCLATURE | FUNCTION |
| :---: | :---: | :---: |
| 1 | PA 1 RF DRIVE Indicator | Illuminates to indicate RF drive is present at power amplifier 1. |
| 2 | PA 1 FAULT Indicator | Illuminates to indicate a fault has occurred in power amplifier 1. |
| 3 | PA 2 RF DRIVE Indicator | Illuminates to indicate RF drive is present at power amplifier 2. |
| 4 | PA 2 FAULT Indicator | Illuminates to indicate a fault has occurred in power amplifier 2 . |
| 5 | MOD PWM DRIVE <br> Indicator | Illuminates to indicate the exciter PWM drive is present at the modulator circuit board. |
| 6 | MOD POWER <br> Indicator | Illuminates to indicate dc power is present at the modulator circuit board. |



FIGURE 3-3. POWER MODULE CONTROLS AND INDICATORS

TABLE 3-3. POWER MODULE CONTROLS AND INDICATORS
(Sheet 2 of 2)

| INDEX <br> NO. | NOMENCLATURE | FUNCTION |
| :---: | :--- | :--- |

3-5. OPERATION.


CAUTION<br>CAUTION

> WHEN AC POWER IS APPLIED TO THE TRANSMITTER AND THE RF DRIVE AND PWM DRIVE INDICATORS ON RF POWER MODULES IN A POWER BLOCK ARE EXTINGUISHED, THE RF POWER MODULES MUST BE REMOVED FROM THE TRANSMITTER CHASSIS TO PREVENT DAMAGE TO THE MODULES.


NOTE
NOTE

## ENSURE THE TRANSMITTER IS COMPLETELY INSTALLED PRIOR TO PERFORMING THE FOLLOWING PROCEDURES.

3-6. TURN-ON.
3-7. Operate the transmitter to ON by performing the following procedure.
3-8. Ensure the transmitter rear-panel ac on/off switch is operated to ON. The ECU and RF power module front-panel indicators will illuminate.

3-9. Observe the ECU and RF power module indicators. Ensure normal operating conditions are displayed by all indicators. If an indicator displays a fault condition, operate the ac power switch to off and refer to SECTION V, MAINTENANCE to locate the problem.
$3-10$. Select an output power level by depressing the desired power level switch/indicator. The following events will occur:

1. The power level switch indicator will illuminate.
2. The transmitter flushing fans will begin operation.
3. The transmitter output power will be displayed on the FORWARD and REFLECTED power meters.

3-11. Operate the FORWARD and REFLECTED power meters to observe the transmitter forward and reflected power indications.

3-12. Adjust the transmitter output power if required by performing the POWER ADJUST procedure presented in the following text.

3-13. If remote control operation is desired, operate the local/remote switch on the controller circuit board to remote. This will enable both local and remote operation.

## 3-14. TURN OFF.

$3-15$. Operate the transmitter to OFF by depressing the OFF switch/indicator to illuminate the switch/indicator. The transmitter will operate to off.

3-16. METERING.
3-17. FORWARD POWER. The forward power meter presents forward power indications. To operate the meter, proceed as follows:

1. To monitor low forward power levels, operate the FORWARD POWER meter switch to LOW. In the AM-10A, the LOW scale is from 0 W to 3 kW . In the AM-6A, the LOW scale is from 0 W to 1750 watts.
2. To monitor high forward power levels, operate the FORWARD POWER meter switch to HIGH. In the AM-10A, the HIGH scale is from 0 W to 12 kW . In the AM-6A, the HIGH scale is from 0 W to 7 kW .
3. To configure the FORWARD POWER meter to off, operate FORWARD POWER meter switch to OFF.

3-18. REFLECTED POWER. The reflected power meter presents reflected power and ac input indications. To operate the meter, proceed as follows:

1. To monitor low reflected power levels, operate the REFLECTED POWER meter switch to LOW. In the AM-10A, the LOW scale is from 0 to 300 watts. In the AM-6A, the LOW scale is from 0 to 150 watts.
2. To monitor high reflected power levels, operate the REFLECTED POWER meter switch to HIGH. In the AM-10A, the HIGH scale is from 0 to 1200 watts. In the AM-6A, the HIGH scale is from 0 to 600 watts.
3. To monitor the ac input voltage, operate the REFLECTED POWER meter switch to VAC.

3-19. POWER ADJUST.
3-20. The POWER $\boldsymbol{\Delta}$ and $\boldsymbol{\nabla}$ switches adjust the transmitter output power. To adjust the transmitter power, proceed as follows:

1. Depress the POWER $\triangle$ switch to increase the transmitter output power. Observe the transmitter output power indications on the FORWARD and REFLECTED power meters.
The switch will increase power from $10 \%$ to $15 \%$ of the selected power level.
OR
2. Depress the POWER $\boldsymbol{\nabla}$ switch to decrease the transmitter output power. Observe the transmitter output power indications on the FORWARD and REFLECTED power meters.

The switch will decrease power from $10 \%$ to $15 \%$ of the selected power level.

## 3-21. MONO/STEREO OPERATION.

3-22. To configure the transmitter for monophonic or stereophonic operation, perform the following procedures.
3-23. STEREO OPERATION. To configure the transmitter for stereo operations, depress the exciter mode control switch to illuminate the stereo indicator on the stereo circuit board. In addition, the ECU front-panel stereo indicator will illuminate.
3-24. MONO OPERATION. The transmitter can be configured to the monophonic mode by: 1) manually selecting the desired mono mode using the stereo circuit board or 2) automatically configuring the transmitter by removing the stereo circuit board. To configure the transmitter for mono operations, proceed as follows:
3-25. Mono Operation - Stereo Circuit Board. To configure the transmitter for mono operation using the stereo circuit board, depress the exciter mode control switch to illuminate the mono $\mathrm{L}+\mathrm{R}$, mono left, or mono right indicators on the stereo circuit board. In addition, the ECU front-panel MONO indicator will illuminate.
3-26. Mono Operation - No Stereo Circuit Board. In the event of a stereo circuit board failure, the transmitter will automatically configure to the monophonic mode when the stereo circuit board is removed from the ECU. To remove the stereo circuit board and configure the transmitter for monophonic operation, proceed as follows:

CAUTION
TO PREVENT DAMAGE TO THE TRANSMITTER, ENSURE THE TRANSMITTER PRIMARY POWER IS OPER-
CAUTION ATED TO OFF BEFORE REMOVING THE STEREO CIRCUIT BOARD.

1. Operate the transmitter primary power to off.
2. Completely remove the stereo circuit board from the ECU. Do not leave the circuit board in the ECU chassis.
3. Refer to Figure 2-6 in SECTION II, INSTALLATION and ensure the monophonic audio channel select jumper is configured for the desired audio channel.
4. If required, adjust the single channel level by referring to SECTION II, INSTALLATION and performing the SINGLE CHANNEL LEVEL procedure.
3-27. PILOT CONTROL.
$3-28$. The pilot switch on the stereo circuit board controls the pilot tone. Operate the pilot switch to on to enable the pilot tone. Operate the pilot switch to off to disable the pilot tone.
$3-29$. EXCITER MONITOR OPERATION.
3-30. The following text presents procedures for specific exciter monitoring functions. Perform the appropriate procedure for the type of monitor function desired.
3-31. MONO/STEREO INDICATIONS. The MONO and STEREO indicators display the operating mode of the exciter. The MONO indicator will illuminate to indicate when the exciter is configured for mono $\mathrm{L}+\mathrm{R}$, mono left, or mono right operation. The STEREO indicator will illuminate to indicate when the exciter is configured for stereo operation.
3-32. INPUT SELECTION. Depress the $\mathbf{L} / \mathbf{R} / \mathbf{L}+\mathbf{R} / \mathbf{L}-\mathbf{R}$ MODE switch/indicator to: 1) illuminate the $\mathbf{L} / \mathbf{R}$ indicator to select left and right channel information or 2) illuminate the $\mathbf{L}+\mathbf{R} / \mathbf{L}-\mathbf{R}$ indicator to select $\mathbf{L}+\mathbf{R}$ and $\mathbf{L}-\mathbf{R}$ information. The selected parameter will appear on the EXCITER MONITOR display.
3-33. POLARITY SELECTION. Depress the POLARITY switch/indicator to: 1) illuminate the + indicator to select positive peak audio or 2) illuminate the - indicator to select negative peak audio. The selected parameter will appear on the EXCITER MONITOR display.

3-34. X10 AUTORANGE INDICATIONS. The EXCITER MONITOR display is designed with an autorange function to provide the appropriate resolution for the applied signal level. The $\mathbf{L} / \mathbf{L}+\mathbf{R}$ display $\mathbf{X 1 0}$ indicator will illuminate to indicate the display is expanded by 10 . The $\mathbf{R} / \mathbf{L}-\mathbf{R}$ display $\mathbf{X 1 0}$ indicator will illuminate to indicate the display is expanded by 10 .

## 3-35. FAULT RESET.

3-36. The transmitter monitors several parameters for fault conditions. The RESET indicator will illuminate to indicate a fault when one of the following conditions occur:

1) over-temperature, 2) exciter fault, 3) power supply fault, 4) RF power module fault, 5) high reflected/forward power, 6) reflected power emergency, or 7) lightning. Once the fault condition is removed, the fault circuitry must be reset. If a power supply fault is encountered, the transmitter AC power must be disconnected to remove the fault condition (refer to POWER SUPPLY FAULT RESET in the following text). To reset the fault circuitry, depress the RESET switch. The fault circuitry will be reset.

3-37. POWER SUPPLY FAULT RESET.
$3-38$. If a power supply fault is encountered, ac power must be disconnected from the transmitter to clear the fault. To reset a power supply fault, proceed as follows:

1. Operate the rear-door ac ON/OFF switch to off.
2. Operate the rear-door ac on/off switch to on.
3. Depress the RESET switch.

3-39. OVER-CYCLE OFF.
$3-40$. The transmitter controller is equipped with an on/off cycle counter circuit. The circuit is designed to monitor transmitter on/off cycles. If the transmitter is operated on/off seven times within 15 seconds, the transmitter will automatically operate to OFF. The power level or OFF switch/indicators will not respond. To operate the transmitter to ON, proceed as follows:

1. Do not depress any power level switch/indicators or the OFF switch/indicator for approximately 30 seconds. This allows the circuit to reset.
2. Depress the desired power level switch/indicator.

3-41. OVER-MODULATION PWM MUTE.
3-42. The transmitter is protected from modulation levels above $150 \%$ by an over-modulation circuit. If the transmitter modulation increases to a level above $150 \%$, the PWM signal will be muted. This will mute the output power and prevent damage to the transmitter power supply modules.

## $3-43$. TRANSMITTER MONITOR.

3-44. The TRANSMITTER MONITOR is designed to present the operating status of: 1) the exciter, 2) the RF power modules, 3) the power supply, 4) the antenna, 5) the remote control, 6) antenna conflict conditions, 7) lightning conditions, 8) interlocks, 9) foldback conditions, and 10) over-temperature conditions. Use the information presented in Table 3-2 to determine the status of the transmitter components and operating conditions.

3-45. BATTERY TEST.
$3-46$. The battery test and battery OK indicator check the ECU battery backup system. To check the ECU battery, depress the battery test switch. The battery OK indicator will illuminate to indicate an acceptable battery voltage. If the battery OK indicator does not illuminate, replace the battery.


## 3-47. CONTROLLER PWM MUTE INDICATOR.

3-48. The PWM mute indicator illuminates to indicate when the power control PWM signal is muted. The power control PWM signal is muted during: 1) lightning conditions, 2) an exciter fault, 3) reflected power emergency conditions, 4) an open remote control fail-safe, or 5) a transmitter mute control signal.

3-49. CONTROLLER REMOTE FAIL-SAFE INDICATOR.
$3-50$. The controller remote fail-safe indicator illuminates to indicate the remote control unit is enabled. The indicator will extinguish when the remote control unit is disabled.

3-51. EXCITER LOCK INDICATOR.
$3-52$. The exciter circuit board lock indicator illuminates to indicate when the exciter is locked to the programmed carrier frequency. The indicator will extinguish when the exciter is unlocked from the programmed carrier frequency.

3-53. EXCITER +5V/+15V/-15V INDICATORS.
$3-54$. The exciter circuit board $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V indicators display the status of the operating potentials from the ECU power supply. The $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V indicators will illuminate to indicate the +5 volt, +15 volt, and -15 supplies are operational.

## $3-55$. STEREO EQUALIZATION INDICATORS.

$3-56$. The stereo circuit board equalization 1 indicator illuminates to indicate when equalization circuit 1 is selected. The stereo circuit board equalization 2 indicator illuminates to indicate when equalization circuit 2 is selected.

## $3-57$. RF POWER MODULE INDICATORS.

3-58. The RF power module indicators are designed to present the operating status of the power amplifier circuit boards and the modulator circuit board. Use the information presented in Table 3-3 to determine the status of the power amplifier circuit boards and the modulator circuit board.

3-59. POWER SUPPLY INDICATORS.
3-60. The power supply indicators on the transmitter lower front-panel are designed to present the operating status of the power supply circuit boards. AM-10A transmitters are equipped with power supply $1-2,3-4,5-6,7-8$, and $9-10$. AM-6A transmitters are equipped with power supply $1-2,3-4$, and $5-6$. The indicators illuminate to indicate a failure in a power supply.

3-61. EXCITER NEGATIVE LIMITER INDICATOR.
3-62. The exciter circuit board negative limiter indicator displays the status of the exciter negative limiter circuit. The indicator will illuminate to indicate the negative limiter circuit is enabled. The indicator is factory adjusted to illuminate at approximately $94 \%$ negative modulation.

3-63. HIGH AC LINE CONDITIONS.
3-64. The transmitter is equipped with a feature to mute the transmitter output power in the event the ac power line increases above 270 volts. If this occurs: 1 ) the transmitter output power will be muted and 2) no fault or emergency condition will be generated by the transmitter. The transmitter will unmute when the high ac line condition is removed.

# SECTION IV THEORY OF OPERATION 

## 4-1. INTRODUCTION.

$4-2$. This section presents the theory of operation for the Broadcast Electronics AM-10A/AM-6A transmitters.
$4-3$. The following text presents the AM-10A/AM-6A transmitter overall theory of operation. The transmitter is divided into modular components for the discussion. The modular components consist of the: 1) exciter/control unit (ECU), 2) output network, 3) RF power module, 4) RF combiner, and 5) power supply. The ECU, RF power module, and power supply are presented in further detail by the publication sections at the end of this manual.

4-4. Figures 4-1 and 4-2 present the AM-10A and AM-6A block diagrams. Figure 4-1 presents the AM-10A block diagram. Refer to Figure 4-1 and the AM-10A overall schematic diagram in SECTION VII as required for the following discussion. Figure 4-2 presents the AM-6A block diagram. Refer to Figure 4-2 and the AM-6A overall schematic diagram in SECTION VII as required for the following discussion.

## 4-5. FUNCTIONAL DESCRIPTION.

## 4-6. ECU.

4-7. GENERAL. The transmitter ECU (exciter/control unit) is a modular assembly containing plug-in stereo, exciter, controller, and extender circuit board assemblies. A forward power meter is provided to monitor the transmitter forward output power. A reflected power/primary ac power meter provides reflected power and primary ac voltage indications. The ECU switch and display circuitry is contained on switch and display circuit boards. Power for the ECU is provided by a modular switching power supply unit.
4-8. STEREO CIRCUIT BOARD. The ECU stereo circuit board consists of C-QUAM AM stereo circuitry. C-QUAM AM stereo is a mode of AM stereo transmission utilizing amplitude modulated ( $\mathrm{L}+\mathrm{R}$ ) information and independently quadrature modulated stereo (L-R) information. The results produce a stereo transmission system compatible with mono receivers.

4-9. The stereo circuit board is equipped with four modes of operation: 1) mono left, 2) mono right, 3) mono L+R, and 4) stereo. Configuring the circuit board to monophonic operation is accomplished by: 1) operating the circuit board to the mono left, mono right, or mono $\mathrm{L}+\mathrm{R}$ mode or 2 ) removing the stereo circuit board. The circuit board is equipped with two equalization circuits. The circuits allow the transmitter to be configured for two different antenna patterns such as for a day pattern and a night pattern.

4-10. The stereo circuit board operates in association with the ECU exciter circuit board to provide RF drive to the RF power modules. The stereo circuit board receives left and right channel audio and an unmodulated TTL level RF signal at 4 times the carrier frequency from the exciter circuit board. The stereo circuit board outputs a TTL level RF signal to the exciter circuit board.
4-11. EXCITER CIRCUIT BOARD. The ECU exciter circuit board is a modular plug-in exciter assembly. The circuit board operates in association with the stereo circuit board to produce a C-QUAM AM stereo RF output. Instrumentation amplifiers provide balanced left and right channel transformerless audio inputs.

4-12. The exciter circuit board generates: 1) a PWM (pulse-width-modulation) signal and 2) an RF carrier frequency signal. The 122 kHz to 135 kHz PWM signal is routed for application to the modulator circuit boards in the RF power modules. The RF carrier frequency signal is applied to the power amplifier circuit boards in the RF power modules. The exciter carrier frequency is established by a digital frequency synthesizer. The synthesizer is a phase-locked-loop circuit which provides extremely accurate and reliable carrier frequency operation.

4-13. CONTROLLER CIRCUIT BOARD. All transmitter control operations are directed by the ECU controller circuit board. The controller circuit board is designed with CMOS control and monitoring circuitry.
4-14. The controller circuit board is designed with two interlock circuits. A transmitter external interlock is provided such as for a test load. An antenna interlock circuit is provided to prevent the transmitter from operating into an incorrect antenna.
4-15. The transmitter power is controlled by a power control circuit. The circuit allows the transmitter to be operated at five power levels. A power trim circuit allows the transmitter power to be increased or decreased as required. A high reflected power detection circuit, a high forward power detection circuit, and a high temperature detection circuit operate in association with the power control circuit to foldback the transmitter power during high reflected power, high forward power, and high temperature conditions. In addition, a lightning detector circuit is provided to mute the transmitter when lightning is present at the antenna.

4-16. Several monitoring and display circuits provide information on transmitter operating conditions. An RF power module status circuit displays: 1) if a module is removed for maintenance or 2 ) if a power module fault has occurred. A power supply status circuit displays: 1) if a power supply circuit board is removed for maintenance or 2 ) if a power supply fault has occurred. An exciter status circuit indicates if a fault has occurred in the exciter. An antenna status circuit displays: 1) $1.2: 1$ VSWR conditions, 2) high reflected power conditions, and 3 ) emergency reflected power conditions.
4-17. Additional display circuits include: 1) remote, 2) conflict, 3) lightning, 4) interlock, 5) over-temperature, and 6) reset. A remote indicator displays the status of the remote control system. A conflict indicator illuminates to indicate an incorrect power level is selected for operation into an antenna. A lightning indicator illuminates to indicate the presence of lightning at the transmitter output. An interlock indicator displays the status of the internal and external interlock. An over-temperature indicator illuminates to indicate a transmitter temperature greater than 70 degrees C. A reset indicator illuminates to indicate a transmitter fault has occurred. Transmitter faults include: 1) exciter failure, 2) power supply failure, 3) RF power module failure, 4) high reflected power conditions, 5) reflected power emergency conditions, 6) over-temperature conditions, 7) lightning conditions, and 8) 1.2:1 VSWR conditions.

4-18. POWER SUPPLY. DC operating potentials for the ECU assembly is provided by a modular switching power supply unit. The unit provides $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V dc operating potentials for the ECU circuit boards. $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V indicators are provided on the exciter circuit board.

4-19. RF POWER MODULE.
4-20. An RF power module is a plug-in assembly containing two RF amplifier circuit boards and a modulator circuit board. Each RF power module is designed to produce 1100 watts of RF power. Two RF power modules are contained in a power block. The AM-10A transmitter is equipped with 5 power blocks. The AM-6A transmitter is equipped with 3 power blocks.

4-21. The modular design of the RF power modules allow the modules to be removed from the transmitter for maintenance. The remaining power modules will provide power to maintain on-air operation.
$4-22$. The PWM signal from the exciter circuit board is applied to the modulator circuit board. The modulator circuit board is designed to amplify and convert the PWM signal to a dc voltage which varies at an audio rate. The output of the modulator circuit board is applied to the RF amplifier circuit boards. Four indicator circuits monitor and display the status of the: 1) PWM drive signal, 2) B+ dc supply, 3) modulator fault conditions, and 4) blown fuse conditions.

4-23. The RF amplifier circuit boards are designed with Class E amplifier technology and MOSFET power transistors. The circuit board operates from: 1) the varying dc voltage from the modulator circuit board and 2) the RF drive signal from the exciter circuit board. The RF drive signal from the exciter circuit board and the varying dc voltage from the modulator are applied to a push-pull power MOSFET transistor amplifier circuit. The amplifier circuit is designed to output approximately 550 watts of RF power. A fault detection circuit monitors amplifier operation for fault conditions.

4-24. RF COMBINER.
4-25. Power from each RF amplifier circuit board is applied to a star combiner network. The combiner components are located on the rear panel of each power block. The star combiner network consists of individual transformer and inductor networks for each amplifier circuit board. The combiner accepts RF power from each RF power module to produce the rated RF output power.
$4-26$. In addition to combining the RF power from the RF power modules, the combiner design allows one or more RF power modules to be removed from the transmitter for maintenance. The remaining RF power modules will continue to operate to maintain on-air operation. This is accomplished without the use of dummy modules or bypass switches.

## 4-27. OUTPUT NETWORK.

4-28. The output network is a modular assembly designed to match the transmitter impedance to the antenna. The assembly consists of a: 1) bandpass filter, 2) directional coupler circuit board, 3) T-matching network, 4) lightning protection circuit board, and 5) a lightning detection circuit board.

4-29. The bandpass filter is an eight element LC filter designed to attenuate all harmonic frequencies to FCC, DOC, and CCIR levels. The directional coupler circuit board consists of a circuit designed to sample the transmitter RF output. The circuit board generates both forward and reflected power samples for application to the controller circuit board. The "T" matching network consists of an LC network. The network is designed to match the transmitter impedance to the antenna.

4-30. A lightning protection circuit board is provided to protect the transmitter circuitry from direct lightning potentials. The circuit protects the transmitter by shunting lightning potentials to ground. The lightning detector circuit board is designed to mute the transmitter RF output during the presence of a lightning potential. The lightning detector circuit board is controlled by a spark gap. The circuit will respond to potentials of 2700 volts in AM-10A models and 2100 volts in AM-6A models. This prevents the transmitter from muting during near-by lightning activity.



## 4-31. POWER SUPPLY.

4-32. The transmitter operates from a three phase power source of 196 to 252 volts ac $50 / 60 \mathrm{~Hz}$ or 339 to 437 volts ac $50 / 60 \mathrm{~Hz}$. The transmitter can also operate from a single phase power source of 196 to 252 volts ac $50 / 60 \mathrm{~Hz}$ using a single phase power supply option. A rear-door ac on/off circuit breaker provides: 1) ac power control, 2) disconnects all ac power to the transmitter when the door is opened, and 3) protects the transmitter from over-current conditions.

4-33. The ac line voltage is sampled at the ac sample circuit board. The sample circuit board provides an ac line voltage sample for application to the meter switch circuit board. A three-pole low-pass filter is provided to prevent the coupling of EMI into the power supply circuitry.

4-34. POWER SUPPLY CIRCUIT BOARD. DC operating potentials for the RF power modules are provided by power supply circuit boards. One power supply circuit board provides dc operating potentials for one power block. The AM-10A transmitter is equipped with 5 power supply circuit boards. The AM-6A transmitter is equipped with 3 power supply circuit boards.

4-35. The power supply circuit board consists of a: 1) switching power supply circuit, 2) conventional bridge rectifier circuit, 3) fault detection circuit. The switching power supply circuit operates directly from the ac power source. No primary ac power transformer is included in the circuit. An SCR controlled bridge rectifier circuit and a switching regulator circuit converts ac potentials to dc potentials at a desired voltage. Control of the dc output voltage is provided by a power control PWM signal from the controller.

4-36. A transformer with five secondary windings provide low-voltage ac potentials to five full-wave bridge rectifiers circuits. The circuits provide dc operating potentials for the power supply circuit board and RF power module circuitry.

4-37. The power supply design provides the RF power modules with a constant and stable dc operating supply by not responding to fluctuations or surges in the ac line voltage. The supply will produce a constant dc voltage during high/low ac line voltage or surge conditions.

4-38. The switching power supply output voltage is controlled by a power control PWM signal from the controller circuit board. Current reduction at turn-on is controlled by a soft-start circuit. The circuit is designed to generate start pulses synchronized to the ac line phase to slowly bias the SCR bridge rectifier circuit on during initial turn-on operations. The switching regulator circuitry is monitored for proper operation by an overvoltage and loss-of-PWM signal circuitry. The switching regulator operation is performed by IGBT (insulated-gate-bi-polar-transistors) transistors. The IGBTs are designed to provide extremely reliable and efficient operation.

4-39. METERING.
4-40. The transmitter metering consists of the forward power meter, reflected power/primary ac input voltage meter, and the exciter modulation meter. Forward power information is presented on the forward power meter. Reflected power/primary ac input voltage information is presented on the reflected power/primary ac input voltage meter. The meters are controlled by three-position switches. Forward and reflected power samples for the metering circuitry are provided by the directional coupler circuit board. An ac sample for the reflected power/primary ac input voltage meter is provided by an ac sample circuit board.

4-41. Monitoring of exciter operations is provided by the exciter modulation monitor. Two 30 segment multi-color bar graph displays present $L / L+R$ and $R / L-R$ information. A X10 mode allows the monitoring of low level signals such as the pilot tone.

## 4-42. COOLING FANS.

4-43. The AM-10A transmitter is equipped with 5 cooling fans. The AM-6A transmitter is equipped with 3 cooling fans. The fans are controlled by an optically-coupled-relay. In the AM-10A, the fans provide 1200 CFM of cooling air for the transmitter. In the AM-6A, the fans provide 720 CFM of cooling air for the transmitter. A temperature sensor circuit board monitors the transmitter air temperature and provides status information to the controller.

## 4-44. INTERFACE CIRCUIT BOARD.

4-45. Communication between the controller, RF power modules, and the power supply circuit boards is provided by an interface circuit board. The circuit board: 1) routes status information from the RF power modules and power supply circuit boards to the controller and 2) routes control signals from the controller to the RF power modules and the power supply circuit boards.
4-46. DETAILED DESCRIPTION.
4-47. POWER SUPPLIES.
4-48. The AM-10A/AM-6A transmitter requires: 1) a 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ delta/wye three phase power source, 2) a 339 V to 437 V ac $50 / 60 \mathrm{~Hz}$ wye three phase power source, or 3) a 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ single phase power source (refer to Figure 4-3). The following text presents the ac power source requirements.

| AM-10A |  |
| :--- | :--- |
| POWER SUPPLY | AC POWER SOURCE |
| Three Phase | Delta/Wye 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ or Wye 339 V to 437 V <br> ac $50 / 60 \mathrm{~Hz}$ three phase at 150 Amperes. <br> Single Phase 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ single phase at 225 Amperes. |


| AM-6A |  |
| :--- | :--- |
| POWER SUPPLY | AC POWER SOURCE |
| Three Phase | Delta/Wye 196V to 252V ac 50/60 Hz or Wye 339V to 437 V <br> ac $50 / 60 \mathrm{~Hz}$ three phase at 75 Amperes. |
| Single Phase | 196 V to 252 V ac $50 / 60 \mathrm{~Hz}$ single phase at 125 Amperes. |

4-49. AC INPUT CIRCUITRY.
$4-50$. When the transmitter fused disconnect is closed, ac power is routed to rear-door ac input switch CB1. CB1 is the transmitter primary ac power safety device and overload protection. CB1 disconnects primary ac power when the transmitter rear door is opened. Metal-Oxide-Varistors MOV1, MOV2, and MOV3 protect the transmitter power supply circuitry from ac line voltage surge potentials. AC power from the MOVs is applied to the following circuits: 1) the ECU power supply assembly, 2) the transmitter flushing fans, 3) low voltage power supply transformer T1, 4) the power supply circuit board, and 5) the ac sample circuit board.

4-51. ECU POWER SUPPLY ASSEMBLY.
$4-52$. The ECU power supply is a 40 W modular switching power supply unit. The power supply assembly provides regulated $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V operating potentials for the ECU circuit boards.

4-53. The power supply for the ECU controller circuit board is backed-up by a 9 V battery. During an ac power failure, the battery will maintain the transmitter operating configuration stored in the controller logic circuitry. Once power is returned to the transmitter, the transmitter will automatically resume operation in the configuration appearing prior to the ac failure. If an extended ac power failure occurs, the transmitter will be operated to off by an ac loss/auto shutdown circuit.
$4-54$. The battery back-up system requires a standard 9 V battery. The battery will maintain the controller logic for several months. Replace the battery approximately once a year to ensure proper transmitter operation during ac power failure conditions.
4-55. TRANSMITTER FLUSHING FANS.
$4-56$. Cooling air for the transmitter circuitry is provided by flushing fans B1 through B5 in AM-10A models and B1 through B3 in AM-6A models. Control of the fans is provided by optically-coupled-relay (OCR) K1.
$4-57$. The flushing fans are controlled by a signal from the ECU controller circuit board. When a power level switch/indicator is depressed, the controller circuit board will enable optically-coupled relay (OCR) K1 to energize the fans. The fans will operate during transmitter operation.

4-58. LOW-VOLTAGE POWER SUPPLY TRANSFORMER.
4-59. Low-voltage operating potentials for the transmitter power supply circuit board and RF power modules are provided by ac power transformer T1. Transformer T1 consists of: 1 ) one primary winding and 2) five secondary windings. The secondary windings provide low-voltage ac potentials for application to five rectifier circuits on the power supply circuit board. The circuitry provides dc operating potentials for the power supply and the RF power modules.
4-60. POWER SUPPLY CIRCUIT BOARD.
4-61. Low and high voltage dc operating potentials for the RF power modules are provided by the power supply circuit board. The AM-10A is equipped with 5 power supply circuit boards. The AM-6A is equipped with 3 power supply circuit boards. Each power supply circuit board provides dc operating potentials for two RF power modules.
4-62. The power supply circuit board is equipped with: 1) a switching power supply circuit designed to produce high-voltage operating potentials and 2) conventional rectifier circuitry designed to produce low-voltage operating potentials. The following text describes the circuitry.
4-63. CONVENTIONAL RECTIFIER CIRCUITRY. +30 V and +20 V dc operating potentials for the RF power modules are provided by four conventional rectifier circuits. AC power from a winding of ac power transformer T1 is applied to bridge rectifier D9. D9 rectifies the ac potential into an unregulated +20 volt ac supply for application to: 1) the modulator circuit board and 2) to regulator U 3 . U 3 is a +15 volt dc regulator. The output of U 3 routed for application to the components on the power supply circuit board.
4-64. AC power from a second winding of transformer T1 is applied to bridge rectifier D10. D10 rectifies the ac potential into an unregulated +20 V dc supply for application to the RF power module power amplifier circuit boards. AC power from a third winding of power transformer T1 is applied to bridge rectifier D11. D11 rectifies the ac potential into an unregulated +30 V dc supply for application to the RF power module power amplifier circuit boards. AC power from a fourth winding of power transformer T1 is applied to bridge rectifier D12. D12 rectifies the ac potential into an unregulated +15 V dc supply for application to: 1) the power supply circuit board and 2) regulator U 4 . U 4 is a +12 volt de regulator. The output of U4 routed for application to the components on the power supply circuit board.


4-65. An ac sample from a winding of T 1 is also routed to a soft-start circuit. The soft-start circuit is designed to generate control pulses synchronized with the ac line phase. A complete description of the soft-start circuit is presented in Rectifier/Soft-Start Circuit (refer to the following text).

4-66. SWITCHING POWER SUPPLY CIRCUIT. AC power from fuses F1 and F2 is applied to ac line filter FL1. FL1 is a modular line filter designed to protect the circuitry from EMI. The ac from filter FL1 is applied to fuses F1 and F2 on the power supply circuit board. The fuses protects the power supply circuitry from overload conditions. Metal-Oxide-Varistor MOV1 prevents damage to the switching power supply circuit from ac line voltage surge potentials.

4-67. Rectifier/Soft-Start Circuit. The ac line is full-wave rectified by an isolated SCR controlled bridge rectifier circuit. The SCR bridge rectifier consists of diodes D15 through D17 and SCRs D13 and D14. The rectifier is controlled by a soft-start circuit. The soft-start circuit is designed to: 1) determine when the ac line waveform crosses the 0 volt axis and 2) generate short duration pulses in synchronization with the ac line 0 volt crossings. The pulses are amplified and applied to the gates of the rectifier circuit SCR components to slowly bias the components on during initial start operations. This operation eliminates the component stress at power-on by limiting the supply in-rush current. The rectifier will output an unregulated and unfiltered dc supply at approximately 300 V to an inductor and capacitor filter network.

4-68. The output of the rectifier circuit is applied to an LC filter consisting of: 1) inductor L1 and 2) capacitors C24 through C27. The output of the LC filter generates a 300 V main operating supply for the RF power modules. The positive leg of the dc supply is the common for the dc voltages contained in the switching regulator circuitry and the RF power modules. The negative leg of the supply is regulated and controlled to generate the required operating potentials for the RF power modules.

4-69. Switching Regulator Circuit. The main operating supply is regulated by a buck-type switching regulator circuit. The switching regulator circuit generates the negative leg of the B supply. The regulator circuit consists of: 1) a power supply mute circuit, 2) a switching regulator power control PWM circuit, 3) optical coupler U17 4) inverting buffer U19, and 5) switching regulator transistors Q21 and Q22.

4-70. A dc operating supply for optical coupler U17 and buffer U19 is generated by bridge rectifier D25. D25 full-wave rectifies an ac potential from ac transformer T1 into an unregulated +20 V supply. The supply is applied to +18 V regulator U16. U16 outputs a +18 V supply which is further regulated to a 5 V operating potential by a resistive divider and a zener diode. The 5V supply is applied to optical couplers U17 and buffer U19.

4-71. Control of the regulator circuit is provided by the switching regulator power control PWM circuit, a current sampling circuit, and a voltage and current feedback correction circuit. Together, the circuits function in a closed-loop to control regulator operation. The switching regulator power control PWM circuit is designed to produce two out-of-phase square wave signals with varying duty cycles. The duty cycle is varied in response to the signal from the correction circuit. The output of the control circuit is applied to optical coupler U17. U17 provides isolation between two different ground circuits. The output of the coupler is applied to gate drive inverting buffer U19. The output of U19 is applied to the gates of IGBT switching regulator transistors Q21 and Q22. Q21 and Q22 are operated to on for a specific time duration to regulate the output voltage for varying load conditions.

4-72. The regulator circuit output voltage is directed by a 1 kHz power control PWM signal from the controller. The signal is applied to the correction circuit on the power supply circuit board. In addition to the 1 kHz PWM signal, a voltage and current sample from the regulator output is routed to the voltage and current feedback correction circuit. The correction circuit responds by evaluating the output samples and the power control signal and generating a correction voltage. The voltage is applied to the switching regulator power control PWM circuit to adjust the output of the regulator.

4-73. The output of the transistor switching regulator circuit is applied to filter inductor L2. Protection of the transistors from switching transients during turn on/off operation is provided by clamp diode D32. Clamp diode D32 protects the transistors by limiting positive peak voltages. The output of the regulator circuit is applied to circuitry on RF power module modulator circuit boards.

## 4-74. MODULATOR CIRCUIT BOARD.

4-75. The B- leg from the power supply circuit board is routed to circuitry on the RF power module modulator circuit board. The B- leg is applied to relay K1 on the modulator circuit board. K1 is controlled by a fault detector circuit. The relay is designed to immediately remove the supply from the forward converter circuit during a fault condition. The output of the relay is applied to the converter circuit.
4-76. Transistors Q1 and Q2 are the switching devices in the forward converter circuit. The circuit is controlled by the audio PWM signal from the driver circuit board. The circuit operates by switching the applied B- leg at a 122 kHz to 135 kHz rate. The duty cycle of the PWM signal is $40 \%$ with no modulation. The output of the forward converter circuit is applied to an LC PWM low-pass filter network. Protection of the transistors from switching transients is provided by clamp diodes D2 and D3. D2 and D3 limit the positive peak transients appearing on the output.

4-77. A sample of the modulator circuit output is routed to a fault detector circuit. The circuit will respond to a fault by: 1) routing a control signal to relay K1 to disconnect the amplifier circuit from the B- supply and 2 ) route a control signal to the power supply circuit board to momentarily mute the power supply. After a short delay, a control signal is routed to the power supply to enable the supply to provide power to RF module 2.

4-78. The $\mathrm{B}+$ leg of the supply is also routed to the modulator circuit board. The $\mathrm{B}+\mathrm{leg}$ is applied to fuse F1 and is the common for the dc voltages contained in the power supply circuit board switching regulator circuit and the RF power modules. F1 is provided to protect clamp diodes D2 and D3 from overcurrent conditions.

4-79. POWER AMPLIFIER CIRCUIT BOARDS.
4-80. The power amplifier circuit board circuitry is configured in a Class E switching amplifier design. A Class E design is recognized by: 1) the application of the B+ power supply through an RF choke to combining transformers and 2) the use of only two MOSFET power transistors in a push-pull configuration per amplifier. The circuitry on each amplifier circuit board is identical, therefore only amplifier circuit board 1 will be discussed.
$4-81$. The dc voltage output of the modulator circuit board is routed to the power amplifier 1 circuitry through fuse F1. F1 protects the amplifier circuitry from over-current conditions. The supply is applied to a switching amplifier circuit consisting of transistors Q1 and Q2. The B+ leg of the main dc supply from the power supply circuit board is applied to Q1 and Q2 through choke L4 to a primary center tap of combiner transformer T4. RF choke L4: 1) prevents RF signals from entering the de supply and 2) functions as the last series inductor for the PWM low-pass filter on the modulator circuit board.

4-82. The amplifier circuit is driven by the RF drive signal from the exciter circuit board. The RF drive signal consists of a square-wave signal at the carrier frequency. The signal is amplified prior to application to Q1 and Q2 by a driver circuit.
4-83. The amplifier circuit functions by switching the dc voltage from the modulator circuit board at an RF rate to produce a monophonic or a C-QUAM AM stereo signal at the programmed carrier frequency. The signal appears at the primary of combiner transformer T4. The RF signal is transferred to the secondary of T4 and routed to power amplifier 2 circuit board combiner transformer T3. The RF output signal from T4 is combined with the RF output signal from transformer T3 to generate a C-QUAM signal at approximately 1100 watts of carrier.

## 4-84. SEQUENCE OF OPERATION.

4-85. When transmitter circuit breaker CB1 is closed, ac power is routed to: 1 ) the ECU power supply, 2) fan control relay K1, 3) low-voltage ac power transformer T1, 4) the power supply circuit board, and 5) the ac sample circuit board. In response to the application of ac power with no error conditions, the following controller and RF power module indicators will illuminate green:

## CONTROLLER INDICATORS

1. Exciter
2. Power Modules
3. Power Supply
4. Antenna
5. Mono or Stereo (depending on exciter mode of operation)
6. Exciter Circuit Board: 1) $+15 \mathrm{~V}, 2$ ) -15 V
3) Lock, and 4) +5 V
7. Stereo Circuit Board: 1) Mono L+R/Stereo/

Mono L/Mono R (depending on exciter mode
of operation), 2) Equalization 1 or Equalization 2
(depending on antenna configuration)
4-86. A start sequence is initiated when a power level switch/indicator is depressed. Logic from the controller will enable optically-coupled-relay K 1 to enable the flushing fans.
4-87. Logic from the controller will also enable the SCR controlled bridge rectifier circuit on the power supply circuit board. The B+ dc potential from the rectifier is applied to the inductor and capacitor filter networks on the power supply panel. Generation of the Bleg is provided by the IGBT switching regulator circuit.
4-88. Power output of the regulator is controlled by the PWM signal from the controller. The regulator will increase or decrease power as determined by the PWM signal. The output of the regulator is routed to the modulator circuit board. The modulator POWER indicator will illuminate if the $B+$ supply from the power supply circuit board is present. The modulated output from the modulator circuit board is routed to the power amplifier 1 and power amplifier 2 circuit board for amplification.
4-89. RF CIRCUITRY.
4-90. EXCITER CIRCUIT BOARD. Audio for application to the AM-10A/AM-6A transmitter is applied to the exciter circuit board (refer to Figure 4-4). The exciter circuit board is designed to: 1) process left/right channel or monaural audio to generate a Pulse-Width-Modulated (PWM) signal at 122 kHz to 135 kHz and 2) generate an RF signal using a frequency synthesizer, a phase modulator for IPM correction, and an RF driver network.


597-1113-18
FIGURE 4-4. AM-10A/AM-6A RF CIRCUITRY SIMPLIFIED SCHEMATIC (SHEET 1 OF 2)


597-1113-18A
FIGURE 4-4. AM-10AAM-6A RF CIRCUITRY

4-91. Left channel audio is applied to an RFI filter and a defeatable 10 Hz high-pass filter. The 10 Hz high-pass filter is provided to remove low frequency residual products from specific audio processing units. Balanced-to-unbalanced signal conversion is provided by an instrumentation amplifier. The output of the instrumentation amplifier is applied to a defeatable high frequency boost circuit. The high frequency boost circuit is provided to increase high frequency response to compensate for a Bessel filter in the PWM modulator. The output of the high frequency boost circuit is applied to an active PWM filter/equalizer and a mode switching circuit. The output of the PWM filter is routed for application to the stereo circuit board.
4-92. The mode switching circuit is designed to select the left or right channel for mono left or mono right operation. A summing amplifier is provided as a mono support circuit to increase the gain of the circuit 6 dB during mono operations. The output of the summing amplifier is applied to a 24 uS delay and limiter circuit. The delay circuit is provided for stereo equalization. The negative limiter is provided to limit negative modulation from $90 \%$ to $100 \%$.

4-93. The output of the 24 uS delay and negative limiter is applied to: 1 ) a PWM circuit and 2) an IPM comparator and corrector circuit. The PWM circuit is designed to output a square wave signal in which the duty cycle changes in response to the applied audio level. The output of the PWM circuit is applied to a PWM driver circuit. The PWM driver circuit consists of parallel transistor drivers to lower the impedance and improve reliability.
4-94. The transmitter carrier frequency is generated by digitally programmed frequency synthesizer circuit. The frequency synthesizer is designed to output: 1) the carrier frequency to a mono/stereo select circuit, 2) a FcX4 (carrier frequency times four) signal for application to the stereo circuit board, and 3) a 25 Hz pilot signal for application to the stereo circuit board. A mono/stereo select circuit functions as an automatic mono/stereo select switch. If a stereo signal from the internal stereo circuit board or an external stereo generator is present, the exciter will be configured for stereo operation. If the stereo signal is not present, the circuit will configure the exciter for mono operation. The output of the mono/stereo select circuit is applied to the IPM (Incidental Phase Modulation) signal generator and modulator. The IPM signal generator is designed to produce a waveform similar to the signal produced by the RF amplifier circuitry. The IPM generator signal is out-of-phase with the signal generated by the RF power modules. The signal is applied to a modulator circuit which will generate a phase compensated RF signal at the carrier frequency. The phase compensation will effectively cancel the IPM generated in the RF circuitry.
4-95. The output of the IPM circuitry is applied to an RF driver network. The network consists of a high/low side driver and output drive transistors.
4-96. STEREO CIRCUIT BOARD. Left/right channel audio and an RF signal at FcX4 (carrier frequency times four) from the exciter circuit board is applied to the stereo circuit board. The stereo circuit board is designed to generate a TTL level RF signal. The circuit board contains identical left/right channel and equalization $1 / 2$ circuitry. Therefore, only the left channel equalization 1 circuit will be discussed.
$4-97$. Left channel audio from the exciter circuit board is applied to the left channel equalization 1 circuit. The equalization circuit consists of 1) a state variable low-pass filter, 2) an 8 uS group delay section, and 3) a 4 uS group delay section. The circuit is designed to equalize frequencies to produce maximum separation.
$4-98$. The output of each equalization circuit is routed to an equalization and mono/stereo select circuit. The equalization circuit selects equalization 1 or equalization 2 as determined by the selected antenna pattern. The mono/stereo circuit selects the required signals for stereo, mono left, mono right, or mono $\mathrm{L}+\mathrm{R}$ operation.

4-99. The output of the equalization and mono/stereo select circuits is applied to a summing amplifier network. The network functions as a matrix to generate the $\mathrm{L}+\mathrm{R}$ and $\mathrm{L}-\mathrm{R}$ stereo signals. The output of the summing amplifier network is applied to a digital switching modulator. The modulator accepts: 1) the L+R and L-R signals and 2) four RF out-of-phase signals at the carrier frequency. The modulator outputs two signals: 1) an AM modulated signal containing the $\mathrm{L}+\mathrm{R}$ information and 2) a double-sideband-suppressed-carrier signal referenced to a 90 degree carrier. The signals are summed and amplified at U37 to produce a quadrature signal. The output of U37 is applied to a fourth order linear phase bandpass filter. The output of the filter is applied to an amplitude limiter circuit. The limiting operation produces the phase modulation (L-R information) component of the C-QUAM signal. The output of the limiter circuit is routed to the exciter circuit board.

4-100. RF POWER MODULE. The PWM and RF drive signals from the exciter circuit board are routed to the RF power modules. The RF power modules consist of a modulator circuit board and two RF amplifier circuit boards.

4-101. Modulator Circuit Board. The modulator circuit board consists of a MOSFET forward converter circuit and a filter network. The forward converter circuit consists of MOSFET transistors Q1 and Q2. The filter network consists of inductors L1 through L3 and capacitors C13 through C16. A dc operating voltage for transistors Q1 and Q2 is provided by the power supply circuit board. The B- leg of the supply is routed through relay K1 to the transistors. K1 is provided to immediately terminate the supply during a modulator fault condition.

4-102. The PWM signal at a 15 volt level from the exciter circuit board is applied to the gates of MOSFET transistors Q1 and Q2. Q1/Q2 function to switch the B- leg at a 122 kHz to 135 kHz rate. The output from Q1/Q2 is applied to the LC low-pass filter network to convert the square-wave PWM signal to a dc voltage. The output from the filter will produce a 50 volt dc signal with: 1) a nominal PWM duty cycle of $40 \%$ and 2) no audio modulation. The dc voltage will vary from 0 to 125 volts with $-100 \%$ to $+150 \%$ modulation. The output of the filter network is applied to the drains of MOSFET amplifier transistors on the power amplifier circuit boards.

4-103. Power Amplifier Circuit Boards. The RF circuitry on the power amplifier circuit boards consists of a Class E MOSFET power amplifier circuit. Each power amplifier circuit board is designed to output approximately 350 watts. The power amplifier circuit boards are identical. Therefore, only power amplifier 1 will be discussed.

4-104. The MOSFET amplifier circuit is designed in a push-pull design Class E configuration. Class E power amplifier characteristics consist of: 1) the transistor drain-to-source voltage must be nominally zero immediately prior to the turn-on of the transistor and 2) the time slope of the drain-to-source voltage waveform must be nominally zero prior to the turn-on of the transistor. The Class E circuit results in: 1) lower device dissipation resulting in reduced transistor operating temperature which greatly increases component life, 2) an operating efficiency of $95 \%$ or greater, and 3 ) increased reliability when operated into VSWR conditions.

4-105. Additional characteristics of a Class E amplifier design is the application of dc power to the amplifier transistors. The B+leg of the B supply is applied to RF choke L1. The choke is connected to the primary center tap winding of combiner transformer T1. The transistors are connected to the primary winding of the transformers.

4-106. Two signals are applied to the power amplifier 1 circuit board: 1) an $R F$ square-wave signal from the driver circuit board and 2) a dc voltage from the modulator circuit board which varies at an audio rate. The RF square-wave signal at the carrier frequency is applied to the gates of MOSFETs Q1 and Q2. The varying dc voltage from the modulator circuit board is applied to the source of MOSFETs Q1 and Q2. Q1/Q2 operate in a push-pull configuration to develop approximately 350 watts of RF power at combiner transformer T1. The power at transformer T1 is combined with the 550 watts of RF power from power amplifier circuit board 2 to generate 1100 watts of RF power from the RF power module.

4-107. RF COMBINER. The RF combiner components are located on the rear-panel of each power block assembly. The combiner consists of a star combiner design. The star combiner contains an individual transformer, an RF choke, and an impedance matching circuit for each power amplifier circuit board. The impedance matching circuit consists of star inductors. The circuit presents the correct impedance when a module is removed from the chassis. This allows the transmitter to operate at an output power which is proportional to the modules removed from the power block chassis.

4-108. HARMONIC BAND-PASS FILTER. The output signal harmonic and spur frequencies are reduced to FCC, DOC, and CCIR levels by a band-pass filter. The filter consists of a fourth order LC network consisting of inductors L1 through L3 and capacitors C1 through C 4 . The components are located in the output network assembly and are frequency dependent. The output of the filter is routed to the directional coupler circuit board.

4-109. DIRECTIONAL COUPLER CIRCUIT BOARD. Transmitter forward and reflected power are sampled by a directional coupler circuit board. The directional coupler circuit board is designed to: 1) process the forward and reflected power samples for application to the controller circuit board and 2) calibrate the RF modulation monitor sample.

4-110. Forward And Reflected Power Sample Circuit. A voltage sample from the RF output is obtained by transformer T203. A current sample of the RF output is obtained by transformers T201 and T202. The current sample is converted to a voltage by a resistor network and applied to transformer T203. A voltage proportional to the square root of the forward power is obtained by summing the voltage from the secondary of T203 with the voltage sample from T201. A voltage proportional to the square root of the reflected power is obtained by summing the voltage from the secondary of T203 and with the voltage sample from T202. The forward power sample voltage is half-wave rectified by diode D202. The reflected power sample voltage is half-wave rectified by diode D201. Diodes D205 through D208 and zener diodes D209 and D210 protect the rectifier diodes from overvoltage conditions. The rectified forward and reflected power samples are routed for application to the controller circuit board. Programmable header J206 is provided to increase the adjustment range of the directional coupler circuitry. The header is programmed at the factory for the adjustment range required by the transmitter.

4-111. Modulation Monitor Calibration Circuit. A voltage sample for application to the modulation monitor calibration circuit is provided by the lightning detection circuit board. A sample from the RF output is obtained by a capacitor circuit and applied to a relay circuit on the directional coupler circuit board. The relay circuit is designed to select a voltage sample from a calibration potentiometer for application to the modulation monitor receptacle. The relays are controlled by power level 1 through 5 commands from the controller circuit board. Each relay circuit operates in an identical manner, therefore only the circuit for power level 5 will be explained.

4-112. A voltage is applied to the modulation monitor receptacle when the power level 5 command energizes relay K201. K201 applies a sample voltage to power level 5 modulation monitor calibration control R201. R201 is provided to a obtain a 2 volt RMS sample to the modulation monitor receptacle. Frequency programming switch S201 is provided to compensate the RF sample for frequencies within the AM band for power levels 1 through 3. Power level programming switch P203 is provided to program the power level 3 circuit for low power range or high power range operation. The calibrated sample from potentiometer R201 is applied to the modulation monitor receptacle.

4-113. T-MATCHING NETWORK. Output matching to antenna loads for up to a VSWR condition of $1.4: 1$ at any phase angle relative to the 50 Ohm load is provided by a T-matching network. The T-matching network consists of tune control L4, load control L6, inductor L5 and capacitor C5/C5A. Inductor L5 and capacitor C5/C5A are frequency dependent components. The tune and load controls are designed to be adjusted to present the optimum impedance for the power amplifier modules.

4-114. LIGHTNING PROTECTION CIRCUIT BOARD. The transmitter is protected from lightning potentials present at the output network by the lightning protection circuit board. The circuit board consists of series connected transzorbs. The AM-10A transmitter is equipped with transzorbs D1 through D8. The AM-6A transmitter is equipped with transzorbs D1 through D7. The transzorbs are designed to conduct the lightning potentials to ground prior to the operation of the lightning detection circuit spark-gap.
4-115. LIGHTNING DETECTION CIRCUIT BOARD. Lightning potentials present at the transmitter output are detected by the lightning detection circuit board. The circuit board is equipped with an RF sampling circuit and an optically operated transistor circuit.

4-116. The RF sampling circuit consists of a parallel capacitor circuit. The circuit is designed to provide a constant RF voltage sample for application to the directional coupler circuit board. The optically operated transistor circuit is designed to detect lightning potentials present at the transmitter output. The circuit operates in association with the lightning detector spark-gap. When lightning is present at the transmitter RF output, the spark-gap will: 1) be biased on to conduct the potential to ground and 2) emit a light pulse to optically operated transistor Q401. Q401 will be biased on to output a lightning detect signal to the controller circuit board.

4-117. RF OUTPUT POWER CONTROL CIRCUITRY. The transmitter output power is controlled by circuitry on the controller and power supply circuit boards. The transmitter power level is controlled by a Pulse-Width-Modulated (PWM) signal generated by the controller circuit board. The power control PWM signal is routed for application to the power supply circuit board(s). The power supply circuit board(s) respond by routing the required dc voltage to the modulator circuit boards and the RF amplifier circuit boards. The following text presents a description of the RF power control circuitry.

4-118. RF Output Power Control - Controller Circuit Board. A transmitter RF output power level is selected by the power control 1 through power control 5 switch/indicators. The power control switch/indicators route a LOW control signal to a priority encoder circuit. The priority encoder circuit determines which control pulse is routed to the power control circuitry. The circuit allows transmitter off commands to be assigned a high priority. With no transmitter off commands present, the power control signal is applied to multiplexer U39. U39 selects a reference voltage from the power control potentiometers on the controller circuit board. The potentiometers are designed to establish a preset transmitter power level such as 1 kW . The voltage is used as the reference for digital-to-analog converter U42. With no fault conditions present, the voltage is applied without change to power trim digital-to-analog converter U43. With no power trim commands present, the reference voltage is applied to a driver circuit which converts the dc control voltage to a power control PWM signal. The power control PWM duty cycle responds to the changes in the voltage reference level. When the voltage reference increases, the power control PWM signal duty-cycle increases. When the voltage reference decreases, the power control PWM signal duty-cycle decreases. The power control PWM signal is routed for application to the power supply circuit board(s).

4-119. The transmitter output power level is trimmed to a precise level by the power up and down switches. The switches output a LOW control signal to a control logic circuit. The control logic circuit generates the required control signals to drive an up/down counter circuit. The circuit is designed to: 1) count up if power is required to be increased or 2) count down if power is required to be decreased. The up/down counter circuit output is converted to a dc potential by digital-to-analog converter U43. The output of U43 is summed with the dc potential from power control switch digital-to-analog converter U42 to generate a dc power control signal. The power control signal is applied to the driver circuit which converts the signal to a power control PWM signal.

4-120. Automatic Power Control Circuitry. The transmitter power control circuitry is equipped with several monitor circuits designed to determine if power control correction is required during adverse operating conditions. Circuitry on the controller circuit board monitors the transmitter components and the RF output for: 1) lightning, 2) high forward power, 3) high reflected power, and 4) over-temperature. If a lightning, high forward power, high reflected power, or over-temperature, condition occurs, a signal is routed to the fault detection circuit.

4-121. The fault detection circuit: 1) processes lightning and over-temperature signals and $2)$ analyzes forward and reflected power signals. As determined by the the fault condition, the fault detection circuit will generate a fast or slow control signal to the up/down counter circuit. The counter circuit will respond by decreasing the power control voltage at digital-to-analog converter U42. U42 will respond by decreasing the output power to an acceptable level. Once the condition which caused the fault to occur is removed, the fault detection circuitry will automatically output a control signal to increase power to a normal level.
4-122. Forward/Reflected Power Circuitry. Samples of the transmitter forward and reflected power are processed by forward and reflected power circuits on the controller circuit board. Forward power samples from the directional coupler circuit board are applied to the forward power circuit. The forward power circuit converts the sample into a dc signal for application to the fault detection circuitry and to the meter switch circuit board. Reflected power samples from the directional coupler circuit board are applied to the reflected power circuit. The reflected power circuit converts the sample into a dc signal for application to the fault detection circuit and the meter switch circuit board.

4-123. Meter Switch Circuit Board. Forward and Reflected power samples from the controller circuit board are applied to the meter switch circuit board. The circuit board allows the selection of forward power, reflected power, and ac input samples for display on forward power meter M1 and reflected power meter M2.

4-124. RF Output Power Control - Power Supply Circuit Board/RF Power Modules. The power control PWM signal from the controller circuit board is applied to a correction circuit on the power supply circuit board. The PWM signal is converted to a dc signal and combined with a dc feedback signal to generate a power control signal for application to the switch regulator power control PWM circuit. The circuit converts the de signal into two PWM 180 degree out-of-phase square-wave drive signals. The square-wave drive signals are applied to a driver circuit. The driver circuit outputs the out-of-phase square-wave signals to an IGBT transistor regulator circuit. The regulator circuit transistors are operated to on for a specific time duration to generate a specific B- supply voltage. The B- supply voltage is filtered by capacitor C55 and applied to the forward power converter on the modulator circuit boards.

4-125. The main operating supply B+ leg is created by a SCR controlled bridge rectifier circuit. AC power from an ac input filter is applied to the SCR controlled bridge rectifier. The rectifier is controlled by a soft-start circuit. The full-wave rectified dc potential is filtered by inductor L1 and capacitors C24 through C27. The output of the filter generates the positive leg of a B supply. The B+ line of the power supply is applied to the forward power converter circuit on modulator circuit boards and the RF amplifier transistors on RF amplifier circuit boards.

4-126. To provide an example of output power control operation, a 10 kW output level is required from the transmitter. The controller power control PWM duty-cycle will be approximately $85 \%$. The power supply will respond by generating a 120 volt B- supply for application to the forward power converter on the modulator circuit boards. The modulator circuit boards will output a dc voltage which varies at an audio rate to the amplifier circuit boards. The amplifier circuit boards will respond by using the modulator circuit board dc voltage and the $\mathrm{B}+$ leg of the main supply to amplify the RF drive signal from the exciter circuit board.

# SECTION V <br> MAINTENANCE 

## 5-1. INTRODUCTION.

5-2. This section provides maintenance information, electrical adjustment procedures, and troubleshooting information for the Broadcast Electronics AM-10A and AM-6A transmitters.

5-3. SAFETY CONSIDERATIONS.

WARNING
THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS
WARNING WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

5-4. The AM-10A/AM-6A transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents.

5-5. In addition to high voltages and currents, the transmitter contains multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.

## 5-6. FIRST LEVEL MAINTENANCE.

5-7. First level maintenance consists of procedures applied to the equipment to prevent future failures. The procedures are performed on a regular basis and the results recorded in a maintenance log. Preventive maintenance of the transmitter consists of good housekeeping and checking performance levels using the meters and various indicators built into the equipment.

5-8. ROUTINE MAINTENANCE.

5-9. INSPECTION AND CLEANING. On a regular basis, clean the equipment of accumulated dust using a brush and vacuum cleaner. Inspect the modulator circuit boards, RF amplifier circuit boards, and the power supply circuit boards for damage caused by components overheating. Overheated components are identified by circuit board discoloration near the component leads. Inspect the circuit boards for loose hardware as required.

5-10. CONTROLLER BATTERY. Periodically, the controller battery in the ECU assembly should be checked by depressing the battery test switch on the controller circuit board. The battery test indicator will illuminate to indicate the battery is operational. If the battery test indicator fails to illuminate, the battery must be replaced. A good-quality Alkaline battery is recommended for replacement. Typically, it is recommended the controller battery be replaced annually.

5-11. AIR FILTERS. The AM-10A/AM-6A transmitters are equipped with a single screen-type air filter. The screen filter is designed to be removed and cleaned using a brush and vacuum. A dirty filter results in restricted air flow and increased operating temperatures for the transmitter solid-state components. Check the filter approximately once a week. The filter is designed to be removed during transmitter operation. To remove the filter, proceed as follows:

1. Refer to Figure 5-1 and remove the two filter housing screws.
2. Using the handles, lift the filter housing up and off of the rear door.
3. Remove the filter.

5-12. FLUSHING FANS. Inspect the transmitter flushing fans for dust accumulation and periodically clean the fans using a brush and vacuum cleaner. Do not use compressed air and an air gun. The fans are cooled by air passing around each motor. If dust is allowed to accumulate on the motors, the ambient air temperature will increase due to restricted air flow. When the ambient air temperature increases, the fan motor bearing lubricant will gradually vaporize and bearing failure will occur.

5-13. It is recommended the flushing fan mounting hardware be periodically checked. The flushing fans are equipped with sealed bearings which do not permit lubrication. If a bearing fails, the motor must be replaced.

5-14. SPARK GAP. The output network is equipped with a spark gap. The spark gap is provided to safely conduct lightning potentials appearing at the transmitter output to ground. Inspect the spark gap annually to ensure the gap is operational.

## 5-15. SECOND LEVEL MAINTENANCE.

5-16. Second level maintenance consists of procedures required to adjust the transmitter circuitry or restore the transmitter to operation after a fault has occurred. The procedures consist of electrical adjustments, troubleshooting, and component replacement procedures.


FIGURE 5-1. REMOVING THE AIR FILTER

NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED. ENSURE ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED BEFORE ATTEMPTING MAINTENANCE ON ANY AREA WITHIN THE TRANSMITTER.

5-17. The maintenance philosophy for the AM-10A/AM-6A transmitters consists of isolating a problem to a specific area. Once the specific area is located, subsequent troubleshooting using the information in the following text and the modular sections in PART II of this manual will assist in problem isolation to a replaceable assembly or component. If required, the assembly may be: 1) returned to the factory for repair or exchange or 2) repaired locally.

5-18. ELECTRICAL ADJUSTMENTS.
WARNING NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED. EN-
WARNING SURE ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED BEFORE ATTEMPTING MAINTENANCE ON ANY AREA WITHIN THE TRANSMITTER.

5-19. Adjustment procedures for controls associated with the transmitter circuitry is presented in the ECU, output network, RF power module, and power supply module sections of this manual. Determine the transmitter modular component requiring adjustment and refer to the appropriate section of this manual for the adjustment procedures.

5-20. TRANSMITTER FREQUENCY RE-PROGRAMMING.
5-21. The AM-10A/AM-6A transmitters are configured for a specific frequency when shipped from the factory. The transmitters are equipped with several frequency dependent parts and circuits. Due to the frequency dependent parts, frequency dependent circuits, and specialized procedures, the transmitters can not be reprogrammed for a different frequency in the field. If a transmitter is required to be programmed for a different frequency, contact the Broadcast Electronics Customer Service department.

5-22. TROUBLESHOOTING.

WARNING

WARNING
WARNING
WARNING

## THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS with respect to the cabinet which is at EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

5-23. The AM-10A/AM-6A transmitters are equipped with extensive indicator and meter circuitry to allow the operator to isolate problems to a specific area within the transmitter. Due to the hazardous voltages and currents contained in the equipment, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. Therefore, the transmitter indicators and meters must be used to isolate a problem to a specific area.
5-24. TRANSMITTER INDICATORS. The following text presents a description of the transmitter indicators and typical meter indications. Refer to the following text as required to determine the function of a specific indicator.

## TABLE 5-1. AM-10A INDICATORS

(Sheet 1 of 4)

| ASSEMBLY | INDICATOR FUNCTION |
| :---: | :--- |
| ECU ASSEMBLY |  |
| TRANSMITTER MONITOR |  |
| EXCITER | GREEN DISPLAY - Indicates normal exciter |
|  | operation. |
|  | RED DISPLAY - Indicates no exciter RF drive or |
| PWM output. |  |
| POWER MODULES | GREEN DISPLAY - Indicates all RF power modules |
|  | are operating normally. |
|  | YELLOW DISPLAY - Indicates one or more RF power |
|  | modules are removed from the transmitter for |
|  | maintenance. |
|  | RED DISPLAY - Indicates a modulator or power |
| amplifier circuit board fault in one or more RF power |  |
|  | modules. |
|  | GREEN DISPLAY - Indicates normal power supply |
|  | operation. |
|  | RED DISPLAY - Indicates an open loop or over- |
|  | voltage fault in one or more power supply modules. |
|  | YELLOW Display - Indicates one or more power |
|  | supplies are removed from the transmitter. |
|  |  |
|  |  |
|  |  |

TABLE 5-1. AM-10A INDICATORS
(Sheet 2 of 4)

| ASSEMBLY | INDICATOR FUNCTION |
| :---: | :---: |
| ANTENNA VSWR | GREEN DISPLAY - Indicates a normal antenna load. YELLOW DISPLAY - Indicates a VSWR condition of 1.2:1. <br> RED Display - Indicates a high reflected/forward power condition. In the AM-10A, indicates a 400 watt reflected power condition or a condition which results in a high forward power indication of greater than $20 \%$. In the AM-6A, indicates a 240 watt reflected power condition or a condition which results in a high forward power indication of greater than $20 \%$. <br> FLASHING RED Display - Indicates a reflected power emergency condition. In the AM-10A, indicates a 2000 watt reflected power condition. In the AM-6A, indicates a 1200 watt reflected power condition. |
| REMOTE | Illuminates to indicate transmitter remote control operations are enabled. Extinguishes to indicate transmitter remote control operations are disabled: 1) using the remote/local switch on the controller circuit board or 2) due to a fault in the remote control unit. |
| CONFLICT <br> transmitter. | Illuminates to indicate an incorrect power level is selected for operation into the antenna connected to the |
| LIGHTNING | In the AM-10A, Illuminates to indicate a 2700 volt or greater potential is present at the transmitter output. In the AM-6A, illuminates to indicate a 2100 volt or greater potential is present at the transmitter output. |
| INTERLOCK | Illuminates to indicate all internal and external interlocks are closed. |
| FOLDBACK | Illuminates to indicate when the transmitter is in a foldback condition. Foldback is when the transmitter output power is automatically reduced in response to one of the following fault conditions: 1) high reflected power, 2) high forward power, 3) high temperature, or 4) detection of a lightning potential. |
| OVERTEMP | Illuminates to indicate when the transmitter operating temperature exceeds $70^{\circ} \mathrm{C}\left(158{ }^{\circ} \mathrm{F}\right)$. |
| RESET | Illuminates to indicate one or more of the following transmitter faults have occurred: 1) over-temperature, 2) exciter fault, 3) power supply fault, 4) RF power module fault, 5) high reflected power, 6) reflected power emergency, or 7) lightning. Once the fault condition is removed, the fault circuitry must be reset. |

TABLE 5-1. AM-10A INDICATORS
(Sheet 3 of 4)

| ASSEMBLY | INDICATOR FUNCTION |
| :---: | :---: |
| CONTROLLER CIRCUIT BOARD PWM Mute |  |
|  | Illuminates to indicate the power control PWM signal is muted in response to a fault such as lightning, an exciter an open remote control fail-safe, an external transmitter mute, lightning |
| fault, a reflected power emergency |  |
| or high reflected or forward power. |  |
| Remote Fail-safe | Illuminates to indicate the remote control unit is enabled. |
| Battery OK | When the battery test switch is depressed, the indicator will: 1) illuminate to indicate the battery is operational or 2) not illuminate to indicate the battery is to be replaced. |
| STEREO CIRCUIT BOARD |  |
| Stereo Equalization 1 | Illuminates to indicate stereo equalization circuit 1 is active. |
| Stereo Equalization 2 | Illuminates to indicate stereo equalization circuit 2 is active. |
| EXCITER CIRCUIT BOARD |  |
| Exciter Lock | Illuminates to indicate the exciter is locked to the programmed carrier frequency. |
| Exciter +5 V | Illuminates to indicate the ECU +5 V supply is operational. |
| Exciter +15V | Illuminates to indicate the ECU +15 V supply is operational. |
| Exciter -15V | Illuminates to indicate the ECU -15 V supply is operational. |
| RF POWER MODULE |  |
| PA 1 RF DRIVE | Illuminates to indicate RF drive from the exciter circuit board is present at power amplifier 1. |
| PA 1 FAULT | Illuminates to indicate a fault has occurred in power amplifier 1. |
| PA 2 RF DRIVE | Illuminates to indicate RF drive from the exciter circuit board is present at power amplifier 2 . |
| PA 2 FAULT | Illuminates to indicate a fault has occurred in power amplifier 2. |

TABLE 5-1. AM-10A INDICATORS
(Sheet 4 of 4)

| ASSEMBLY | INDICATOR FUNCTION |
| :---: | :---: |
| MOD PWM DRIVE | Illuminates to indicate the PWM drive signal from the exciter is present at the modulator circuit board. |
| MOD POWER | Illuminates to indicate dc power from the power supply circuit board is present at the modulator circuit board. |
| MOD FAULT | Illuminates to indicate a modulator, fuse, or power supply fault has occurred in the modulator circuit board. |
| MOD FUSE | Illuminates to indicate the modulator circuit board fuse has blown. |
| POWER SUPPLY 1-2 | Illuminates to indicate an open loop, over-current, or over-voltage fault in the 1-2 power supply. The supply provides power for modules 1-2. |
| POWER SUPPLY 3-4 | Illuminates to indicate an open loop, over-current, or over-voltage fault in the $3-4$ power supply. The supply provides power for modules 3-4. |
| POWER SUPPLY 5-6 | Illuminates to indicate an open loop, over-current, or over-voltage fault in the 5-6 power supply. The supply provides power for modules 5-6. |
| POWER SUPPLY 7-8 <br> (AM-10A Only) | Illuminates to indicate an open loop, over-current, or over-voltage fault in the $7-8$ power supply. The supply provides power for modules 7-8. |
| POWER SUPPLY 9-10 <br> (AM-10A Only) | Illuminates to indicate an open loop, over-current, or over-voltage fault in the 9-10 power supply. The supply provides power for modules 9-10. |
| Exciter -15V | Illuminates to indicate the ECU -15 V supply is operational. |



## CAUTION WHEN AC POWER IS APPLIED TO THE TRANSMITTER AND THE RF DRIVE AND PWM DRIVE INDICATORS ON RF POWER MODULES IN A POWER BLOCK ARE EXTINGUISHED, THE RF POWER MODULES MUST BE REMOVED FROM THE TRANSMITTER CHASSIS TO PREVENT DAMAGE TO THE MODULES.

5-25. RF POWER MODULE REMOVAL. When ac power is applied to the transmitter, check the RF DRIVE and PWM DRIVE indicators on the RF power modules. If the RF DRIVE and PWM DRIVE indicators on RF power modules in a power block are extinguished, the RF power modules must be removed from the transmitter to prevent damage to the modules.

5-26. TRANSMITTER TROUBLESHOOTING PROCEDURES. Table $5-2$ presents troubleshooting information for the AM-10A/AM-6A transmitters. Refer to Table 5-2 to isolate the problem to a specific assembly. Once the trouble is isolated, refer to the applicable modular section of this manual for the theory of operation and schematic diagrams to assist in problem resolution.

5-27. TRANSMITTER COMPONENT LOCATIONS. Figures 5-2 through 5-4 present transmitter component locations. Refer to Figures 5-2 to 5-4 as required during the troubleshooting procedures to locate components within the transmitter.

TABLE 5-2. AM-10A/AM-6A TROUBLESHOOTING
(Sheet 1 of 5)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| NO OUTPUT POWER | 1. Check the ac line voltage using the reflected power/ |
| NO NORMAL/FAULT | ac voltage meter. If no line voltage is present, check |
| INDICATIONS |  |
| circuit breaker CB1. |  |

TABLE 5-2. AM-10A/AM-6A TROUBLESHOOTING
(Sheet 2 of 5)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| RED POWER SUPPLY | 1. Check for an over-temperature condition by <br> INDICATION <br> inspecting the fans and filter. |
|  | 2. If the fans and filter are normal, use the power supply <br> fault display circuit boards in each cabinet to <br> determine the defective power supply module. When <br> the defective power supply is located, refer to the <br> POWER SUPPLY MODULE section and troubleshoot <br> the power supply module. |
| YELLOW ANTENNA INDICATION |  |

# TABLE 5-2. AM-10A/AM-6A TROUBLESHOOTING 

(Sheet 3 of 5)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| CONFLICT INDICATION | 1. Ensure a +5 volt status signal from the selected antenna is applied to the antenna $\mathrm{A}, \mathrm{B}$, or C input on the ECU rear-panel. <br> 2. Ensure the correct transmitter power level is selected for operation into the antenna. <br> 3. Check the antenna interlock circuit programming on the controller circuit board. <br> 4. Refer to the ECU section and troubleshoot the controller circuit board for a conflict indication. |
| NO OUTPUT POWER LIGHTNING INDICATOR ILLUMINATED | 1. Transmitter operated to off due to $7 \mathrm{on} / \mathrm{off}$ cycles within 15 seconds. Operate the transmitter to on as follows: 1) do not depress any controller switch/indicators for approximately 30 seconds and 2) depress the desired power level switch/indicator. <br> 2. Ensure J 1 on output network is connected. <br> 3. Check Q401 on the lightning detection circuit board. |
| NORMAL OUTPUT POWER LIGHTNING INDICATOR ILLUMINATED | 1. Indicates the presence of lightning at the output of transmitter. Depress the RESET switch to reset the indicator. |
| INTERLOCK INDICATOR EXTINGUISHED | 1. Ensure a +5 volt signal is applied to external interlock input TB1-29 on the ECU rear panel. |
| OVERTEMP INDICATOR ILLUMINATED | 1. Ensure the transmitter air filter is clean. <br> 2. Check the transmitter fans in each cabinet. If the fans are not operating, check optical-coupled-relay (OCR) K1. <br> 3. Ensure the transmitter exhaust area is clear of obstructions. |
| MISSING NORMAL/FAULT INDICATIONS FOR A POWER BLOCK | 1. Check the fuses for the power supply: 1) power supply 1-2 = F6 and F7, 2) power supply 3-4 = F8 and F9, 3) power supply 5-6 = F10 and F11, 4) power supply $7-8=\mathrm{F} 12$ (AM-10A only) and F13, 5) power supply $9-10=$ F14 and F15 (AM-10A only). <br> 2. Check power transformer T1 on the power supply panel. |
| NO L+R MODULATION ACTIVITY DURING MONO OPERATION | 1. Ensure audio is present at TB2-25 through TB2-30 on the ECU rear panel. <br> 2. Check for audio at J101-29 through J101-31 and J101-36/J101-37 on the ECU motherboard. If no audio is present, check the filter components on the ECU motherboard. <br> 3. Refer to the ECU section and troubleshoot the exciter circuit board. |

TABLE 5-2. AM-10A/AM-6A TROUBLESHOOTING
(Sheet 4 of 5)

| SYMPTOM |
| :--- |
| NO L+R MODULATION ACTIVITY |
| DURING STEREO OPERATION |
|  |
|  |
|  |
|  |
| RF DRIVE INDICATORS |
| EXTINGUISHED FOR A |
| POWER BLOCK |

LOW DEMODULATOR LEFT CHANNEL MODULATION LEVEL
WITH LOW EXCITER
MONITOR LEFT CHANNEL MODULATION LEVEL
LOW DEMODULATOR RIGHT CHANNEL MODULATION LEVEL WITH LOW EXCITER MONITOR RIGHT CHANNEL MODULATION LEVEL

LOW DEMODULATOR LEFT CHANNEL MODULATION LEVEL WITH NORMAL EXCITER MONITOR LEFT CHANNEL MODULATION LEVEL
LOW DEMODULATOR RIGHT CHANNEL MODULATION LEVEL WITH NORMAL EXCITER MONITOR RIGHT CHANNEL MODULATION LEVEL
PWM DRIVE INDICATOR EXTINGUISHED ON A POWER BLOCK

1. Ensure audio is present at TB2-25 through TB2-30 on the ECU rear panel.
2. Check for audio at J101-29 through J101-31 and J101-36/J101-37 on the ECU motherboard. If no audio is present, check the filter components on the ECU motherboard.
3. Refer to the ECU section and troubleshoot the exciter circuit board.
4. Check the RF drive output on the ECU motherboard as follows: 1) output 1 -P101-7, 2) output 2 - P101-47 $3)$ output $3=$ P101-9, 4) output $4=$ P101-49 (AM-10A only), and 5) output $5=\mathrm{P} 101-5$ (AM-10A only).
5. If no RF drive is present, refer to the ECU section and troubleshoot the exciter circuit board.
6. If RF drive is present at the exciter circuit board, check bridge rectifiers D10 and D11 on the power supply module for the power block.
7. Refer to the RF POWER MODULE section and troubleshoot each RF power module.
8. Refer to the ECU section and troubleshoot the exciter circuit board.
9. Refer to the ECU section and troubleshoot the exciter circuit board.
10. Refer to the ECU section and troubleshoot the stereo circuit board.
11. Refer to the ECU section and troubleshoot the stereo circuit board.
12. Refer to the ECU section and troubleshoot the exciter circuit board. ELECTRONICS INC

TABLE 5-2. AM-10A/AM-6A TROUBLESHOOTING
(Sheet 5 of 5)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| PWM DRIVE AND RF DRIVE INDICATORS EXTINGUISHED ON ALL POWER BLOCKS | 1. Refer to the ECU section and troubleshoot the exciter circuit board. |
| MOD PWR INDICATORS EXTINGUISHED ON A POWER BLOCK | 1. Check for a power control PWM signal at the drain of Q22 on the controller circuit board. <br> A. If the PWM signal is not present, refer to the ECU section and troubleshoot the controller circuit board for no power control PWM signal. <br> B. If the PWM output is present, check for a LOW at Q13 on the controller circuit board. <br> 1. If the LOW at Q13 is not present, refer to the ECU section and troubleshoot the controller circuit board for no transmitter on signal. <br> 2. If the LOW at Q13 is present, refer to the POWER SUPPLY section and troubleshoot the power supply for no MOD POWER indicator on a power block. |
| REFLECTED POWER METER <br> FLUCTUATES WITH MODULATION | 1. Narrow-band antenna. Contact the Broadcast Electronics Customer Service Department. |
| FORWARD POWER METER <br> FLUCTUATES WITH MODULATION | 1. Enable the high-pass filter on the exciter circuit board. |

5-28. COMPONENT REPLACEMENT PROCEDURE. Component replacement on printed circuit boards requires extreme care to avoid damage to the circuit board traces. The following text describes the procedure to replace components on the circuit boards.
$5-29$. On all circuit boards, the adhesive securing the copper trace to the board melts at almost the same temperature at which solder melts. A circuit board trace can be destroyed by excessive heat or lateral movement during soldering. Use of a small iron with steady pressure is required for circuit board repairs.

5-30. To remove a component from a circuit board, cut the leads from the body of the defective component while the device is still soldered to the board.
5-31. Grip each component lead, one at a time, with long-nose pliers. Rotate the circuit board and touch a soldering iron to the lead at the solder connection. When the solder begins to melt, push the lead through the back side of the board. Each lead may now be heated independently and pulled out of each hole. The holes may be cleared of solder by carefully re-heating each hole with a low wattage iron and removing the residual solder with a soldering vacuum tool.

MOST SOLVENTS WHICH WILL REMOVE ROSIN FLUX ARE VOLATILE AND TOXIC BY THEIR NATURE AND SHOULD BE USED ONLY IN SMALL AMOUNTS IN A WELL VENTILATED AREA, AWAY FROM FLAME SUCH AS FROM A SOLDERING IRON OR SMOKING MATERIALS. OBSERVE THE MANUFACTURER'S CAUTIONARY INSTRUCTIONS.

5-32. Install the new component and apply solder from the bottom side of the circuit board. After soldering, remove flux with a cotton swab moistened with a suitable solvent. Rubbing alcohol is highly diluted and is not effective.

5-33. The board should be checked to ensure the flux has been removed and not just smeared. Rosin flux is not normally corrosive, but rosin will absorb enough moisture in time to become conductive and cause problems.

5-34. INTEGRATED CIRCUITS. Special care should be exercised with integrated circuits. Each integrated circuit must be installed by matching the integrated circuit notch with the notch on the socket. Do not attempt to remove an integrated circuit from a socket with your fingers. Use an integrated circuit puller to lightly pry the component from the socket.


FIGURE 5-2. AM-10A COMPONENT LOCATOR (SHEET 1 OF 4)



FIGURE 5-2. AM-10A COMPONENT LOCATOR (SHEET 2 OF 4)


597-1113-17
FIGURE 5-2. AM-10A COMPONENT LOCATOR (SHEET 3 OF 4)


597-1113-19
FIGURE 5-2. AM-10A COMPONENT LOCATOR (SHEET 4 OF 4)


FIGURE 5-3. AM-6A COMPONENT LOCATOR (SHEET 1 OF 4)


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FIGURE 5-3. AM-6A COMPONENT LOCATOR (SHEET 2 OF 4)


FIGURE 5-3. AM-6A COMPONENT LOCATOR (SHEET 3 OF 4)


597-1113-19A

FIGURE 5-3. AM-6A COMPONENT LOCATOR (SHEET 4 OF 4)


ECU COMPONENT LOCATOR


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POWER BLOCK COMPONENT LOCATOR COPYRIGHT © 1997 BROADCASt ELECTRONICS, INC
FIGURE 5-4. ECU/POWER BLOCK COMPONENT LOCATOR

## SECTION VI <br> PARTS LIST

## 6-1. INTRODUCTION.

6-2. This section provides parts lists for the AM-10A/AM-6A transmitter. The parts lists provide descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance. Each parts list entry in this section is indexed by reference designators appearing on the applicable schematic diagrams.

TABLE 6-1. AM-10A/AM-6A REPLACEABLE PARTS LIST INDEX (Sheet 1 of 2)

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :---: | :---: | :---: | :---: |
| 6-2 | AM-10A Transmitter, 3-Phase/Single-Phase | $\begin{array}{r} 907-1010-001 / \\ -041 / \\ -011 \end{array}$ | 6-3 |
| 6-3 | AM-6A Transmitter, 3-Phase/Single-Phase | $\begin{array}{r} 907-6000 /-030 / \\ -040 \end{array}$ | 6-3 |
| 6-4 | AM-10A Rack Assembly | 907-0110 | 6-4 |
| 6-5 | AM-6A Rack Assembly | 907-0106 | 6-4 |
| 6-6 | AM-10A Fan Assembly | 380-7650-010 | 6-5 |
| 6-7 | AM-6A Fan Assembly | 380-7650-006 | 6-5 |
| 6-8 | Interface Circuit Board Assembly | 917-0306-003 | 6-5 |
| 6-9 | Power Supply Status LED Circuit Board Assembly | 917-0306-006 | 6-5 |
| 6-10 | Temperature Sensor Circuit Board Assembly | 917-0306-009 | 6-6 |
| 6-11 | Wire Harness Main AM Transmitter | 947-0182 | 6-6 |
| 6-12 | Harness, Add-On, AM-6A | 947-0190 | 6-6 |
| 6-13 | AC Distribution Panel Assembly, AM-10A | $\begin{array}{r} 957-0021-001 / \\ -041 / \\ -011 \end{array}$ | 6-7 |
| 6-14 | AC Distribution Panel Assembly, AM-6A | $\begin{array}{r} 957-0013-010 / \\ -030 /- \end{array}$ | $\begin{gathered} 6-7 \\ -040 \end{gathered}$ |
| 6-15 | Optically Coupled Relay Circuit Board Assembly | 919-0096-001 | 6-8 |
| 6-16 | Optically Coupled Relay Circuit Board Assembly | 919-0096 | 6-8 |
| 6-17 | AC Sample Circuit Board Assembly | 917-0306-007 | 6-9 |
| 6-18 | AC Distribution Harness Assembly, AM-10A | 947-0185 | 6-10 |
| 6-19 | AC Distribution Harness Assembly, AM-6A | 947-0191 | 6-10 |
| 6-20 | Power Block, Single Assembly/Double Assembly, AM-10A | $\begin{array}{r} 957-0022-001 / \\ -002 \end{array}$ | 6-9 |
| 6-21 | Power Block, Single Assembly, AM-6A | 957-0022-061 | 6-10 |
| 6-22 | Power Block, Double Assembly, AM-6A | 957-0022-062 | 6-11 |
| 6-23 | Power Block Motherboard Circuit Board Assembly | 917-0303 | 6-11 |
| 6-24 | Combiner Circuit Board Assembly, AM-10A/AM-6A | 917-0321/-006 | 6-11 |

TABLE 6-1. AM-10A/AM-6A REPLACEABLE PARTS LIST INDEX
(Sheet 2 of 2)

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :---: | :---: | :---: | :---: |
| 6-25 | Accessory Parts Kit, AM-10A | 957-0031/-010 | 6-11 |
| 6-26 | Accessory Parts Kit, AM-6A | 957-0033 | 6-12 |
| 6-27 | Frequency Dependant Kit, AM-10A, 522-650 KHZ | 957-0015-101 | 6-12 |
| 6-28 | Frequency Dependant Kit, AM-10A, 651 - 770 KHZ | 957-0015-102 | 6-13 |
| 6-29 | Frequency Dependant Kit, AM-10A, 771 - 920 KHZ | 957-0015-103 | 6-13 |
| 6-30 | Frequency Dependant Kit, AM-10A, 921-1080 KHZ | 957-0015-104 | 6-13 |
| 6-31 | Frequency Dependant Kit, AM-10A, 1081-1300 KHZ | 957-0015-105 | 6-13 |
| 6-32 | Frequency Dependant Kit, AM-10A, 1301-1580 KHZ | 957-0015-106 | 6-13 |
| 6-33 | Frequency Dependant Kit, AM-10A, 1581-1700 KHZ | 957-0015-107 | 6-14 |
| 6-34 | Frequency Dependant Kit, AM-6A, $522-650 \mathrm{KHZ}$ | 957-0015-061 | 6-14 |
| 6-35 | Frequency Dependant Kit, AM-6A, $651-770$ KHZ | 957-0015-062 | 6-14 |
| 6-36 | Frequency Dependant Kit, AM-6A, $771-920$ KHZ | 957-0015-063 | 6-14 |
| 6-37 | Frequency Dependant Kit, AM-6A, 921 - 1080 KHZ | 957-0015-064 | 6-14 |
| 6-38 | Frequency Dependant Kit, AM-6A, 1081 - 1300 KHZ | 957-0015-065 | 6-15 |
| 6-39 | Frequency Dependant Kit, AM-6A, 1301 - 1580 KHZ | 957-0015-066 | 6-15 |
| 6-40 | Frequency Dependant Kit, AM-10A, 1581-1700 KHZ | 957-0015-067 | 6-15 |
| 6-41 | Power Block Frequency Dependant Kit, AM-10A, 522-650 KHZ | 957-1025-051 | 6-15 |
| 6-42 | Power Block Frequency Dependant Kit, AM-10A, 651-770 KHZ | 957-1025-052 | 6-15 |
| 6-43 | Power Block Frequency Dependant Kit, AM-10A, 771 - 920 KHZ | 957-1025-053 | 6-16 |
| 6-44 | Power Block Frequency Dependant Kit, AM-10A, 921-1080 KHZ | 957-1025-054 | 6-16 |
| 6-45 | Power Block Frequency Dependant Kit, AM-10A, 1081 - 1300 KHZ | 957-1025-055 | 6-16 |
| 6-46 | Power Block Frequency Dependant Kit, AM-10A, 1301 - 1580 KHZ | 957-1025-056 | 6-16 |
| 6-47 | Power Block Frequency Dependant Kit, AM-10A, 1581 - 1700 KHZ | 957-1025-057 | 6-16 |
| 6-48 | Power Block Frequency Dependant Kit, AM-6A, 522-650 KHZ | 957-1025-061 | 6-17 |
| 6-49 | Power Block Frequency Dependant Kit, AM-6A, 651-770 KHZ | 957-1025-062 | 6-17 |
| 6-50 | Power Block Frequency Dependant Kit, AM-6A, 771 - 920 KHZ | 957-1025-063 | 6-17 |
| 6-51 | Power Block Frequency Dependant Kit, AM-6A, 921-1080 KHZ | 957-1025-064 | 6-17 |
| 6-52 | Power Block Frequency Dependant Kit, AM-6A, 1081 - 1300 KHZ | 957-1025-065 | 6-17 |
| 6-53 | Power Block Frequency Dependant Kit, AM-6A, 1301 - 1580 KHZ | 957-1025-066 | 6-17 |
| 6-54 | Power Block Frequency Dependant Kit, AM-6A, | 957-1025-067 | 6-18 |

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TABLE 6-2. AM-10A TRANSMITTER, 3-PHASE/SINGLE-PHASE -907-1010-001/-041/-011

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| M1 | Meter, 3.5 Inch ( 8.89 cm ), Taut Band Type, FS = $1 \mathrm{~mA} \mathrm{dc} \pm 1 \%$, 35 Ohm Resistance (FORWARD POWER METER) | 310-0067 | 1 |
| M2 | Meter, 3.5 Inch ( 8.89 cm ), Taut Band Type, FS = $1 \mathrm{~mA} \mathrm{dc} \pm 1 \%$, 35 Ohm Resistance (REFLECTED POWER Meter) | 310-0066 | 1 |
| ---- | Assembly, Rack, AM-10A | 957-0110 | 1 |
| ---- | Air Filter, FXA 17.40 X 41.00 X .86 Inch (44.2 X 104.14 X 2.18 cm ) | 407-0174 | 1 |
| ---- | Connector, Anchor Insulated (Bullet) $15 / 8$ " Line | 427-0009 | 1 |
| ---- | Adapter, $15 / 8$ Inch EIA Flanged to Unflanged | 427-0010 | 1 |
| ---- | Pins, Connector | 417-0036 | 10 |
| ---- | Connector Housing, 2-Pin, Male | 418-0702 | 5 |
| ---- | AC Distribution Panel Assembly, AM-10A 1 Phase | 957-0021-011 | 1 |
| ---- | Exciter/Controller Assembly, AM-1A | 957-0009-011 | 1 |
| ---- | Power Module Assembly, AM-1A | 957-0010-001 | 10 |
| ---- | Power Block, Single AM-A Assembly | 957-0022-001 | 1 |
| ---- | Power Block, Double AM-A Assembly | 957-0022-002 | 2 |
| ---- | Output Network Assembly, AM-10A | 957-0030 | 1 |
| ---- | Power Supply Panel Assembly, AM-10 | 957-0315 | 5 |
| ---- | Kit, Frequency Dependent Parts | 957-0015-XXX | 1 |
| FOR 907-1010-001 ASSEMBLIES |  |  |  |
| ---- | AC Distribution Panel Assembly, AM-10A 3 Phase | 957-0021-001 | 1 |
| ---- | Accessory Parts Kit, AM-10A 3 Phase | 957-0031 | 1 |
|  | - FOR 907-1010-041 ASSEMBLIES |  |  |
| ---- | AC Distribution Panel Assembly, AM-10A, 4 Wire Wye | 957-0021-041 | 1 |
| ---- | Accessory Parts Kit, AM-10A 3 Phase | 957-0031 | 1 |
| FOR 907-1010-011 ASSEMBLIES |  |  |  |
| --- | AC Distribution Panel Assembly, AM-10A Single- Phase | 957-0021-011 | 1 |
| --- | Accessory Parts Kit, AM-10A Single-Phase | 957-0031-010 | 1 |

TABLE 6-3. AM-6A TRANSMITTER, 3-PHASE/SINGLE-PHASE - 907-6000/-030/-040 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| ---- | Meter, 3.5 Inch ( 8.89 cm ), Taut Band Type, FS $=1 \mathrm{~mA} \mathrm{dc} \pm 1 \%$, 35 Ohm Resistance (REFLECTED POWER METER) | 310-0064 | 1 |
| --- | Meter, 3.5 Inch ( 8.89 cm ), Taut Band Type, FS $=1 \mathrm{~mA} \mathrm{dc} \pm 1 \%$, 35 Ohm Resistance (FORWARD POWER METER) | 310-0077 | 1 |
| ---- | Assembly, Rack, AM-6A | 957-0106 | 1 |
| -- | Air Filter, FXA 17.40 X 41.00 X .86 Inch (44.2 X 104.14 X 2.18 cm ) | 407-0174 | 1 |
| ---- | Exciter/Controller Assembly | 957-0009-011 | 1 |
| ---- | Power Module Assembly | 957-0010-001 | 6 | ELECTRONICS INC

TABLE 6-3. AM-6A TRANSMITTER, 3-PHASE/SINGLE-PHASE - 907-6000/-030/-040
(Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| --- | Power Block, Single Single AM-6A Assembly | 957-0022-061 | 1 |
| ---- | Power Block, Double AM-6A Assembly | 957-0022-062 | 1 |
| --- | Output Network Assembly | 957-0032 | 1 |
| ---- | Accessory Parts Kit, AM-6A | 957-0033 | 1 |
| ---- | Power Supply Panel Assembly, AM-10 | 957-0315 | 3 |
| -- | AC Distribution Panel Assembly, AM-6A 1 Phase | 957-0013-010 | 1 |
| ---- | Kit, Frequency Dependent Parts | 957-0015-XXX | 1 |
|  | FOR 907-6000-030 ASSEMBLIES |  |  |
| --- | AC Distribution Panel, AM-6A 3 Phase Delta $\qquad$ FOR 907-6000-040 ASSEMBLIES | 957-0013-030 | 1 |
| - | AC Distribution Panel Assembly, AM-6A 3 Phase WYE $\qquad$ FOR 907-6000-030/-040 ASSEMBLIES | 957-0013-040 | 1 |
|  | DELETE PARTS |  |  |
| --- | Fuse, 100 Amperes, Dual Element, Time Delay | 334-0002 | 2 |
| --- | AC Distribution Panel Assembly, AM-6A 1 Phase | 957-0013-010 | 1 |
| ---- | ADD PARTS <br> Fuse, 60 Amperes, FLN-R60 | 334-2502 | 3 |

TABLE 6-4. AM-10A RACK ASSEMBLY- 907-0110

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Assembly, Fan, 6 inch | $380-7650-010$ | 1 |
| ---- | Interface Circuit Board Assembly, AM-1A | $917-0306-003$ | 1 |
| --- | Power Supply Status LED Circuit Board Assembly, AM-1A | $917-0306-006$ | 1 |
| ---- | Temperature Sensor Circuit Board Assembly, AM-1A | $917-0306-009$ | 1 |
| ---- | Wire Harness Main AM-10A Transmitter | $947-0182$ | 1 |

TABLE 6-5. AM-6A RACK ASSEMBLY- 907-0106

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Assembly, Fan, 6 inch | $380-7650-006$ | 1 |
| ---- | Interface Circuit Board Assembly, AM-1A | $917-0306-003$ | 1 |
| --- | Power Supply Status LED Circuit Board Assembly, AM-1A | $917-0306-006$ | 1 |
| ---- | Temperature Sensor Circuit Board Assembly, AM-1A | $917-0306-009$ | 1 |
| ---- | Wire Harness, Add-On, AM-6A | $947-0190$ | 1 |

TABLE 6-6. AM-10A FAN ASSEMBLY - 380-7650-010

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Fan, 6 inch $(15.24 \mathrm{~cm}), 250 \mathrm{ft} 3 / \mathrm{min} 220 \mathrm{~V} \mathrm{ac}, 50 / 60 \mathrm{~Hz}, 40 \mathrm{Watt}$ | $380-7650$ | 5 |
| ---- | Pins, Connector | $417-0036$ | 10 |
| --- | Housing, Connector, $2-P i n$ | $418-0702$ | 5 |

TABLE 6-7. AM-6A FAN ASSEMBLY - 380-7650-006

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Fan, 6 inch $(15.24 \mathrm{~cm}), 250 \mathrm{ft} 3 / \min 220 \mathrm{~V} \mathrm{ac}, 50 / 60 \mathrm{~Hz}, 40 \mathrm{Watt}$ | $380-7650$ | 3 |
| --- | Pins, Connector | $417-0036$ | 6 |
| --- | Housing, Connector, $2-P i n$ | $418-0702$ | 3 |

TABLE 6-8. INTERFACE CIRCUIT BOARD ASSEMBLY - 917-0306-003

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| D301 thru | Diode, 1N4005, Silicon, 600V @ 1 Ampere | $203-4005$ | 5 |
| D305 |  |  |  |
| J301 | Connector, Male, 24-Pin | $417-2401$ | 1 |
| J302 thru | Connector, 9-Pin | $418-0900$ | 3 |
| J304 |  |  |  |
| J305 | Connector, Male, 20-Pin, PCB Mount | $417-0230$ | 1 |
| J306, J307 | Receptacle, Male, 3-Pin In-line | $417-0003$ | 2 |
| J308 | Connector, 9-Pin | $418-0900$ | 1 |
| J309 | Connector, Male, 2-Pin In-Line | $417-4004$ | 1 |
| P306, P307, | Jumper, Programmable, 2-Pin | $340-0004$ | 3 |
| P309 |  |  | $103-4423$ |

TABLE 6-9. POWER SUPPLY STATUS LED CIRCUIT BOARD ASSEMBLY - 917-0306-006

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C601 thru | Capacitor, Monolythic Ceramic, $.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 5 |
| C605 |  |  |  |
| DS601 thru | Indicator, LED, Red, $521-9212,1.7 \mathrm{~V} @ 50 \mathrm{~mA}$ Maximum | $323-9217$ | 5 |
| DS605 | Receptacle, 12-Pin | $417-1276$ | 1 |
| J601 | Blank, Power Supply Status LED Circuit Board | $517-0306-006$ | 1 |

TABLE 6-10. TEMPERATURE SENSOR CIRCUIT BOARD ASSEMBLY - 917-0306-009

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C902 | Capacitor, Monolythic Ceramic, $.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C906 | Capacitor, Monolythic Ceramic, $.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C907 | Capacitor, Ceramic, $0.001 \mathrm{uF}, 1 \mathrm{kV}$ | $002-1034$ | 1 |
| J901 | Socket, 4-Pin | $418-0255$ | 1 |
| R901 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $100-1051$ | 1 |
| R902 | Resistor, 2.21 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-2241$ | 1 |
| R903 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $100-1051$ | 1 |
| TP901, TP902 | Terminal, Turret, Double Shoulder | $413-1597$ | 2 |
| U901 | Integrated Circuit, LM35DZ, Celsius Temperature Sensor, | $220-0035$ | 1 |
|  | TO-92 Case |  |  |
| ---- | Blank, Temperature Sensor Circuit Board | $517-0306-009$ | 1 |

TABLE 6-11. WIRE HARNESS MAIN AM TRANSMITTER, AM-10A - 947-0182

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Pin Connector | $417-0036$ | 32 |
| ---- | Pins, Connector | $417-0053$ | 308 |
| ---- | Connector Plug, 9-Pin | $417-0059$ | 3 |
| ---- | Pins, Connector | $417-0142$ | 69 |
| ---- | Receptacle, 20-Pin | $417-0176$ | 1 |
| ---- | Connector Plug, 25-Pin | $417-0251$ | 3 |
| ---- | Connector, Housing, 15-Pin | $417-2379$ | 2 |
| ---- | Housing, Female, 24-Pin | $417-2402$ | 12 |
| ---- | Kit, Housing, 25-Pin | $417-2510$ | 3 |
| ---- | Plug, Housing, 4-Pin | $418-0240$ | 1 |
| ---- | Connector Housing, 6-Pin | $418-0670$ | 1 |
| ---- | Connector Housing, 2-Pin, Female | $418-0701$ | 7 |
| ---- | Connector Housing, 2-Pin, Male | $418-0702$ | 6 |
| ---- | Plug, Connector Housing, 12-Pin | $418-1271$ | $418-2379$ |

TABLE 6-12. HARNESS, ADD-ON, AM-6A - 947-0190
(Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Pin Connector |  | $417-0036$ |
| ---- | Pins, Connector | $417-0053$ | 16 |
| ---- | Connector Plug, 9-Pin | $417-0059$ | 212 |
| ---- | Pins, Connector | $417-0142$ | 3 |
| ---- | Receptacle, 20-Pin | $417-0176$ | 51 |
|  |  |  | 1 |

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TABLE 6-12. HARNESS, ADD-ON, AM-6A - 947-0190
(Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| ---- | Connector Plug, 25-Pin | $417-0251$ | 3 |
| ---- | Connector, Housing, 15-Pin | $417-2379$ | 2 |
| ---- | Housing, Female, 24-Pin | $417-2402$ | 7 |
| ---- | Kit, Housing, 25-Pin | $417-2510$ | 3 |
| ---- | Plug, Housing, 4-Pin | $418-0240$ | 1 |
| ---- | Connector Housing, 6-Pin | $418-0670$ | 1 |
| ---- | Connector Housing, 2-Pin, Female | $418-0701$ | 5 |
| ---- | Connector Housing, 2-Pin, Male | $418-0702$ | 4 |
| ---- | Plug, Connector Housing, 12-Pin | $418-1271$ | 1 |
| ---- | Plug, 15-Pin, Male | $418-2379$ | 2 |

TABLE 6-13. AC DISTRIBUTION PANEL ASSEMBLY, AM-10A -
$957-0021-001 /-041 /-011$

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| K1 | Optically Coupled Relay Circuit Board Assembly | 919-0096-001 | 1 |
| TB1 | Barrier Strip, 9 Terminal | 412-0090 | 1 |
| TB2 | Barrier Strip, 3 Position, 4 AWG TO 1/4" QCX4 | 412-0049 | 1 |
| ---- | Varistor, V271BA60, Harris, 275V | 140-0032 | 3 |
| ---- | Fuse, 3AG, 250V, 2 Amperes | 330-0200 | 10 |
| ---- | Fuse Holder, AGC | 415-2012 | 10 |
| ---- | Terminal, Male | 410-0064 | 2 |
| ---- | AC Distribution, "A" Version AM Panel | 471-5091-100 | 1 |
| ---- | AC Sample Circuit Board Assembly, AM-1A | 917-0306-007 | 1 |
| ---- | Circuit Breaker, 150 Amperes, 600 V ac | 341-0051 | 1 |
| ---- | AC Distribution Harness AM-10A 3 Phase Assembly | 947-0185 | 1 |
|  | - FOR 957-0021-041 ASSEMBLY |  |  |
| ---- | Circuit Breaker, 150 Amperes, 600 V ac | 341-0051 | 1 |
| ---- | AC Distribution Harness AM-10A 3 Phase Assembly $\qquad$ FOR 957-0021-011 ASSEMBLY | 947-0186 | 1 |
| ---- | Circuit Breaker, 200 Amperes, 600 V ac | 341-0001-1 | 1 |
| --- | AC Distribution Harness AM-10A 1 Phase Assembly | 947-0187 | 1 |

TABLE 6-14. AC DISTRIBUTION PANEL ASSEMBLY, AM-6A - 957-0013-010/-030/-040 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| ---- | Metal-Oxide Varistor, B40K275, 275V, 1680 Joules | $140-0021$ | 3 |
| --- | Fuse, 3AG, 250V, 2 Amperes | $330-0200$ | 6 |

TABLE 6-14. AC DISTRIBUTION PANEL ASSEMBLY, AM-6A - 957-0013-010/-030/-040 (Sheet 2 of 2)


TABLE 6-15. OPTICALLY COUPLED RELAY CIRCUIT BOARD ASSEMBLY - 919-0096-001

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Optically Coupled Relay Circuit Board Assembly | $919-0096$ | 1 |
| DELETE PARTS | $000-1051$ | 1 |  |
| R2 | Capacitor, Ceramic Disc, $0.1 \mathrm{uF}, 600 \mathrm{~V}$ | $110-5633$ | 1 |

TABLE 6-16. OPTICALLY COUPLED RELAY CIRCUIT BOARD ASSEMBLY - 919-0096 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C1 | Capacitor, Ceramic, $0.001 \mathrm{uF}, 1 \mathrm{kV}$ | $002-1034$ |  |
| C2 | Capacitor, Electrolytic, $47 \mathrm{uF}, 35 \mathrm{~V}$ | $020-4773$ | 1 |
| C3 | Capacitor, Ceramic Disc, $0.1 \mathrm{uF}, 600 \mathrm{~V}$ | $000-1051$ | 1 |

TABLE 6-16. OPTICALLY COUPLED RELAY CIRCUIT BOARD ASSEMBLY - 919-0096 (Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C4 | Capacitor, Ceramic, $0.001 \mathrm{uF}, 1 \mathrm{kV}$ | 002-1034 | 1 |
| D1 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D2 | Diode, Zener, 1N5359, 24V $\pm 10 \%$, 5 W | 200-5359 | 1 |
| D4 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D5 | Bridge Rectifier, MDA970A3, 4 Amps, 50-200V | 239-0003 | 1 |
| E1 thru E5 | Terminal, Male Disconnect | 410-0025 | 5 |
| F1, F2 | Fuse, 3 Amps, 250V, Printed Circuit Board Mount | 330-0055 | 2 |
| K1 | Relay, Printed Circuit Board Mount <br> Coil: 24 V dc, 660 Ohm $\pm 10 \%$ <br> Contacts: SPST-NO, 0.5 to $15 \mathrm{~A} @ 12$ to 240 V ac Resistance | 270-0054 | 1 |
| MOV1 | Varistor, 27V, V27ZA60 | 140-0023 | 1 |
| R1 | Resistor, 2 k Ohm $\pm 3 \%, 10 \mathrm{~W}, \mathrm{~W} / \mathrm{W}$ | 130-2032 | 1 |
| R2 | Resistor, $560 \mathrm{Ohm} \pm 5 \%$, 1/2W | 110-5633 | 1 |
| R3 | Resistor, $820 \mathrm{Ohm} \pm 5 \%, 1 / 2 \mathrm{~W}$ | 110-8233 | 1 |
| R4 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R5 | Resistor, 2 k Ohm $\pm 3 \%, 10 \mathrm{~W}, \mathrm{~W} / \mathrm{W}$ | 130-2032 | 1 |
| U1 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 1 |
| XU1 | Socket, 6-Pin DIP | 417-0600 | 1 |
| ---- | Cover, Dust Relay, 35C620A | 270-0054-001 | 1 |
| ---- | Blank, Optically Coupled Relay Circuit Board | 519-0096 | 1 |

TABLE 6-17. AC SAMPLE CIRCUIT BOARD ASSEMBLY - 917-0306-007

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C701 | Capacitor, Polypropylene Film, $.47 \mathrm{uF} \pm 10 \%, 600 \mathrm{~V}$ | $033-4763$ | 1 |
| D701 thru | Diode, 1N4005, Silicon, $600 \mathrm{~V} @ 1$ Ampere | $203-4005$ | 4 |
| D704 |  |  |  |
| E701, E702 | Terminal, Male Disconnect | $410-0025$ | 2 |
| J701 | Connector, 2-Pin | $417-0700$ | 1 |
| R701 thru | Resistor, 150 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1561$ | 6 |
| R706 |  |  | $100-3373$ |

TABLE 6-18. AC DISTRIBUTION HARNESS ASSEMBLY, AM-10A - 947-0185

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Pins, Connector | Connector Housing, 2-Pin, Female | $417-0053$ |
| --- | Plug, Connector Housing, 12-Pin | $418-0701$ | 12 |
| ---- | Wire, AWG 10, Stranded 65/28, Black | $418-1271$ | 1 |
| ---- | Wire, AWG 6, Hypalon, Belden 34406 | $601-0110$ | 1 |
| ---- | Wire, AWG 12, Stranded 19/25, Red | $601-0600$ | 3 |
| --- | Wire, AWG 16, Stranded 19/29, Yellow | $601-1202$ | 5 |
| ---- | Wire, AWG 18, Stranded 19/30, Black | $601-1604$ | 7 |
| ---- | AC Line Cord, N.E.M.A. 3-Wire North American Plug | $601-1800$ | 10 |
| ---- | $682-0001$ | 24 |  |
|  |  |  | 1 |

TABLE 6-19. AC DISTRIBUTION HARNESS ASSEMBLY, AM-6A - 947-0191

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Pins, Connector | $417-0053$ | 12 |
| ---- | Connector Housing, 2-Pin, Female | $418-0701$ | 1 |
| ---- | Plug, Connector Housing, 12-Pin | $418-1271$ | 1 |
| ---- | Wire, AWG 10, Stranded 65/28 Black | $601-0110$ | 3 |
| ---- | Wire, AWG 6, Hypalon, Belden 34406 | $601-0600$ | 5 |
| ---- | Wire, AWG 12, Stranded 19/25, Red | $601-1202$ | 7 |
| ---- | Wire, AWG 16, Stranded 19/29, Yellow | $601-1604$ | 10 |
| ---- | Wire, AWG 18, Stranded 19/30, Black | $601-1800$ | 24 |
| ---- | AC Line Cord, N.E.M.A. 3-Wire North American Plug | $682-0001$ | 1 |

TABLE 6-20. POWER BLOCK, SINGLE ASSEMBLY /DOUBLE ASSEMBLY, AM-10A-
$957-0022-001 /-002$

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Power Block Motherboard Circuit Board Assembly | $917-0303$ | 1 |
| --- | Combiner Circuit Board Assembly | $917-0321$ | 1 |

TABLE 6-21. POWER BLOCK, SINGLE ASSEMBLY, AM-6A - 957-0022-061

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| --- | Power Block Motherboard Circuit Board Assembly | $917-0303$ | 1 |
| ---- | Combiner Circuit Board Assembly | $917-0321-006$ | 1 |

TABLE 6-22. POWER BLOCK, DOUBLE ASSEMBLY, AM-6A - 957-0022-062

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| --- | Power Block Motherboard Circuit Board Assembly | $917-0303$ | 2 |
| ---- | Combiner Circuit Board Assembly | $917-0321-006$ | 2 |

TABLE 6-23. POWER BLOCK MOTHERBOARD CIRCUIT BOARD ASSEMBLY - 917-0303

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1, C2 | Capacitor, Ceramic, Monolythic, $.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ |  |
| C3, C4 | Capacitor, Polypropylene Film, $2.2 \mathrm{uF}, 400 \mathrm{~V}$ | $030-2256$ | 2 |
| E1, E2, | Stud, PEM, KFH-832-8ET, PCB Mount | $426-8007$ | 14 |
| E5 thru E8 |  |  |  |
| E11 thru E16 |  | $417-2401$ |  |
| E22, E23 | Connector, Male, 24-Pin | $417-0300$ | $417-0375$ |
| J3 | $370-0037$ | 6 |  |
| J1A thru J1F | Socket, Card Edge, AMP 531353-6 | $517-0303$ | 2 |
| J2A thru J2F | Connector, 15-Pin SUB-D, Female | 2 |  |
| T1, T2 | Transformer, P.A. Drive, AM-1/5 |  |  |
| ---- | Blank, Power Block Motherboard Circuit Board |  |  |

TABLE 6-24. COMBINER CIRCUIT BOARD ASSEMBLY, AM-10A/AM-6A - 917-0321/-006

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| E1 thru E9 | Stud, PEM, KFH-832-8ET, PCB Mount | $426-8007$ | 9 |
| L1 thru L4 | RF Choke Assembly, AM-1A | $360-0107$ | 4 |


|  |  |  |  |
| :--- | :--- | :--- | :--- |
| T1 thru T4 | Combiner Transformer Assembly | $370-0057$ | 4 |


|  |  |  |  |
| :--- | :--- | :--- | :--- |
| T1 thru T4 | Combiner Transformer Assembly |  |  |
| TP1 thru | Terminal, Test Point, Oval, Red | $370-0058$ | 4 |
| TP10 A17-321-006 AM-6A ASSEMBLY | $413-0106$ | 10 |  |
| ---- | Blank, Combiner Circuit Board, AM-1A | $517-0321$ | 1 |

TABLE 6-25. ACCESSORY PARTS KIT, AM-10A - 957-0031/-010
(Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Fuse, 3AG, 250V, 2 Amperes | $330-0200$ | 12 |
| ---- | Fuse, 3AB, 15 Amperes, 65 V, Very Fast | $330-1502$ | 5 |

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TABLE 6-25. ACCESSORY PARTS KIT, AM-10A - 957-0031/-010
(Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| -- | Fuse, 3AB, 250V, 20 Amperes | 330-2000 | 5 |
| ---- | Fuse, 30 Amperes, 125V | 334-0030-001 | 4 |
| - | Fuse, 5 X 20MM, 1.5A, Slow-Blow | 334-1150 | 8 |
| FOR 957-0031 ASSEMBLIES |  |  |  |
| ---- | Fuse, AGC, 1A, MDL, 250V, Slow-Blow | 334-0100 | 4 |
|  | - FOR 957-0031-010 ASSEMBLIES |  |  |
| --- | Fuse, 3AG, 1/2A, 250V, Slow-Blow | 334-0500 | 4 |
| ---- | Battery, 9 Volt, Alkaline | 350-0002 | 1 |
| ---- | Ferrite Core Toroid .5 X 2.187 X 3.375 | 360-0099 | 2 |
| --- | Ferrite Core 1.102 OD X . 63 ID X . 512 THK | 375-0009 | 2 |
| --- | Mounting, Adhesive Back, SMS-A-15-PANDUIT | 401-0015 | 5 |
| ---- | Adjustment Tool, Extended and Recessed Flat Blades | 407-0186 | 1 |
| -- | Kit, Instruction Manual, AM-6A/10A | 977-1113 | 1 |
| ---- | Adjustment Tool, 3/16 Hex | 710-0400 | 1 |

TABLE 6-26. ACCESSORY PARTS KIT, AM-6A - 957-0033

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Fuse, 3AG, 250V, 2 Amperes | $330-0200$ | 8 |
| ---- | Fuse, 3AB, 15 Amperes, 65V, Very Fast | $330-1502$ | 3 |
| ---- | Fuse, 3AB, 250V, 20 Amperes | $330-2000$ | 3 |
| ---- | Fuse, 30 Amperes, 125V | $334-0030-001$ | 4 |
| ---- | Fuse, AGC, 1A, MDL, 250V, Slow-Blow | $334-0100$ | 3 |
| ---- | Fuse, 5 X 20MM, 1.5A, Slow-Blow | $334-1150$ | 6 |
| ---- | Battery, 9 Volt, Alkaline | $350-0002$ | 1 |
| ---- | Ferrite Core Large AM Transmitter | $375-0007-001$ | 2 |
| ---- | Ferrite Core 1.102 OD X .63 ID X .512 THK | $375-0009$ | 2 |
| ---- | Mounting, Adhesive Back, SMS-A-15-PANDUIT | $401-0015$ | 5 |
| ---- | Adjustment Tool, Extended and Recessed Flat Blades | $407-0186$ | 1 |
| ---- | Kit, Instruction Manual, AM-3A/5A/10A | $977-1113$ | 1 |

TABLE 6-27. FREQUENCY DEPENDANT KIT, AM-10A, 522-650 KHZ - 957-0015-101
REF. DES. $\quad$ DESCRIPTION PART NO. QTY.

|  | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, Board, 522 - 650 KHZ | 957-1015-001 |
| :---: | :---: | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Block, 522-650 KHZ | 957-1025-051 |
|  | Kit, Frequency Dependent Parts, Output Network, 522-650 KHZ | 957-1035-101 |

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TABLE 6-28. FREQUENCY DEPENDANT KIT, AM-10A, 651-770 KHZ - 957-0015-102

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, $957-1015-002$ <br> Board, 651 - 770 KHZ | 1 |  |
| ---- | Kit, Frequency Dependent Parts, Power Block, $651-770 \mathrm{KHZ}$ | $957-1025-052$ | 1 |
| ---- | Kit, Frequency Dependent Parts, Output Network, $651-770 \mathrm{KHZ}$ | $957-1035-102$ | 1 |

TABLE 6-29. FREQUENCY DEPENDANT KIT, AM-10A, 771 - 920 KHZ - 957-0015-103

| REF. DES. $\quad$ DESCRIPTION PART NO. QTY. |
| :--- | :--- | :--- |

---- Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, 957-1015-003 Board, 771 - 920 KHZ
---- Kit, Frequency Dependent Parts, Power Block, 771 - 920 KHZ $957-1025-053 \quad 1$
---- Kit, Frequency Dependent Parts, Output Network, 771 - 920 KHZ $957-1035-103 \quad 1$

TABLE 6-30. FREQUENCY DEPENDANT KIT, AM-10A, 921-1080 KHZ - 957-0015-104

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, Board, 921 - 1080 KHZ | 957-1015-004 | 1 |
| ---- | Kit, Frequency Dependent Parts, Power Block, 921-1080 KHZ | 957-1025-054 | 1 |
| ---- | Kit, Frequency Dependent Parts, Output Network, 921 - 1080 KHZ | 957-1035-104 | 1 |

TABLE 6-31. FREQUENCY DEPENDANT KIT, AM-10A, 1081 - 1300 KHZ - 957-0015-105

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |


|  | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, Board, 1081 - 1300 KHZ | 957-1015-005 |
| :---: | :---: | :---: |
|  | Kit, Frequency Dependent Parts, Power Block, 1081 - 1300 KHZ | 957-1025-055 |
| ---- | Kit, Frequency Dependent Parts, Output Network, 1081-1300 KHZ | 957-1035-105 |

TABLE 6-32. FREQUENCY DEPENDANT KIT, AM-10A, 1301-1580 KHZ - 957-0015-106
REF. DES. DESCRIPTION PART NO. QTY.
---- Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, 957-1015-006 ..... 1

$$
\text { Board, } 1301-1580 \mathrm{KHZ}
$$

---- Kit, Frequency Dependent Parts, Power Block, 1301 - 1580 KHZ 957-1025-056 1
---- Kit, Frequency Dependent Parts, Output Network, 1301-1580 KHZ 957-1035-106 1

TABLE 6-33. FREQUENCY DEPENDANT KIT, AM-10A, 1581 - $\mathbf{1 7 0 0}$ KHZ - 957-0015-107

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :---: | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, $957-1015-007$ | 1 |  |
| $-\quad$ Board, 1581 - 1700 KHZ |  |  |  |

TABLE 6-34. FREQUENCY DEPENDANT KIT, AM-6A, 522 - 650 KHZ - 957-0015-061
REF. DES. DESCRIPTION PART NO. QTY.
---- Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, 957-1015-001 Board, 522 - 650 KHZ
---- Kit, Frequency Dependent Parts, Power Block, 522-650 KHZ 957-1025-061 1
---- Kit, Frequency Dependent Parts, Output Network, 522-650 KHZ 957-1035-061 1

TABLE 6-35. FREQUENCY DEPENDANT KIT, AM-6A, 651-770 KHZ - 957-0015-062

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, Board, 651 - 770 KHZ | 957-1015-002 | 1 |
| ---- | Kit, Frequency Dependent Parts, Power Block, 651-770 KHZ | 957-1025-062 | 1 |
| ---- | Kit, Frequency Dependent Parts, Output Network, 651-770 KHZ | 957-1035-062 | 1 |

TABLE 6-36. FREQUENCY DEPENDANT KIT, AM-6A, 771-920 KHZ - 957-0015-063

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, <br> Board, $771-920 \mathrm{KHZ}$ | $957-1015-003$ | 1 |
| ---- | Kit, Frequency Dependent Parts, Power Block, $771-920 \mathrm{KHZ}$ | $957-1025-063$ | 1 |
| --- | Kit, Frequency Dependent Parts, Output Network, $771-920 \mathrm{KHZ}$ | $957-1035-063$ | 1 |

TABLE 6-37. FREQUENCY DEPENDANT KIT, AM-6A, 921 - 1080 KHZ - 957-0015-064
REF. DES. DESCRIPTION PART NO. QTY.
---- Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, 957-1015-004 1 Board, 921 - 1080 KHZ
---- Kit, Frequency Dependent Parts, Power Block, 921-1080 KHZ 957-1025-064 1
---- Kit, Frequency Dependent Parts, Output Network, 921-1080 KHZ 957-1035-064 1

TABLE 6-38. FREQUENCY DEPENDANT KIT, AM-6A, 1081-1300 KHZ - 957-0015-065

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, Board, 1081 - 1300 KHZ | 957-1015-005 | 1 |
| ---- | Kit, Frequency Dependent Parts, Power Block, 1081 - 1300 KHZ | 957-1025-065 | 1 |
| ---- | Kit, Frequency Dependent Parts, Output Network, 1081 - 1300 KHZ | 957-1035-065 | 1 |

TABLE 6-39. FREQUENCY DEPENDANT KIT, AM-6A, 1301 - 1580 KHZ - 957-0015-066

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- | :---: |
| ---- | Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, $957-1015-006$ | 1 |  |
| Board, 1301-1580 KHZ |  |  |  |

TABLE 6-40. FREQUENCY DEPENDANT KIT, AM-10A, 1581 - 1700 KHZ - 957-0015-067

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |

---- Kit, Frequency Dependent Parts, Power Amplifier Modulator Circuit, 957-1015-007 $\quad 1$
---- Kit, Frequency Dependent Parts, Power Block, 1581 - 1700 KHZ $957-1025-067 \quad 1$
---- Kit, Frequency Dependent Parts, Output Network, 1581-1700 KHZ 957-1035-067 1

TABLE 6-41. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 522 - 650 KHZ -957-1025-051

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru Coil, $522-650 \mathrm{kHz}$  $360-0114-\mathrm{XXX}$ <br> L8    | 4 |  |  |

TABLE 6-42. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 651 - 770 KHZ -957-1025-052

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru <br> L8 | Coil, $651-770 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ |

TABLE 6-43. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 771-920 KHZ -957-1025-053

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $771-920 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ |
| L8 |  |  | 4 |

TABLE 6-44. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 921-1080 KHZ -957-1025-054

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $921-1080 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ |
| L8 |  |  | 4 |

TABLE 6-45. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 1081 - 1300 KHZ -957-1025-055

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $1081-1300 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 |  |  |  |

TABLE 6-46. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 1301-1580 KHZ -957-1025-056

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| L5 thru | Coil, $1301-1580 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 | Inductor, $120 \mathrm{uH}, 1.5$ Amperes $\pm 10 \%$ | $360-1824$ | 1 |

TABLE 6-47. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-10A, 1581 - 1700 KHZ -957-1025-057

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| L5 thru | Coil, $1581-1700 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 | Inductor, $100 \mathrm{uH}, 1.5$ Amperes $\pm 10 \%$ | $360-1823$ | 1 |

TABLE 6-48. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 522-650 KHZ -957-1025-061

| REF. DES. | DESCRIPTION | PART NO. | QTY. |  |
| :--- | :--- | :--- | :--- | :--- |
| L5 thru | Coil, $522-650 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ | 4 |
| L8 |  |  |  |  |

TABLE 6-49. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 651-770 KHZ -957-1025-062

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $651-770 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 |  |  |  |

TABLE 6-50. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 771-920 KHZ -957-1025-063

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $771-920 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ |
| L8 |  | 4 |  |

TABLE 6-51. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 921-1080 KHZ -957-1025-064

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| L5 thru | Coil, $921-1080 \mathrm{kHz}$ |  | $360-0114-\mathrm{XXX}$ |
| L8 |  |  |  |

TABLE 6-52. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 1081-1300 KHZ -957-1025-065

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $1081-1300 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 |  |  |  |

TABLE 6-53. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 1301-1580 KHZ -957-1025-066

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| L5 thru | Coil, $1301-1580 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 | Inductor, $120 \mathrm{uH}, 1.5$ Amperes $\pm 10 \%$ | $360-1824$ | 1 |

TABLE 6-54. POWER BLOCK FREQUENCY DEPENDANT KIT, AM-6A, 1581-1700 KHZ -957-1025-067

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L5 thru | Coil, $1581-1700 \mathrm{kHz}$ | $360-0114-\mathrm{XXX}$ | 4 |
| L8 | Inductor, $100 \mathrm{uH}, 1.5$ Amperes $\pm 10 \%$ | $360-1823$ | 1 |

## SECTION VII DRAWINGS

## 7-1. INTRODUCTION.

7-2. This section provides schematic diagrams and assembly diagrams as indexed below for the Broadcast Electronics AM-10A/AM-6A transmitters.

| FIGURE | TITLE | NUMBER |
| :---: | :---: | :---: |
| 7-1 | OVERALL SCHEMATIC DIAGRAM, AM-10A TRANSMITTER, THREE-PHASE, 220V | SB907-1010-001 |
| 7-2 | OVERALL SCHEMATIC DIAGRAM, AM-10A TRANSMITTER, THREE-PHASE, 415V | SB907-1010-041 |
| 7-3 | OVERALL SCHEMATIC DIAGRAM, AM-10A TRANSMITTER, SINGLE PHASE | SB907-1010-011 |
| 7-4 | OVERALL SCHEMATIC DIAGRAM, AM-6A TRANSMITTER, THREE-PHASE, 220V | SB907-6000-030 |
| 7-5 | OVERALL SCHEMATIC DIAGRAM, AM-6A TRANSMITTER, THREE-PHASE, 415V | SB907-6000-040 |
| 7-6 | OVERALL SCHEMATIC DIAGRAM, AM-6A TRANSMITTER, SINGLE PHASE | SB907-6000 |
| 7-7 | SCHEMATIC DIAGRAM, INTERFACE CIRCUIT BOARD | SB917-0306-003 |
| 7-8 | SCHEMATIC DIAGRAM, POWER SUPPLY STATUS CIRCUIT BOARD | SA917-0306-006 |
| 7-9 | SCHEMATIC DIAGRAM, TEMPERATURE SENSOR CIRCUIT BOARD | SA917-0306-009 |
| 7-10 | SCHEMATIC DIAGRAM, AC SAMPLE CIRCUIT BOARD | SA917-0306-007 |
| 7-11 | ASSEMBLY DIAGRAM, ECU DISPLAY CIRCUIT BOARD | $\begin{aligned} & \text { AD917-0306-001/ } \\ & -002 /-003 /-004 / \\ & -005 /-006 /-007 / \\ & -009 /-014 \end{aligned}$ |
| 7-12 | SCHEMATIC DIAGRAM, POWER BLOCK MOTHERBOARD AND COMBINER | SB917-0303/-001 |
| 7-13 | ASSEMBLY DIAGRAM, POWER BLOCK MOTHERBOARD | AC917-0303/-001 |
| 7-14 | ASSEMBLY DIAGRAM, COMBINER | $\begin{array}{r} \mathrm{AC} 917-0321 /-001 \\ -006 \end{array}$ |
| 7-15 | SCHEMATIC DIAGRAM, OPTICALLY COUPLED RELAY | SB919-0096/-001 |
| 7-16 | ASSEMBLY DIAGRAM, OPTICALLY COUPLED RELAY (OCR) | AB919-0096/-001 |



























|  | D | MATERIAL$\begin{gathered} \text { SEE B/M } \\ 919-0096 \\ 919-0096-001 \\ \hline \end{gathered}$ | TELEX 250142 CABLE BROADCAST FAX 217/224-960? |  |  |  |  |  |  |  |
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|  |  | FINISHSEE DWG RA59z-8008 | optically coupled relay bo. |  |  |  |  |  |  |  |
|  | PROJ. LEADER <br> J. TUCKER 7-14-86 |  |  |  |  |  |  |  |  |  |
|  |  |  | A | B | 919-009 | 919- | - |  |  | N |
|  | MFG. <br> J.STEINKAMP 7-14-8\$ |  | MODEL | TRA | NSMITTERS | SCALE | $1=1$ | SHEET | OF |  |



## TABLE OF CONTENTS

PARAGRAPH
PAGE NO.

SECTION I
1-1
1-3
1-6
1-8
1-10
1-12
1-15
1-18
1-20
1-23
1-25
1-28
1-30
1-31
1-33
1-34
1-38
1-43
1-47
SECTION II
2-1
2-3
2-6
2-8
2-10
2-12
2-13
2-14
2-17
2-18
SECTION III
3-1
SECTION IV 4-1

FIGURE
1-1

TABLE
2-1
3-1
POWER SUPPLY THEORY OF OPERATION
Introduction ..... 1-1
General Description ..... 1-1
AC Input ..... 1-1
Conventional Rectifier Circuitry ..... 1-1
Soft-Start Circuit ..... 1-1
AC Line Detection/Synchronization ..... 1-2
Soft-Start Control Circuit ..... 1-2
Power Factor Corrector Circuit Board Control Circuit ..... 1-2
SCR Controlled Rectifier Circuit ..... 1-5
Filter Circuit ..... 1-5
Power Supply Enable Circuit ..... 1-5
Switching Regulator Circuit ..... 1-5
Low Voltage Power Supply ..... 1-6
Switching Regulator Control Circuit ..... 1-6
Switching Regulator Circuit Operation ..... 1-6
Power Control/Correction Circuit ..... 1-6
Fault Detection ..... 1-7
Crowbar Circuit ..... 1-7
Power Supply Circuit Grounds ..... 1-8
POWER SUPPLY CIRCUIT BOARD MAINTENANCE
Introduction ..... 2-1
Safety Considerations ..... 2-1
First Level Maintenance ..... 2-1
Cleaning and Inspection ..... 2-1
Second Level Maintenance ..... 2-2
Troubleshooting ..... 2-2
Safety Considerations ..... 2-2
Removing/Installing a Power Supply Circuit Board ..... 2-2
Troubleshooting Procedures ..... 2-3
Component Replacement Procedure ..... 2-4
POWER SUPPLY CIRCUIT BOARD PARTS LIST
Introduction ..... 3-1
POWER SUPPLY CIRCUIT BOARD DRAWINGS
Introduction ..... 4-1
LIST OF ILLUSTRATIONS
TITLEPOWER SUPPLY CIRCUIT BOARDSIMPLIFIED SCHEMATIC
LIST OF TABLES
TITLE
POWER SUPPLY MODULE TROUBLESHOOTING ..... 2-3

3-1
PAGE NO.

PAGE NO.
1-3

# SECTION I POWER SUPPLY THEORY OF OPERATION 

## 1-1. INTRODUCTION.

1-2. This section presents a general description of the Broadcast Electronics AM-10A/AM-6A transmitter power supply assembly.
1-3. GENERAL DESCRIPTION.
1-4. $\quad \mathrm{DC}$ operating potentials for the RF power modules are provided by power supply assemblies (refer to Figure 1-1). The power supply assembly consists of: 1) a power supply circuit board and 2) filter and transformer components located on a power supply panel. One power supply assembly provides dc operating potentials for one power block. The AM-10A transmitter is equipped with 5 power supply assemblies. The AM-6A transmitter is equipped with 3 power supply assemblies.

1-5. The modular design of the power supply assembly allows the power supply circuit board to be removed from the transmitter for maintenance. The following text presents a description of the power supply circuit board and the components located on the power supply panel assembly.

## 1-6. AC INPUT.

1-7. AC power from the ac input switch is applied through fuses F6 and F7 to power transformer T1. Fuses F6 and F7 protect the circuitry from over-current conditions. Transformer T1 consists of: 1) a single primary winding and 2) five secondary windings. The transformer is designed to provide low-voltage ac samples for application to five conventional bridge rectifier circuits.

1-8. CONVENTIONAL RECTIFIER CIRCUITRY.
1-9. AC power from a winding of power transformer T1 is applied to bridge rectifier D11. D11 rectifies the ac potential into an unregulated 30 V dc supply for application to the RF power module power amplifier circuit boards. Capacitor C21 provides filtering for the supply. AC power from a second winding of transformer T1 is applied to bridge rectifier D10. D10 rectifies the ac potential into an unregulated +20 V dc supply for the power supply circuit board circuitry. Capacitor C20 provides filtering for the supply. AC power from a third winding of ac power transformer T1 is applied to bridge rectifier D9. D9 rectifies the ac potential into an unregulated +20 volt dc supply for application to: 1 ) the modulator circuit board and 2) to regulator U3. U3 is a +15 volt dc regulator. The output of U3 routed for application to the components on the power supply circuit board. AC power from a fourth winding of power transformer T1 is applied to bridge rectifier D12. D12 rectifies the ac potential into an unregulated +15 V dc supply for application to: 1) the power supply circuit board and 2) regulator U 4 . U4 is a +12 volt dc regulator. The output of U 4 routed for application to the components on the power supply circuit board. An ac sample from the winding is routed for application to a soft-start circuit. Capacitor C15 provides filtering for the supply.

1-10. SOFT-START CIRCUIT.
1-11. An ac sample from the winding of T1 is also routed to a soft-start circuit. The soft-start circuit is designed to eliminate component stress during turn-on by limiting the current in-rush. The circuit consists of an ac line detection/synchronization and soft-start control circuits.

1-12. AC LINE DETECTION/SYNCHRONIZATION. An ac sample from a winding of transformer T1 is rectified by diodes D7 and D8 and applied to integrated circuit U6B. U6B functions as a zero phase detector. As the ac line phase approaches zero degrees, U6B will output a HIGH pulse. The HIGH pulse is applied to: 1) transistor Q2, 2) transistor Q7 of the soft-start circuit, and 3) ac line detector U5A/U5B. The pulse biases transistor Q2 and optical coupler U2 on. Q2 and U2 will output a pulse each time the ac line phase is zero. As a result, U2 will output a 120 Hz signal to the controller circuit board.

1-13. U5A and U5B function as an ac line voltage detector. When ac line voltage is present, U5A will output a LOW. The LOW allows transistor Q3 to be biased on. With Q3 on, a +12 volt dc signal is applied to optical coupler U1. When a power supply enable and a PWM OK signal is applied to U1, U1 will output a reference voltage to a soft-start control circuit for power supply operation. When ac line voltage is not present, U5A will output a HIGH, the HIGH biases transistor Q3 off to terminate power supply operation. When ac power is re-applied, U5B will maintain a HIGH for 100 milliseconds to allow the circuit to stabilize during turn-on operations.
1-14. In addition to the ac line voltage detection circuit, integrated circuit U6A functions as a low line voltage detector. When the dc supply is above the threshold at U6A, U6A will output a LOW to bias transistor Q1 off. As a result, a HIGH ac OK signal indicating acceptable ac line voltage is applied to optical coupler U9. When the dc supply is below 185 volts, U6A will output a HIGH to bias transistor Q1 on. As a result, a LOW ac OK signal indicating low ac line voltage is applied to optical coupler U9. When the voltage increases to approximately 190 volts, the output of U6A will go LOW to enable the power supply.

1-15. This circuit is also used to detect high ac line voltage potentials. If the ac line voltage is above approximately 270 volts, transistor Q28 will be biased on. With Q28 on, the input to U6A will be muted. When the input is muted: 1) the transmitter output power will be muted and 2) no transmitter fault or emergency condition will be generated.

1-16. SOFT-START CONTROL CIRCUIT. The soft-start control circuit consists of: 1) transistors Q4 through Q9 and 2) integrated circuit U7. The circuit is designed to generate short duration pulses in each time the ac line waveform crosses the 0 volt axis. The pulses are applied to an SCR controlled rectifier to slowly bias the components on during initial start operations. This operation eliminates the component stress at power-on by limiting the supply in-rush current.
1-17. The circuit generates the soft-start pulses from two signals: 1 ) a ramp signal and 2) a triangle signal. The ramp signal is generated by transistors Q4 and Q5. When ac line voltage is detected, $\mathrm{a}+12$ volt signal from U 1 is applied to transistor Q4. Q4 operates in association with capacitor C16 and transistor Q5 to generate a ramp voltage. The triangle signal is generated by transistors Q6 and Q7. Pulses from U6B are applied to transistor Q7. Q7 operates in association with capacitor C17 and transistor Q6 to generate a triangle signal. The triangle signal and the ramp signal are applied to comparator U7. U7 responds by generating a square-wave signal with a short duty cycle when the ac line phase is zero. The square-wave signal from U7 is applied to soft-start driver transistors Q8 and Q9. Q8 and Q9 will slowly bias the rectifier circuit on to limit the current in-rush.

## 1-18. POWER FACTOR CORRECTOR CIRCUIT BOARD CONTROL CIRCUIT.

1-19. Transistors Q26 and Q27 control a power factor corrector circuit board (not used in A-Series AM transmitters). During soft-start operation, ramp voltage will drop below approximately 3 V . When this occurs, the output of transistor Q26 will go LOW. This LOW biases transistor Q27 on. With Q27 on, a LOW energizes two relays on the power factor corrector circuit board. With the relays energized, a capacitor is inserted into the circuit to enable power factor correction.


## SCR CONTROLLED RECTIFIER CIRCUIT.

1-21. The ac line voltage is rectified into a main dc supply for the modulator and amplifier circuitry by an SCR controlled bridge rectifier circuit. Primary ac power for the main dc supply is applied to ac line filter FL1. FL1 is a modular line filter designed to protect the circuitry from EMI. The ac from filter FL1 is applied to fuses F1 and F2. The fuses protect the power supply circuitry from over-current conditions. Metal-Oxide-Varistor MOV1 prevents damage to the rectifier circuitry from ac line voltage surge potentials.

1-22. The SCR controlled rectifier circuit consists of diodes D15 through D17 and SCRs D13 and D14. The rectifier circuit is controlled by the soft-start control circuit. When power is required from the circuit, the soft-start circuit will output synchronized ac line pulses to SCRs D13 and D14. The SCRs will respond by slowly biasing the rectifier circuit on. The rectifier will output an unregulated and unfiltered dc supply at a maximum of 300 V to an inductor and capacitor filter network located on the power supply panel.

1-23. FILTER CIRCUIT.
1-24. The output of the rectifier circuit is applied to a filter network consisting of inductor L1 and capacitors C24 through C27. The filter is designed to remove the ripple in the supply. The output of the capacitor network generates the positive leg of the B supply. The B supply is the main operating supply for the RF power modules. The negative leg of the B supply is generated by a switching regulator circuit (refer to the following text).

1-25. POWER SUPPLY ENABLE CIRCUIT.
1-26. The power supply is controlled by a: 1) power supply enable signal from the controller and 2) power supply mute signal from the modulator circuit boards. When power supply operation is required, the controller will output a LOW power supply enable signal to optical coupler U8. With no mute signals present, U8 will output a HIGH to AND gate U12A. With a HIGH ac OK signal from U9 indicating the presence of ac power and no power supply faults, U12A will output a HIGH to U12B. With a HIGH from U21A/U21B, U12B will output a HIGH to U12C and to Q12. With a HIGH from U14 indicating the crowbar circuit is off, U12C will output a HIGH after a one second delay to: 1) transistor Q10, 2) AND gate U12D, and 3) NAND gate U21C. The HIGH biases Q12 and U15 on to disable the crowbar circuit. Q10 will respond by routing a HIGH power supply enable signal to optical coupler U1. U1 will output a dc voltage to enable the power supply soft-start circuit. AND gate U12D will output a HIGH to transistor Q11. The HIGH biases Q11 on to enable regulator controller U13 and bias Q13 off.

1-27. When a power supply mute operation is required, an RF power module modulator circuit board will output a mute signal to optical coupler U8. U8 will output a LOW to AND gate U12A. With a HIGH ac OK signal from U9, U12A will output a LOW to U12B. U12B will output a LOW to U12C and to Q12. The LOW biases Q12 and U15 off to enable the crowbar circuit. U12C will output a LOW to: 1) transistor Q10, 2) AND gate U12D. Q10 will be biased off to terminate power supply operation by disabling the drive to the SCR rectifier circuit. U12D will disable Q11 which allows a HIGH to disable regulator controller U13 and bias Q13 on. Q13 will output a LOW to disable the fault detection circuit to prevent erroneous fault indications during mute conditions.

1-28. SWITCHING REGULATOR CIRCUIT.
1-29. The B supply is regulated and controlled by a switching regulator circuit. The switching regulator circuit generates the - leg of the $B$ supply and consists of: 1) a low voltage power supply circuit, 2) a power control network, 3) optical coupler U17, 4) inverting buffer U19, and 5) switching regulator transistors Q21 and Q22.

1-30. LOW VOLTAGE POWER SUPPLY. A dc operating supply for the optical couplers and the inverting buffers is generated by bridge rectifier D25. D25 full-wave rectifies an ac potential from ac transformer T1 into an unregulated +20 V supply. The supply is applied to +18 V regulator U16. The output of U16 is further regulated to a 5 V operating potential by a resistive divider and a zener diode. The 5 V supply is applied to optical coupler U17 and buffer U19.

1-31. SWITCHING REGULATOR CONTROL CIRCUIT. The switching regulator circuit is controlled by: 1) regulator controller U13 and 2) a power control/correction circuit. The circuits function in a closed-loop to control the operation of the switching regulator. As a result, the regulator outputs a precision dc operating voltage at the appropriate level for application to the RF power modules.

1-32. Integrated circuit U13 functions as the switching regulator controller. U13 is a PWM output device designed to produce two out-of-phase square wave signals with varying duty cycles. The duty cycle is varied in response to the signal from the voltage correction circuit. With a correction voltage present at U13, U13 will output a PWM square wave signal to optical coupler U17. U17 provides isolation for the transition of the signal from two different circuit ground potentials. The output of coupler U17 is inverted by inverting buffer U19.

1-33. SWITCHING REGULATOR CIRCUIT OPERATION. The PWM output of U19 is applied to the gates of IGBT (insulated-gate-bipolar-transistor) switching regulator transistors Q21 and Q22. The transistors function to regulate the negative leg of the B supply. The output of the transistor switching regulator circuit is applied to filter inductor L2. Protection of the transistors from switching transients during turn on/off operation is provided by clamp diode D32. Capacitor C55 provides filtering for the negative leg of the B supply. The output of the regulator circuit ( $\mathrm{B}-\mathrm{leg}$ ) is applied to circuitry on the modulator circuit board.

## 1-34. POWER CONTROL/CORRECTION CIRCUIT.

1-35. The switching regulator output voltage is controlled by a PWM (pulse-width-modulated) signal from the controller. The PWM signal is a 1 kHz square-wave signal with a duty cycle which varies in response to different power levels. The PWM signal from the controller is applied to optical coupler U22. With a +5 volt signal from the motherboard, U22 will output the PWM signal to transistors Q17 and Q18. Q17 will discharge capacitor C63 when a 1 kHz control signal is present. C63 will output a LOW PWM OK signal to optical coupler U1. Q18 inverts the power control PWM signal. The output of Q18 is applied through buffer U24C to a low-pass filter consisting of: 1) resistors R115, R116, and R117 and 2) capacitors C75, C76, and C77. The filter converts the power control PWM squarewave signal into a dc control voltage. The voltage is routed through buffer U24A to U24B.

1-36. U24B functions as a current feedback loop filter. U24B differentially amplifies the dc control voltage and a current sample from the switching regulator output filter capacitor. As a result, U24B produces a dc control voltage for application to U24D.

1-37. U24D functions as a voltage feedback loop filter. U24D differentially amplifies the control voltage from U24B and a voltage sample from the B+ leg of the supply. As a result, U24D produces a dc control voltage for application to: 1) switching regulator controller U13 and 2) a fault detection circuit. U13 will respond to the correction voltage by changing the duty cycle of the PWM drive signal to optical coupler U17. The switching regulator circuit will respond by changing the output voltage to a level required by the power control PWM signal.
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## 1-38. FAULT DETECTION.

1-39. A fault detection circuit monitors the regulator for four conditions: 1) over-voltage, 2) open-loop, 3) over-current, and 4) over temperature. Over-voltage conditions are monitored by U23A. U23A compares a sample of the B+ leg to a reference voltage. When the B+ sample exceeds the reference voltage, the output of U23A will go LOW. The LOW is routed to fault detector latch U21A/U21B. Open-loop conditions are monitored by U23B. U23B compares a correction voltage sample to a reference voltage. When the correction voltage sample exceeds the reference, the output of U23B will go LOW. The LOW is inverted at U21D and applied to NAND gate U21C. With a HIGH power supply enable signal from U12C, U21C will output a LOW to fault detector latch U21A/U21B.

1-40. Over-current conditions are monitored by transistors Q19 and Q20. When an over-current condition occurs, Q19 and Q20 will output a LOW. The LOW is routed to fault detector latch U21A/U21B. Over-temperature conditions are monitored by temperature sensor U25. When the power supply temperature exceeds 72 degrees C, U25 will output a LOW through transistor Q25 to U21D. The LOW is inverted at U21D and applied to NAND gate U21C.

1-41. With a LOW from U21C or U23A, latch U21A/U21B will: 1) output a HIGH to transistor Q16 and 2) output a LOW to transistor Q15 and to U12B. Transistor Q16 will be biased on and will output a LOW to enable optical coupler U11. U11 will respond by generating a power supply fault signal. AND gate U12B will output a LOW to: 1) disable regulator controller U13, 2) disable the SCR controlled rectifier circuit, and 3) initiate a logic sequence to enable the crowbar circuit (refer to the following text). Transistor Q15 will be biased off and will disable optical coupler U10. The output of U10 will open.

1-42. The output of U10 is connected in parallel with U10 on each power supply circuit board. When the output of U10 on each power supply circuit board is open, a HIGH power supply emergency signal to be applied to the controller. The power supply emergency signal indicates all power supply modules contain fault conditions.

1-43. CROWBAR CIRCUIT.
1-44. The power supply circuit board is equipped with a crowbar circuit to discharge the B supply during power supply off, ac off, and power supply mute conditions. The crowbar circuit consists of: 1) crowbar MOSFET Q23 and 2) resistor R72. Control of the circuit is provided by logic gates which monitor power supply off, ac off, and power supply mute conditions.

1-45. During a power supply off, ac off, or power supply mute condition, AND gate U12A will output a LOW to U12B. With a HIGH from U21A/U21B, U12B will output a LOW to transistor Q12. The LOW biases Q12 and optical coupler U15 off. As a result, a HIGH is applied to the gate of crowbar MOSFET Q23. The HIGH biases Q23 on to short the B supply and discharge capacitors C24, C25, C26, C27 and C55. Resistor R72 limits the current during shorting operations.

1-46. When U15 is biased off, optical coupler U14 will also be disabled. With U14 disabled, a LOW is applied to U12C. U12C will output a LOW to disable the PWM drive to the switching regulator circuit.

## 1-47. POWER SUPPLY CIRCUIT GROUNDS.

1-48. The power supply circuit board is equipped with three isolated circuit grounds: 1) 0 VS , 2) 0 VP , and 3$) 0 \mathrm{VI}$. The circuit grounds are at different potentials and are not referenced to earth ground. The 0VS ground is the circuit ground for the: 1) SCR controlled bridge rectifier circuit, 2) soft-start control circuit, 3) ac line voltage detector circuit, and 4) lowvoltage detection circuit. The 0 VP circuit ground is used to create the negative leg of the B supply. The 0VI ground is the circuit ground for the: 1) crowbar circuit, 2) switching regulator circuit, 3) inverting drive buffers, and 4) switching regulator transistors. The circuit grounds are used in association with the circuitry to generate the operating voltages for the RF power modules.

# SECTION II POWER SUPPLY CIRCUIT BOARD MAINTENANCE 

## 2-1. INTRODUCTION.

2-2. This section provides maintenance information for the AM-10A/AM-6A transmitter power supply circuit board assembly.

2-3. SAFETY CONSIDERATIONS.
warning
THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS
WARNING WITH RESPECT TO THE CABINET WHICH IS AT earth potential. do not energize the TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.


#### Abstract

2-4. The AM-10A/AM-6A transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents. $2-5$. In addition to high voltages and currents, the transmitters contain multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.


2-6. FIRST LEVEL MAINTENANCE.
2-7. First level maintenance consists of precautionary procedures applied to the equipment to prevent future failures. The procedures are performed on a regular basis and the results recorded in a performance log.

2-8. CLEANING AND INSPECTION.

## WARNING

2-9. Ensure all transmitter primary power is disconnected and clean a circuit board of
accumulated dust as required using a nylon bristle brush and vacuum cleaner. Inspect
the circuit board for improperly seated semiconductors and components damage by
overheating. In addition, inspect the circuit board for loose hardware. Repeat the
procedure for each power supply circuit board in the transmitter.

2-10. SECOND LEVEL MAINTENANCE.
2-11. Second level maintenance is the performance of procedures required to restore a power supply circuit board to operation after a fault has occurred. The power supply circuit board contains no adjustments. Therefore, the following text presents only troubleshooting procedures.

2-12. TROUBLESHOOTING.
WARNING
WARNING
WARNING
WARNING
THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

2-13. SAFETY CONSIDERATIONS. The AM-10A/AM-6A transmitters are equipped with extensive indicator and meter circuitry to allow the operator to isolate problems to a specific area within the transmitter. Due to the hazardous voltages and currents contained in the equipment, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.

2-14. REMOVING/INSTALLING A POWER SUPPLY CIRCUIT BOARD. A power supply circuit board is removed by disconnecting three connectors, loosening the mounting hardware, and sliding the circuit board from the mounting pins. To remove or install a power supply circuit board, proceed as follows:

DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.
$2-15$. Disconnect all transmitter primary power.
2-16. To remove a power supply circuit board, proceed as follows:

1. Refer to Figure $5-2 / 5-3$ in SECTION V, MAINTENANCE and locate the desired power supply circuit board to be removed.

2. Disconnect connectors P1, P2, and P3 on the circuit board assembly.
3. Loosen the power supply circuit board mounting hardware.
4. Lift the circuit board from the mounting pins and remove the circuit board from the cabinet.

2-17. TROUBLESHOOTING PROCEDURES. The power supply module troubleshooting procedures are presented in Table 2-1. During the execution of the troubleshooting information, perform all the procedures for a symptom. The symptom may contain multiple component failures. Once the trouble is isolated, refer to the circuit board theory of operation and schematic diagrams to assist in problem resolution.

TABLE 2-1. POWER SUPPLY MODULE TROUBLESHOOTING
(Sheet 1 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| 1. RED POWER SUPPLY INDICATION | 1. Check for an over-temperature condition by inspecting the fans and filter. <br> 2.. Check transistors Q21 and Q22 as follows: <br> A. Using a digital voltmeter, operate the voltmeter to diode check. On Q21, place the negative lead on the drain (center pin) and the positive lead on the source. <br> 1. If the voltmeter indicates a non-shorted condition, check transistor Q23. <br> 2. If the voltmeter indicates a shorted condition, proceed as follows: <br> a. On Q21, place the negative lead on the drain (center pin) and the positive lead on the gate and record the voltmeter indication. <br> b. On Q22, place the negative lead on the drain and the positive lead on the gate and record the voltmeter indication. <br> c. The transistor with the lowest voltage is defective. <br> 2. Place the negative lead on the drain of Q21 and the positive lead on the source and determine if a short circuit condition is present. <br> 3. If a short circuit condition is present, defective Q21. <br> B. Repeat the procedure for transistor Q22. <br> 3. Check transistor Q23 as follows: <br> A. Using a digital voltmeter, operate the voltmeter to diode check and troubleshoot transistor Q23 as follows: <br> 1. Place the negative lead on the drain and the positive lead on the gate and determine if a short circuit condition is present. |

TABLE 2-1. POWER SUPPLY MODULE TROUBLESHOOTING
(Sheet 2 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| RED POWER SUPPLY <br> INDICATION (CONT"D) | 2. Place the negative lead on the drain <br> and the positive lead on the source and <br> determine if a short circuit condition is <br> present. <br> 3. If a short circuit condition is present, <br> defective Q23. |
|  | 3. Visually inspect crowbar resistor R72. <br> 4. Check SCRs D13/D14 and diodes D15, D16, and D17 <br> for a short circuit condition. |
|  | 5. Replace all blown fuses on the circuit board. <br> 1. Check for a 120 Hz square-wave pulse at the <br> source of transistor Q55 on the controller circuit |
| board. |  |
| A. If a 120 Hz signal is present, defective Q55 on |  |
| the controller circuit board. |  |
|  | B. If a 120 Hz signal is not present, defective U3 |
| on the power supply circuit board. |  |

2-18. COMPONENT REPLACEMENT PROCEDURE. Component replacement procedures for the power supply circuit board are presented in PART I SECTION V. Refer to COMPONENT REPLACEMENT in SECTION V as required for the replacement procedures.

# SECTION III POWER SUPPLY CIRCUIT BOARD PARTS LIST 

3-1. INTRODUCTION.
3-2. This section provides descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance of the power supply circuit board. Each table entry in this section is indexed by reference designators appearing on the applicable schematic.

TABLE 3-1. REPLACEABLE PARTS LIST INDEX

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :--- | :--- | :--- | :--- |
| $3-2$ | Power Supply Panel Assembly | $957-0315$ | $3-2$ |
| $3-3$ | Power Supply Circuit Board Assembly | $917-0315-001$ | $3-2$ |
| $3-4$ | Power Supply Panel Harness, AM-10A | $947-0189$ | $3-9$ |
| $3-5$ | Power Supply Capacitor Circuit Board Assembly | $917-0315-004$ | $3-9$ |
| $3-6$ | Power Supply Bulk Capacitor Circuit Board Assembly | $917-0315-002$ | $3-9$ |

TABLE 3-2. POWER SUPPLY PANEL ASSEMBLY - 957-0315

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| L1 | Choke, 3.6 MH, AM XMTR | 370-2363 | 1 |
| L2 | Choke, 1.04 uH , AM XMTR | 370-2364 | 1 |
| T1 | Transformer, Power Supply, Primary: 220 V ac $50 / 60 \mathrm{~Hz}$ <br> Secondary: 1. 20.0V @ .04A <br> 2. 18.0V @.01A <br> 3. 18.0V @.40A <br> 4. $15.5 \mathrm{~V} @ .25 \mathrm{~A}$ <br> 5. 31.0V @ 3.0A | 376-0047 | 1 |
| ---- | RFI Filter, 30VB6, 30A, 120VAC, $50 / 60 \mathrm{~Hz}$ | 339-0024 | 1 |
| ---- | Pin Connector | 417-0036 | 2 |
| ---- | Pins, Connector | 417-0053 | 10 |
| --- | Connector Housing, 2-Pin, Male | 418-0702 | 1 |
| --- | Plug, Connector Housing, 12-Pin | 418-1271 | 1 |
| -- | Blank, Power Supply AC Input Circuit Board | 517-0315-006 | 1 |
| --- | Power Supply Circuit Board Assembly, AM-1A | 917-0315-001 | 1 |
| -- | Power Supply Bulk Capacitor Circuit Board Assembly, AM-1A | 917-0315-002 | 1 |
| --- | Power Supply Capacitor Circuit Board Assembly, AM-1A | 917-0315-004 | 1 |
| ---- | Power Supply Harness | 947-0189 | 1 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001 (Sheet 1 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| C1 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C2 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | $003-1013$ | 1 |
| C3 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%, 200 \mathrm{~V}$ | $030-1033$ | 1 |
| C4 | Capacitor, Electrolytic, $2200 \mathrm{uF}, 35 \mathrm{~V}$ | $014-2293$ | 1 |
| C5, C6 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 2 |
| C7, C8 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF}, \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 2 |
| C9 | Capacitor, Electrolytic, $10 \mathrm{uF}, 50 \mathrm{~V}$ | $023-1076$ | 1 |
| C10 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | $003-1013$ | 1 |
| C11 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%, 200 \mathrm{~V}$ | $030-1033$ | 1 |
| C12 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C13, C14 | Capacitor, Electrolytic, $10 \mathrm{uF}, 50 \mathrm{~V}$ | $023-1076$ | 2 |
| C15 | Capacitor, Electrolytic, $470 \mathrm{uF}, 50 \mathrm{~V}$ | $024-4783$ | 1 |
| C16 | Capacitor, Electrolytic, $100 \mathrm{uF}, 35 \mathrm{~V}$ | $023-1084$ | 1 |
| C17 | Capacitor, Monolythic Ceramic, $.47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-4743$ | 1 |
| C18, C19 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 2 |
| C20 | Capacitor, Electrolytic, $2200 \mathrm{uF}, 35 \mathrm{~V}$ | $014-2293$ | 1 |
| C21 | Capacitor, Electrolytic, $27000 \mathrm{uF} \pm 20 \%, 50 \mathrm{~V}$ | $020-2795-500$ | 1 |
| C22 | Capacitor, Polyester, $.15 \mathrm{uF} \pm 10 \%, 600 \mathrm{WV}$ dc | $030-1523$ | 1 |
| C23 | Capacitor, Polypropylene Film, $.47 \mathrm{uF} \pm 10 \%, 600 \mathrm{~V}$ | $033-4763$ | 1 |
| C29 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |

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TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001 (Sheet 2 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C30, C31 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 2 |
| C32 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C33 | Capacitor, Electrolytic, $10 \mathrm{uF}, 50 \mathrm{~V}$ | 023-1076 | 1 |
| C34 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C35 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 1 |
| C36 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C37 | Capacitor, Monolythic Ceramic, . $0027 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-2723 | 1 |
| C38 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C39 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C40 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%$, 500 V | 040-1022 | 1 |
| C41 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%$, 50 V | 003-4743 | 1 |
| C42 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1013 | 1 |
| C43 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C44 | Capacitor, Electrolytic, $100 \mathrm{uF}, 35 \mathrm{~V}$ | 023-1084 | 1 |
| C45 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C46 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C47 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C49 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C50 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C52 | Capacitor, Polyester, 2.2 uF, 400V | 030-2256 | 1 |
| C56, C57 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 2 |
| C58 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF}, \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C59, C60 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1013 | 2 |
| C61 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C62 | Capacitor, Electrolytic, 10 uF, 35V | 023-1075 | 1 |
| C63 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C64 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1013 | 1 |
| C65, C66 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C67 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C68 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 1 |
| C69 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%$, 500 V | 040-1022 | 1 |
| C70 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C71 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 1 |
| C72 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C73 | Capacitor, Monolythic Ceramic, $0.0047 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-4723 | 1 |
| C74 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1013 | 1 |
| C75 thru C77 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%$, 50 V | 003-4743 | 3 |
| C78 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C79 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 1 |
| C80 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C81 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C82 | Capacitor, Electrolytic, $100 \mathrm{uF}, 35 \mathrm{~V}$ | 023-1084 | 1 |
| C83 | Capacitor, Monolythic Ceramic, $.47 \mathrm{uF} \pm 10 \% 50 \mathrm{~V}$ | 003-4743 | 1 |
| C84 | Capacitor, Ceramic, 0.001 uF $\pm 10 \%$, 200V | 030-1033 | 1 |
| C85 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001
(Sheet 3 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C86 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C91 thru C94 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 4 |
| C95 | Capacitor, Electrolytic, $10 \mathrm{uF}, 50 \mathrm{~V}$ | 023-1076 | 1 |
| C96 | Capacitor, Monolythic Ceramic, $0.0047 \mathrm{uF} \pm 5 \%$, 100V | 003-4723 | 1 |
| C98 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C99 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| D1 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 1 |
| D2, D3 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D4 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 1 |
| D5 , D6 | Diode, Zener, 1N4733A, $5.1 \mathrm{~V} \pm 5 \%$, 1W | 200-4733 | 2 |
| D7, D8 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D9 | Bridge Rectifier, NAE 3060A, 1 Amp, 200V | 239-0001 | 1 |
| D10 | Bridge Rectifier, MDA970A3, 4 Amps, 50-200V | 239-0003 | 1 |
| D11 | Bridge Rectifier, MDA970A3, 4 Amps , 50-200V | 239-0003 | 1 |
| D12 | Bridge Rectifier, NAE 3060A, 1 Amp, 200V | 239-0001 | 1 |
| D13, D14 | Silicon Controlled Rectifiers, 2N6508, 25 Amperes, 600V | 237-6508 | 2 |
| D15 | Rectifier, MR2406, 24 Amperes, 600V | 230-0015 | 1 |
| D16 | Power Rectifier, Switchmode, MUR4100E, 4 Amperes, 1000V | 230-0017 | 1 |
| D17 | Rectifier, MR2406, 24 Amperes, 600V | 230-0015 | 1 |
| D18 | Diode, Zener, 1N4733A, 5.1V $\pm 5 \%$, 1W | 200-4733 | 1 |
| D19 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| $\begin{aligned} & \text { D20 thru } \\ & \text { D22 } \end{aligned}$ | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 3 |
| D23 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D24 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D25 | Bridge Rectifier, NAE 3060A, 1 Amp, 200V | 239-0001 | 1 |
| D26 | Diode, Zener, 1N4733A, 5.1V $\pm 5 \%$, 1W | 200-4733 | 1 |
| D27 | Diode, Zener, 1N4746, 18V $\pm 10 \%$, 1W | 200-4746 | 1 |
| D28 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D29 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D30, D31 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D32 | Rectifier, Fast Recovery, FEN30JP, 30 Amperes, 600V | 230-0013 | 1 |
| D34 | Power Rectifier, Switchmode, MUR4100E, 4 Amperes, 1000V | 230-0017 | 1 |
| D37 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D39 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D40 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D41, D42 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D43, D44 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D45 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| F1, F2 | Fuse, 30 Amperes, 125V, 1/4x1-1/4, Lead Type | 334-0030-001 | 2 |
| J1 | Connector, Male, Printed Circuit Board Mount, PLB16M3N0A1 | 417-0376 | 1 |
| J2 | Receptacle, 12-Pin | 417-1276 | 1 |
| J3 | Connector, AMP 6405051-1, MR Printed Circuit Board, Male 24-Pin | 417-2401 | 1 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001
(Sheet 4 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| J4 | Receptacle, Male, 8-Pin In-Line, Right Angle | 417-0080-001 | 1 |
| J5 thru J7 | Connector, Header, 2-Pin | 417-4004 | 3 |
| J9, J10 | Receptacle, Male, 2-Pin In-line | 417-4004 | 2 |
| MOV1 | Varistor, V320LA40B | 140-0039 | 1 |
| MOV2 | Varistor, V320LA20AGE | 140-0038 | 1 |
| P4 thru P7 | Jumper, Programmable, 2-Pin | 340-0004 | 4 |
| Q1 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |
| Q2 | Transistor, 2N27000, FET, N-Channel, TO-92 Case | 210-7000 | 1 |
| Q3, Q4 | Transistor, 2N3906, PNP, Silicon, TO-92 Case | 210-3906 | 2 |
| Q5 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |
| Q6 | Transistor, 2N3906, PNP, Silicon, TO-92 Case | 210-3906 | 1 |
| Q7 | Transistor, 2N27000, FET, N-Channel, TO-92 Case | 210-7000 | 1 |
| Q8, Q9 | Transistor, 2N2222A, TO-18 Case | 210-2222 | 2 |
| Q10 thru Q13 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 4 |
| Q14 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 1 |
| Q15 thru Q18 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 4 |
| Q19, Q20 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 2 |
| Q21, Q22 | Transistor, Insulated Gate Bipolar, IRGPC50U, TO-247 Case | 210-4060 | 2 |
| Q23 | RF FET APT6018, 600V | 210-6018 | 1 |
| Q24 | Transistor, 2N27000, FET, N-Channel, TO-92 Case | 210-7000 | 1 |
| Q25 | Field Effect Transistor, J3100, RF, N-Channel, TO-92 Case | 212-0310 | 1 |
| Q26, Q27 | Transistor, 2N27000, FET, N-Channel, TO-92 Case | 210-7000 | 2 |
| Q28 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |
| R1 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R2 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R3, R4 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R5 | Resistor, 150 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1561 | 1 |
| R6 | Resistor, $21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2105 | 1 |
| R7 | Resistor, 6.34 k Ohm $\pm 1 \%$, 1/4W | 103-6344 | 1 |
| R8 | Resistor, 499 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4996 | 1 |
| R9 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R10 thru R12 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R13 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R14 | Resistor, $20.0 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2051 | 1 |
| R15 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R16 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R17 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R18 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R19 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R20 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R21 | Resistor, 866 Ohm $\pm 1 \%$, 1/4W | 103-8663 | 1 |
| R22, R23 | Resistor, $1.10 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1104 | 2 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001
(Sheet 5 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R24 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R25 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R26 | Resistor, 5.11 k Ohm $\pm 1 \%$, 1/4W | 103-5141 | 1 |
| R27 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R28 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R29, R30 | Resistor, $3.32 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3324 | 2 |
| R31 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R32 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R33 | Resistor, 665 Ohm $\pm 1 \%$, 1/4W | 103-6653 | 1 |
| R34 | Resistor, 499 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4996 | 1 |
| R35 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R36 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R37, R38 | Resistor, $82 \mathrm{Ohm} \pm 5 \%, 2 \mathrm{~W}$ | 130-8223 | 2 |
| R39, R40 | Resistor, 270 Ohm $\pm 5 \%$, 1/2W | 110-2733 | 2 |
| R41, R42 | Resistor, 47 Ohm $\pm 5 \%, 2 \mathrm{~W}$ | 130-4723 | 2 |
| R41, R42 | Resistor, $68 \mathrm{Ohm} \pm 5 \%, 2 \mathrm{~W}$ | 132-6832 | 2 |
| R43 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R44 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R45 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R46 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R47 | Resistor, $1.10 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1104 | 1 |
| R48, R49 | Resistor, 47 Ohm $\pm 5 \%$, 2W | 130-4723 | 2 |
| R52 | Resistor, 2.21 k Ohm $\pm 1 \%$, 1/4W | 103-2241 | 1 |
| R53 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R54 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R55 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R56 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R57 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R58 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R59 | Resistor, 1.33 k Ohm $\pm 1 \%$, 1/4W | 103-1331 | 1 |
| R60, R61 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| R62 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R63 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R64 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R65 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R66 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R67, R68 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R69 | Resistor, 100 Ohm $\pm 1 \%$, 1/4W | 100-1031 | 1 |
| R70 | Resistor, $866 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8663 | 1 |
| R71 | Resistor, 100k Ohm $\pm 5 \%$, 2W | 130-1062 | 1 |
| R72 | Resistor, $12 \mathrm{Ohm} \pm 20 \%$, 30W | 130-1225 | 1 |
| R73 | Resistor, 34.8 k Ohm $\pm 1 \%$, 1/4W | 103-3485 | 1 |
| R74 | Resistor, 39.2 k Ohm $\pm 1 \%$, 1/4W | 100-3951 | 1 |
| R75 | Resistor, 39.2 k Ohm $\pm 1 \%$, 1/4W | 100-3951 | 1 |
| R76 | Resistor, $1.10 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1104 | 1 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001

## (Sheet 6 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R77 thru R79 | Resistor, 1.33 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1331 | 3 |
| R80 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R81 | Resistor, 393 Ohm $\pm 5 \%$, 1/2W | 110-3933 | 1 |
| R82, R83 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 2 |
| R84 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R85 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R86 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1331 | 1 |
| R87 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R88 | Resistor, 1.33 k Ohm $\pm 1 \%$, 1/4W | 103-1331 | 1 |
| R89 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R90 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R91 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R92 | Resistor, 88.7 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8872 | 1 |
| R93, R94 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 2 |
| R95 | Resistor, $13 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1305 | 1 |
| R96 | Resistor, $3.32 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3324 | 1 |
| R97 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R98 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R99 | Resistor, $33.2 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3325 | 1 |
| R100, R101 | Resistor, 5.11 k Ohm $\pm 1 \%$, 1/4W | 103-5141 | 2 |
| R102, R103 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 2 |
| R104 | Resistor, $3.32 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3324 | 1 |
| $\begin{aligned} & \text { R105 thru } \\ & \text { R107 } \end{aligned}$ | Resistor, 0.1 Ohm $\pm 1 \%$, 10W, WW | 130-1010 | 3 |
| R108 | Resistor, 475 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4753 | 1 |
| R109 | Resistor, $162 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1631 | 1 |
| R110 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R111 thru | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 7 |
| R117 |  |  |  |
| R118 | Resistor, $39.2 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-3951 | 1 |
| R119 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R120, R121 | Resistor, 1 k Ohm $\pm 1 \%$, 1/4W | 100-1041 | 2 |
| R122 | Resistor, $150 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1531 | 1 |
| R123 | Resistor, 82.5 Ohm $\pm 1 \%$, 1/4W | 103-8251 | 1 |
| R124 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R125 | Resistor, $249 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2496 | 1 |
| R126 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R127 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R130 | Resistor, $6.8 \mathrm{k} \mathrm{Ohm} \pm 5 \%, 1 / 2 \mathrm{~W}$, | 110-6843 | 1 |
| R134, R135 | Resistor, 0.1 Ohm $\pm 1 \%$, 10W, WW | 130-1010 | 2 |
| R137, R138 | Resistor, $82 \mathrm{Ohm} \pm 5 \%, 2 \mathrm{~W}$ | 130-8223 | 2 |
| R140 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R141 | Resistor, 48.7 k Ohm $\pm 1 \%$, 1/4W | 103-4875 | 1 |
| R143 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R144 | Resistor, $5.11 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-5141 | 1 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001
(Sheet 7 of 8)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R146 | Resistor, $39.2 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-3951 | 1 |
| R147 | Resistor, 150 k Ohm $\pm 1 \%$, 1/4W | 103-1561 | 1 |
| R148 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R149, R150 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$, | 100-1041 | 2 |
| R151 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R152 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R153 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R154 | Resistor, 249 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2493 | 1 |
| RT1 | Thermistor, 100 Ohms $\pm 20 \%$ | 140-0030 | 1 |
| TP1 thru <br> TP12, TP14 | Terminal, Test Point, Oval, Red | 413-0106 | 13 |
| U1, U2 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo <br> Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 2 |
| U3, U4 | Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 V to 37 V , 1.5 Ampere, TO-220 Case | 227-0317 | 2 |
| U5 | Integrated Circuit, MC14538B, Dual Retriggerable, Resettable Monostable Multivibrator, CMOS, 16-Pin DIP | 228-4538 | 1 |
| U6 | Voltage Comparator, LM393N, 8-Pin DIP | 221-0393 | 1 |
| U7 | Integrated Circuit, TL311P, JFET-Input Differential Comparator, 8-Pin DIP | 220-0311 | 1 |
| U8 thru U11 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo <br> Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 4 |
| U12 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U13 | Integrated Circuit, SG3525AN, PWM Control | 228-3525 | 1 |
| U14, U15 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo <br> Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 2 |
| U16 | Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 V to 37 V , 1.5 Ampere, TO-220 Case | 227-0317 | 1 |
| U17 | Integrated Circuit, Opto-Isolator, 6N137, 8-Pin DIP | 220-6137 | 1 |
| U19 | Integrated Circuit, Driver, Mosfet, TSC4429CAT, 5-Pin, TO-220 Case, Inverting | 220-4429 | 1 |
| U21 | Integrated Circuit, MC14093B, Quad 2-Input NAND Schmitt Trigger, CMOS, 14-Pin DIP | 220-4093 | 1 |
| U22 | Integrated Circuit, Opto-Isolator, 6N137, 8-Pin DIP | 220-6137 | 1 |
| U23 | Voltage Comparator, LM393N, 8-Pin DIP | 221-0393 | 1 |
| U24 | Integrated Circuit, TLO74CN, Quad JFET-Input Operational Amplifier, 14-Pin DIP | 221-0074 | 1 |
| U25 | Temperature Sensor Chip, TMP01FP, 8-Pin DIP | 229-1750 | 1 |
| XU1, XU2 | Socket, 6-Pin DIP | 417-0600 | 2 |
| XU5 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU6, XU7 | Socket, 8-Pin DIP | 417-0804 | 2 |
| $\begin{aligned} & \text { XU8 thru } \\ & \text { XU11 } \end{aligned}$ | Socket, 6-Pin DIP | 417-0600 | 4 |

TABLE 3-3. POWER SUPPLY CIRCUIT BOARD ASSEMBLY - 917-0315-001
(Sheet 8 of 8)

| REF. DES. |  | DESCRIPTION | PART NO. |
| :--- | :--- | :--- | :--- | QTY.

TABLE 3-4. POWER SUPPLY PANEL HARNESS - 947-0189

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Connector, FC112N2, Crimp Contact | $417-0372$ | 16 |
| --- | Connector, Female, PLB16F0000, Positronic | $417-0377$ | 1 |

TABLE 3-5. POWER SUPPLY CAPACITOR CIRCUIT BOARD ASSEMBLY - 917-0315-004

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C87 thru C90 | Capacitor, Electrolytic, $7200 \mathrm{uF}, 200 \mathrm{WVDC}$ | $014-7200$ | 4 |
| MOV3 | Metal Oxide Varistor, V130LA10A, 130V ac RMS, 10 Joules | $140-0006$ | 1 |
| ---- | Blank, Power Supply Capacitor Circuit Board, AM-1A | $517-0315-004$ | 1 |

TABLE 3-6. POWER SUPPLY BULK CAPACITOR CIRCUIT BOARD ASSEMBLY -917-0315-002

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C24 thru C27 | Capacitor, Electrolytic, $1500 \mathrm{uF}, 400 \mathrm{~V} \mathrm{dc}-450 \mathrm{~V}$ dc | $013-1500$ | 4 |
| C28 | Capacitor, Poly Film, $.47 \mathrm{uF}, 600 \mathrm{~V}, \mathrm{Oval}$ | $033-4763$ | 1 |
| R50 | Resistor, 100 k Ohm $\pm 5 \%, 2 \mathrm{~W}$ | $130-1062$ | 1 |
| R51 | Resistor, 36 Ohm $\pm 5 \%, 2 \mathrm{~W}$ | $130-3623$ | 1 |
| R129 | Resistor, $470 \mathrm{k} \mathrm{Ohm} \pm 5 \%, 1 / 2 \mathrm{~W}$ | $110-4763$ | 1 |
| ---- | Blank, Power Supply Bulk Capacitor Circuit Board, AM-1A | $517-0315-002$ | 1 |

## SECTION IV POWER SUPPLY CIRCUIT BOARD DRAWINGS

## 4-1. INTRODUCTION.

4-2. This section provides assembly drawings, wiring diagrams, and schematic diagrams as listed below for the Broadcast Electronics AM-10A/AM-6A power supply circuit board.

FIGURE

4-1 SCHEMATIC DIAGRAM, POWER SUPPLY CIRCUIT BOARD, SB917-0315-001/
-002/
-003/
-004/
-005
4-2 ASSEMBLY DIAGRAM, POWER SUPPLY CIRCUIT BOARD, AC917-0315-001/
-002/
-003/
-004/
-005





## TABLE OF CONTENTS

PARAGRAPH
SECTION I
1-1
1-3
1-5
1-6
1-9
1-16
1-18
1-20
1-22
1-23
1-26
1-27
1-29
SECTION II
2-1
2-3
2-6
2-8
2-10
2-12
2-13
2-15
2-16
2-17
2-18
SECTION III
3-1
SECTION IV

FIGURE
1-1
1-2

## RF POWER MODULE THEORY OF OPERATION

## Introduction <br> 1-1

General Description 1-1
Modulator Circuit Board 1-1
Modulator Circuit 1-1
Fault Detection Circuits 1-1
Power Supply 1-2
RF Amplifier Circuit Board 1-5
Pre-Driver Circuit 1-5
Driver Circuit 1-5
RF Amplifier Circuit 1-5
RF Drive Status Circuit 1-6
Fault Detector Circuit 1-6
Power Supply Circuit 1-6
RF POWER MODULE MAINTENANCE
Introduction 2-1
Safety Considerations 2-1
First Level Maintenance $\quad 2-1$
Cleaning and Inspection $\quad 2-1$
Second Level Maintenance $\quad 2-2$
Troubleshooting 2-2
Safety Considerations 2-2
RF Power Module Assembly Procedure 2-3
RF Power Module Exchange Program 2-3
Troubleshooting Procedures $2-3$
Component Replacement Procedure $2-3$
RF POWER MODULE PARTS LIST
Introduction 3-1
RF POWER MODULE DRAWINGS
Introduction 4-1
LIST OF ILLUSTRATIONS
TITLE
MODULATOR CIRCUIT BOARD
SIMPLIFIED SCHEMATIC
POWER AMPLIFIER CIRCUIT BOARD
SIMPLIFIED SCHEMATIC
LIST OF TABLES
TABLE
2-1
3-1

TITLE
RF POWER MODULE TROUBLESHOOTING
REPLACEABLE PARTS LIST INDEX

PAGE NO.

# SECTION I RF POWER MODULE THEORY OF OPERATION 

## 1-1. INTRODUCTION.

1-2. This section presents a general description of the Broadcast Electronics AM-10A/AM-6A transmitter RF power module.

## 1-3. GENERAL DESCRIPTION.

1-4. An RF power module is a plug-in assembly containing two RF amplifier circuit boards and a modulator circuit board. Each RF power module is designed to produce 1100 watts of RF power. The modular design of the RF power assemblies allow the modules to be removed from the transmitter for maintenance. The remaining power modules will provide power to maintain on-air operation. The following text presents a description of the RF power modules.

1-5. MODULATOR CIRCUIT BOARD.
1-6. MODULATOR CIRCUIT. The modulator circuit board is designed to convert the CMOS level PWM signal from the exciter circuit board into a dc voltage which varies at the audio modulation rate (refer to Figure 1-1). The duty cycle of the 122 kHz to 135 kHz PWM signal is $40 \%$ with no audio modulation. The duty cycle varies to allow modulation of the transmitter from $-100 \%$ to $+150 \%$. The PWM signal from the exciter circuit board is applied to integrated circuit U1. U1 is a high-speed optical coupler designed to provide isolation for the transition of the signal from the exciter circuit board ground system to the modulator circuit board ground system. The output of U1 is applied to level converter U11A. U11A converts the 5 volt signal to a 15 volt peak-to-peak signal. The output of U11A is applied to two MOSFET driver stages. A 9.7 volt dc bias signal is incorporated into the PWM signal by resistor R10, and zener diodes D17/D18.

1-7. Integrated circuits U2 and U13 are MOSFET driver stages. The outputs switch to: 1) a logic 1 at 2 volts and 2) a logic 0 at 0.8 volts. The output of U 2 is applied to the gate of forward converter transistor Q1. The output of U13 is applied to the gate of forward converter transistor Q2. Q1 and Q2 are switched on/off by the PWM signal. The transistors convert the 125 volt B- supply to approximately 50 volts with a nominal PWM duty cycle of $40 \%$. Catch diodes D2 and D3 clamps inductors L1 and L2 to prevent transistor damage from high switching voltages during transistor turn-off operations. A dc operating potential for Q1 and Q2 is provided by the B- supply from the power supply circuit board. Control of the B- leg is provided by relay K1. K1 immediately terminates the power supply during a power supply or modulator failure.

1-8. The output of transistors Q1 and Q2 are applied to an LC low-pass filter network consisting of: 1) inductor L1/L3 and capacitor C13 and 2) inductor L2/L3 and capacitor C14. The LC networks function with inductor L4 and capacitors C15/C16/C49 as a fifth-order Bessel low-pass filter designed to remove the 125 kHz frequency from the output signal. The output from L4/C15/C16/C49 is routed: 1) to a monitor circuit and 2) for application to the power amplifier circuit boards.

1-9. FAULT DETECTION CIRCUITS. The modulator circuitry is monitored for proper operation by four fault detection circuits. The fault detection circuits consist of: 1) a PWM drive detector, 2) a modulator fault detector, 3) a B+ supply fuse fault detector, and 4) a +20 volt power supply fault detector.

1-10. PWM Drive Fault Detector. A sample of the PWM drive signal from integrated circuit U2 is applied to comparator U3A. U3A compares the signal to a reference. When the PWM drive signal is present, the output of U3A will go HIGH. The HIGH is inverted at U5F. U5F will output a LOW to illuminate PWM drive indicator DS1. When the PWM drive signal is not present, the output of U3A will go LOW. The LOW is inverted at U5F. U5F will output a HIGH to extinguish PWM drive indicator DS1.
1-11. Modulator Fault Detector. A sample of the modulator circuit output is applied to comparator U3D. U3D compares the signal to a reference generated by a divider consisting of resistors R43 and R44. When the output signal from the modulator circuit is not present, the output of U3D will go LOW. The LOW is applied to a modulator status circuit (refer to the following text).
1-12. B+Supply Fuse Fault Detector. The B+ supply is protected from over-current conditions on the modulator circuit board by fuse F1. The status of F1 is monitored by a B+ supply fuse fault detector circuit. The circuit consists of optical couplers U4/U12 and comparator U3B. When the fuse has blown, the output of couplers U4/U12 will go HIGH. The HIGH is applied to comparator U3B. U3B compares the signal to a reference. The output of U3B will go HIGH. The HIGH is inverted at U5C. U5C will output a LOW: 1) to illuminate fuse indicator DS2 and 2) to a modulator status circuit.
1-13. B+ Power Supply Fault Detector. The status of the B+ supply is monitored by a B+ power supply fault detector circuit. The circuit consists of B+ power supply fault detector comparator U3C. U3C compares the power supply sample to a reference. When the B+ power supply sample is present, the output of U3C will be HIGH. The HIGH is applied to inverter U5E and NAND gate U6B of the modulator status circuit. U5E will output a LOW to enable power supply indicator DS3. When the B+ power supply sample is not present, the output of U3C will be LOW. The LOW is applied to inverter U5E and NAND gate U6B of the modulator status circuit. U5E will output a HIGH to disable power supply indicator DS3.
1-14. Modulator Status Circuit. The modulator status circuit consists of: 1) NAND gates U6A, U6B, U6C, and U6D, 2) latches U7A, U7B, and U7C, 3) inverters U5B, U5D and U5G, and 4) optical couplers U8 and U9. When a LOW from the modulator fault detector or the B+ supply fuse fault detector is applied to NAND gate U6A, U6A will output a HIGH to U6B. With a HIGH from power supply fault detector U3C, U6B will output a LOW to latches U7B, U7C, and U7A. Latch U7C will output a HIGH to inverter U5G. U5G will output a LOW to enable power supply mute optical coupler U9. U9 will output a LOW power supply mute command to the power supply circuit board. When the supply is muted, comparator U3C will respond by routing a LOW to U5E. U5E will output a HIGH to: 1) disable power supply indicator DS3 and 2) NAND gate U6C.
1-15. Latch U7B will output a HIGH to inverter U5D. U5D will output a LOW to: 1) illuminate modulator fault indicator DS4, 2) enable modulator fault detector optical coupler U8, and 3) NAND gate U6D. U6D will output a HIGH to latch U7D. Latch U7A will output a HIGH to NAND gate U6C. With a HIGH from U5E, U6C will output a LOW to latch U7D. U7D will output a LOW to U5B. U5B will respond by routing a HIGH to bias relay K1 on. Relay K1 is provided to immediately disconnect the forward converter transistors from the power supply during a modulator fault or high B+ supply conditions.
1-16. POWER SUPPLY. A +20 volt operating potential for the modulator circuit board is provided by the applicable power supply circuit board. The +20 volt supply is applied through fuse F2 to +15 volt regulator U10. Fuse F2 protects the +20 volt supply from over-current conditions.
1-17. U10 is a three-terminal adjustable positive regulator containing internal thermal overload protection and short-circuit current limiting features. Further protection for U10 is provided by diodes D8 and D9. D8 protects the regulator from a short circuit on the regulator input. D9 protects the regulator from a reverse polarity potential applied to the output. Capacitor C25 provides filtering for the +15 volt supply. A sample of the +15 supply is regulated into a +5 volt supply by zener diode D1.


## 1-18. RF AMPLIFIER CIRCUIT BOARD.

1-19. Each RF power module is equipped with two RF amplifier circuit boards: 1) power amplifier 1 and 2) power amplifier 2. The circuit boards are designed with Class E power amplifier circuitry. Each circuit board is designed to produce approximately 550 watts of RF power. Figure 1-2 presents the RF amplifier circuit board circuitry. The RF amplifier circuit boards are identical, therefore only power amplifier 1 will be explained.

1-20. PRE-DRIVER CIRCUIT. A +15 volt peak-to-peak square-wave signal at the carrier frequency is applied to a transformer on the power block motherboard assembly. The transformer outputs two signals to inverter U5A.

1-21. The output from U5A is applied through inverters U5B/U5C to high/low side driver U7 and U8. U7/U8 output high and low drive signals to driver circuit transistors Q3/Q5 and Q4/Q6.

1-22. DRIVER CIRCUIT. The driver circuit consists of: 1) transistors Q3 and Q5 and 2) Q4 and Q6. Q3/Q5 and Q4/Q6 are MOSFET transistors configured as a push-pull driver circuit. The outputs of Q3/Q5 and Q4/Q6 are applied to MOSFET power transistors Q1 and Q2. Operating potentials for the driver circuitry is provided by the RF driver +30 volt supply. The supply is protected from over-voltage conditions by a regulator Q7. The regulator limits the voltage to approximately 47 volts dc. Fuse F2 protects the +30 volt supply from over-current conditions. Fuse F3 protects the driver circuit components from over-current conditions.

1-23. RF AMPLIFIER CIRCUIT. The RF amplifier circuit consists of switching MOSFET transistors Q1 and Q2. Q1 and Q2 are configured as a Class E switching amplifier network. Class E power amplifier characteristics consist of: 1) the transistor drain-to-source voltage must be nominally zero immediately prior to the turn-on of the transistor and 2) the time slope of the drain-to-source voltage waveform must be nominally zero prior to the turn-on of the transistor. The Class E circuit results in: 1) reduced device dissipation and lowers the transistor operating temperature which greatly increases the life of the components, 2) an operating efficiency of $95 \%$ or greater, and 3 ) increased reliability when operated into VSWR conditions.

1-24. Additional characteristics of a Class E amplifier design is the application of dc power to the amplifier transistors. The B+ and B- supplies are applied to RF choke L1 on the combiner assembly. The choke is connected to the primary center tap winding of combiner transformer T1. The transistors are connected to the primary winding of the transformers. The B- supply for the power amplifier is provided by the modulator circuit board. The modulator outputs a dc voltage which varies with audio modulation and functions as the RF ground for transistors Q1 and Q2. The RF ground potential will change in response to the applied audio. Fuse F1 protects the power amplifiers from over-current conditions.

1-25. Transistors Q1 and Q2 operate together to generate approximately 550 watts of RF power. Q1 operates 180 degrees out-of phase with transistor Q2. Inductors L1 through L7 improve the efficiency of the drive circuit by storing the energy required to charge the input capacitance of the transistors. Transzorbs D9/D10 prevent the gates of Q1/Q2 from damage by transients during power on and off. Capacitors C 44 through C50 and C51 through C57 provide shaping for the Class E waveform. The RF power from power amplifier 1 is combined with the 550 watts of RF power from power amplifier circuit board 2 at a combiner transformer on the power block motherboard assembly to generate 1100 watts of RF power.

1-26. RF DRIVE STATUS CIRCUIT. The RF drive signal is monitored by an RF drive status circuit. When an RF drive signal is present, a sample of the RF drive signal is rectified by diodes D5/D6. The voltage from D5/D6 is applied to optical coupler U2. The output of U2 will go HIGH and bias transistor Q12 on. The output of Q12 will go LOW to illuminate RF drive status indicator DS1.

1-27. FAULT DETECTOR CIRCUIT. The power amplifier circuit board circuitry is monitored for fault conditions by a fault detector circuit. The circuit is designed to monitor two operations: 1 ) the +30 volt supply and 2 ) the modulator output voltage ( RF ground). The modulator output is monitored by optical coupler U3. The +20 volt supply is monitored by transistor Q11. The power amplifier is protected from over-current conditions by fuse F1. The +30 volt supply is protected from over-current conditions by fuse F2.

1-28. The fault detector functions by monitoring fuses F1 and F2. When fuse F2 is blown, transistor Q11 will output +20 volts to silicon-controlled-rectifier (SCR) Q13. When fuse F1 is blown, optical coupler U3 will output +20 volts to SCR Q13. When either voltage is present, the voltage will bias Q13 on to illuminate PA fault indicator DS2 and bias optical coupler U4 on. U4 will respond by routing a PA fault signal to the controller circuit board.

1-29. POWER SUPPLY CIRCUIT. An operating potential for the amplifier circuit board circuitry is provided by the +30 volt supply from the power supply circuit board. The supply is protected from over-current conditions by fuse F2. The +30 supply is regulated into a: 1) +15 volt supply by U1 and 2$)+20$ volt supply by R29. U1 is a three-terminal adjustable regulator containing internal thermal and short-circuit current limiting features. Fuse F2 protects the +30 volt supply from over-current conditions. Fuse F1 protects the power amplifier components from over-current conditions. Fuse F3 protects the driver circuit components from over-current conditions.



# SECTION II <br> RF POWER MODULE MAINTENANCE 

## 2-1. INTRODUCTION.

2-2. This section provides maintenance information for the AM-10A/AM-6A transmitter RF power modules.

## 2-3. SAFETY CONSIDERATIONS.

WARNING

WARNING
WARNING
WARNING

> THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUUPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

2-4. The AM-10A/AM-6A transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents.
$2-5$. In addition to high voltages and currents, the transmitters contain multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.

2-6. FIRST LEVEL MAINTENANCE.
2-7. First level maintenance consists of precautionary procedures applied to the equipment to prevent future failures. The procedures are performed on a regular basis and the results recorded in a performance log.

## $2-8$. CLEANING AND INSPECTION.

 ELECTRONICS INC2-9. Ensure all transmitter primary power is disconnected and remove an RF power module. Clean the module of accumulated dust as required using a nylon bristle brush and vacuum cleaner. Inspect the circuit boards for improperly seated semiconductors and components damage by overheating. In addition, inspect the module for loose hardware. Repeat the procedure for each module in the transmitter.
2-10. SECOND LEVEL MAINTENANCE.
2-11. Second level maintenance is the performance of procedures required to restore an RF power module to operation after a fault has occurred. The RF power modules contain no electrical adjustments. Therefore, the following text presents only troubleshooting procedures.
2-12. TROUBLESHOOTING.


WARNING
WARNING
WARNING
WARNING
THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT
GROUNDS WITH HIGH AC AND DC POTENTIALS
WITH RESPECT TO THE CABINET WHICH IS AT
EARTH POTENTIAL. DO NOT ENERGIZE THE
TRANSMITTER WITH TEST EQUIPMENT CON-
NECTED TO THE TRANSMITTER OUTPUT
NETWORK, RF POWER MODULE, RF COMBINER, OR
POWER SUPPLY COMPONENTS.

CAUTION
CAUTION

2-13. SAFETY CONSIDERATIONS. The AM-10A/AM-6A transmitters are equipped with extensive indicator and meter circuitry to allow the operator to isolate problems to a specific area within the transmitter. Due to the hazardous voltages and currents contained in the equipment, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.


2-14. The RF power modules are not designed to be removed from the cabinet with the power energized. Therefore, operate the transmitter to off before removing an RF power module from the cabinet for maintenance procedures.

2-15. RF POWER MODULE ASSEMBLY PROCEDURE. In the event of a failure in an RF power module, the module will be required to be disassembled. The module must be properly re-assembled to prevent circuit board and connector mis-alignment. To re-assemble an RF power module, proceed as follows:

1. Locate the PA 2 circuit board and install the hex standoffs in the four locations at the rear of the circuit board.
2. Locate the PA 1 circuit board and install the front panel mounting bracket using the four Phillips-head screws. Do not secure the screws at this time. Repeat the procedure for the PA2 circuit board and the modulator circuit board.
3. Install the PA 1 circuit board in the PA 1 location on the RF power module front panel. Secure the circuit board bracket to the front panel using the hex nuts. Repeat the procedure for the PA 2 and modulator circuit boards.
4. Place the RF power module on a square and flat surface such as a table with the top of the module facing up.
5. Place the module front panel flush with the edge of the table and align the circuit boards as follows:
A. Move the PA 1 circuit board until the front of the circuit board is flush with the RF module front panel and the top edge of the circuit board is straight.
B. Secure the two Phillips-head screws which mount the circuit board to the bracket.
C. Repeat the procedure for the PA 2 and modulator circuit boards.
6. Rotate the module and repeat the alignment procedure for the bottom circuit board bracket screws. Secure the two Phillips-head screws mounting the circuit board to the bracket when each circuit board is properly aligned.
7. Install the hardware securing the PA 1 circuit board and the modulator circuit board to the standoffs.

2-16. RF POWER MODULE EXCHANGE PROGRAM. If an RF power module is determined to be defective, Broadcast Electronics has established an RF power module exchange program. The program allows the customer to exchange a defective module for a re-conditioned module. Terms of the program are available from the Broadcast Electronics Customer Service Department. If an RF power module is determined to be defective, troubleshoot the module or contact the Broadcast Electronics Customer Service department for terms of the module exchange program.

2-17. TROUBLESHOOTING PROCEDURES. The RF power module troubleshooting procedures are presented in Table 2-1. During the execution of the procedures, perform all troubleshooting procedures for a symptom. The symptom may contain multiple component failures. Once the trouble is isolated, refer to the circuit board theory of operation and schematic diagrams to assist in problem resolution.

2-18. COMPONENT REPLACEMENT PROCEDURE. Component replacement procedures for the RF power modules are presented in PART I SECTION V. Refer to COMPONENT REPLACEMENT in SECTION V as required for the replacement procedures.

TABLE 2-1. RF POWER MODULE TROUBLESHOOTING
(Sheet 1 of 3)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| RF DRIVE INDICATOR <br> EXTINGUISHED OR FLICKERING <br> OR FAULT INDICATOR <br> ILLUMINATED | 1. Determine transistor reference voltages of a power amplifier with no faults as follows: <br> A. Remove an operational power amplifier with no faults from an RF power module. <br> B. Using a digital voltmeter, operate the voltmeter to diode check and determine a reference voltage for the transistors on the circuit board as follows: <br> 1. Place the negative lead on the drain of Q1 (center pin) and the positive lead on the gate and determine the voltage. The voltage using a Fluke 77 meter $=.45$. <br> 2. Place the negative lead on the drain of Q1 and the positive lead on the source and determine the voltage. The voltage using a Fluke 77 meter $=.45$. <br> 2. Using the voltmeter as described in the preceding step, measure the drain-to-gate and drain-to-source voltage of transistor Q1 on the defective power amplifier circuit board. <br> A. If the voltage is greater than $\pm 0.1$ volt of the reference, defective Q1, Q3, and Q5. <br> B. If the voltage is equal to the reference, repeat the preceding step for transistor Q2 on the defective power amplifier circuit board. <br> 3. Using a digital voltmeter, operate the voltmeter to diode check and troubleshoot transistor Q3 as follows: <br> A. Place the negative lead on the drain of Q3 (center pin) and the positive lead on the gate and determine if a short circuit condition is present. <br> B. Place the negative lead on the drain of Q3 and the positive lead on the source and determine if a short circuit condition is present. <br> C. If a short circuit condition is present, defective Q3. <br> 4. Repeat the procedure for transistors Q4, Q5, and Q6. <br> 5. Visually inspect regulator U1 for broken leads. <br> 6. Check and replace all blown fuses on the circuit board. |

TABLE 2-1. RF POWER MODULE TROUBLESHOOTING
(Sheet 2 of 3)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| MOD PWM DRIVE INDICATOR EXTINGUISHED AND FAULT OR FUSE INDICATOR ILLUMINATED <br> MOD PWM DRIVE INDICATOR EXTINGUISHED <br> FAULT OR FUSE INDICATOR ILLUMINATED | 1. Refer to RF DRIVE INDICATOR EXTINGUISHED OR FLICKERING OR FAULT INDICATOR ILLUMINATED in the preceding text and troubleshoot the power amplifier circuit board. <br> 2. If no defective circuitry is located on the power amplifier circuit board, refer to FAULT OR FUSE INDICATOR ILLUMINATED in the following text and troubleshoot the modulator circuit board. <br> 1. Defective U2 or U13 on the modulator circuit board. <br> 1. Visually inspect regulator U 10 for broken leads. <br> 2. Determine transistor reference voltages of a modulator circuit board with no faults as follows: <br> A. Remove a modulator with no faults from an RF power module. <br> B. Using a digital voltmeter, operate the voltmeter to diode check and determine a reference voltage for the transistors on the circuit board as follows: <br> 1. Place the negative lead on the drain of Q1 (center pin) and the positive lead on the gate and determine the voltage. The voltage using a Fluke 77 meter $=1.2 \mathrm{~V}$. <br> 2. Place the negative lead on the drain of Q1 and the positive lead on the source and determine the voltage. The voltage using a Fluke 77 meter $=.46 \mathrm{~V}$. <br> 3. Using the voltmeter as described in the preceding step, measure the drain-to-gate and drain-to-source voltage of transistor Q1 on the defective modulator circuit board. <br> A. If the voltage is greater than $\pm 0.1$ volt of the reference, proceed as follows: <br> 1. Remove the wire from terminal E1. <br> 2. Using the voltmeter as described in the preceding text, measure the drain-to-gate and drain-to-source voltage of transistor Q1 on the defective modulator circuit board. <br> B. If the voltage at Q1 is greater than $\pm 0.1 \mathrm{~V}$ of the reference, defective Q1. <br> C. If the voltage at Q1 is equal to the reference, defective Q2. |

TABLE 2-1. RF POWER MODULE TROUBLESHOOTING (Sheet 3 of 3)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| FAULTT OR FUSE INDICATOR | 4. Replace all blown fuses on the circuit board. |
| ILLUMINATED (CONT'D) | 5. Re-install the modulator circuit board and install |
|  | the RF module in the transmitter. If the |
|  | modulator remains defective, replace U2 and U13. |
|  | 6. If the modulator remains defective, contact the |
|  | Broadcast Electronics Customer Service |
|  | Department. |
|  |  |

# SECTION III RF POWER MODULE PARTS LIST 

## 3-1. INTRODUCTION.

3-2. This section provides descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance of the RF Power Module. Each table entry in this section is indexed by reference designators appearing on the applicable schematic.

TABLE 3-1. REPLACEABLE PARTS LIST INDEX

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :--- | :--- | :--- | :--- |
| $3-2$ | Power Module Assembly | $957-0010-001$ | $3-2$ |
| $3-3$ | Modulator Circuit Board Assembly | $917-0302$ | $3-2$ |
| $3-4$ | Power Amplifier Circuit Board Assembly | $917-0304$ | $3-5$ |
| $3-5$ | Power Module Frequency Dependant Kit, $522-650 \mathrm{kHz}$ | $957-1015-001$ | $3-8$ |
| $3-6$ | Power Module Frequency Dependant Kit, $651-770 \mathrm{kHz}$ | $957-1015-002$ | $3-8$ |
| $3-7$ | Power Module Frequency Dependant Kit, $771-920 \mathrm{kHz}$ | $957-1015-003$ | $3-8$ |
| $3-8$ | Power Module Frequency Dependant Kit, $921-1080 \mathrm{kHz}$ | $957-1015-004$ | $3-8$ |
| $3-9$ | Power Module Frequency Dependant Kit $1081-1300 \mathrm{kHz}$ | $957-1015-005$ | $3-9$ |
| $3-10$ | Power Module Frequency Dependant Kit $1301-1580 \mathrm{kHz}$ | $957-1015-006$ | $3-9$ |
| $3-11$ | Power Module Frequency Dependant Kit, $1581-1700 \mathrm{kHz}$ | $957-1015-007$ | $3-9$ |

TABLE 3-2. POWER MODULE ASSEMBLY - 957-0010-001

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| ---- | Modulator Circuit Board Assembly | $917-0302$ | 1 |
| ---- | Power Amplifier Circuit Board Assembly | $917-0304$ | 2 |

## TABLE 3-3. MODULATOR CIRCUIT BOARD ASSEMBLY - 917-0302 (Sheet 1 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C1 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C2 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 1 |
| C3 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |
| C4 | Capacitor, Monolythic Ceramic $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 1 |
| C5 | Capacitor, Electrolytic, 330 uF, 200 V dc | 013-3385-201 | 1 |
| C6 | Capacitor, Polypropylene Film, $47 \mathrm{uF}, 250 \mathrm{~V}$, Oval | 033-4743 | 1 |
| C7 | Capacitor, Mica, $1000 \mathrm{pF} \pm 10 \%, 350 \mathrm{~V}$ | 046-0002 | 1 |
| C8 | Capacitor, Electrolytic, 330 uF, 200 V dc | 013-3385-201 | 1 |
| C9 | Capacitor, Polypropylene Film, $47 \mathrm{uF}, 250 \mathrm{~V}$, Oval | 033-4743 | 1 |
| C10 | Capacitor, Mica, $1000 \mathrm{pF} \pm 10 \%, 350 \mathrm{~V}$ | 046-0002 | 1 |
| C11, C12 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 2 |
| C13, C14 | Capacitor, Polypropylene Film, 2.2 uF, 400V | 030-2256 | 2 |
| C15, C16 | Capacitor, Metallized Polypropylene Film, . 068 uF $\pm 10 \%$, 250V | 030-6843 | 2 |
| C17 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 1 |
| C18, C19 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 2 |
| C20 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | 003-1041 | 1 |
| C21 | Capacitor, Ceramic, 0.001 uF $\pm 10 \%$, 200V | 030-1033 | 1 |
| C22 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C23 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |
| C24 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C25 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |
| C26, C27 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 2 |
| C28 thru C32 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 5 |
| C33 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | 003-1041 | 1 |
| C34 | Capacitor, Electrolythic, $47 \mathrm{uF}, 35 \mathrm{~V}$ | 020-4773 | 1 |
| C35 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C36, C37 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 2 |
| C38, C39 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 2 |
| C40 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C41 | Capacitor, Electrolytic, 33 uF, 25V | 020-3374 | 1 |
| C42 | Capacitor, Polypropylene Film, 2.2 uF, 400V | 030-2256 | 1 |
| C43 | Capacitor, Polypropylene Film, $.47 \mathrm{uF}, 250 \mathrm{~V}$, Oval | 033-4743 | 1 |
| C44 | Capacitor, Polypropylene Film, . 033 uF, $\pm 10 \%$, 200V | 030-3353 | 1 |
| C45 | Capacitor, Mica, $820 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 042-8222 | 1 |
| C46, C47 | Capacitor, Monolythic Ceramic, . $1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 2 |
| C48 | Capacitor, Metallized Polypropylene Film, . 068 uF $\pm 10 \%$, 250V | 030-6843 | 1 |

TABLE 3-3. MODULATOR CIRCUIT BOARD ASSEMBLY 917-0302
(Sheet 2 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C49 | Capacitor, Polypropylene Film, . $033 \mathrm{uF} \pm 10 \%$, 200V | 030-3353 | 1 |
| C50 | Capacitor, Mylar, $0.01 \mathrm{uF} \pm 10 \%$, 100V | 031-1043 | 1 |
| D1 | Diode, Zener, 1N4733A, $5.1 \mathrm{~V} \pm 5 \%$, 1W | 200-4733 | 1 |
| D2, D3 | Diode, Fast Recovery, 16JPF20 | 200-1620 | 2 |
| D4 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D5 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D6 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D7 | Diode, Zener, 1N4739A, 9.1V $\pm 5 \%$, 1W | 200-0009 | 1 |
| D8, D9 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D10 | Diode, 1N6276A, Silicon, Transient Voltage Suppressor, $16 \mathrm{~V} \pm 0.05 \%$ Breakdown | 206-6276 | 1 |
| D11 | Switchmode Power Rectifier, MUR460 | 230-0014 | 1 |
| D12, D13 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D14, D15 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D16 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D17 | Diode, Zener, 1N4739A, 9.1V $\pm 5 \%$, 1W | 200-0009 | 1 |
| D18 | Diode, Zener, 1N4728, 3.3V $\pm 5 \%$, 1W | 201-4728 | 1 |
| D19 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D20 thru D23 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 4 |
| D24,D25 | Diode, 1N5817, Schottky, 20V @ 1 Amperes | 200-0019 | 2 |
| DS1 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 1 |
| DS2 | Indicator, LED, Red, 521-9212, 1.7V @ 50 mA Maximum | 323-9217 | 1 |
| DS3 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 1 |
| DS4 | Indicator, LED, Red, 521-9212, 1.7V @ 50 mA Maximum | 323-9217 | 1 |
| F1 | Fuse, 3AG, 20 Amperes, 250V | 330-2000 | 1 |
| F2 | Fuse, AGC, 1 Ampere, MDL, 250V, Slow-Blow | 334-0100 | 1 |
| J3, J4 | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| K1 | Relay, SPST, 30 Amperes | 270-1213 | 1 |
| P2 | Connector, 15-Pin, SUB-D, Male, Right Angle | 417-0374 | 1 |
| P3 | Receptacle, Male, 3-Pin In-line | 417-0003 | 1 |
| P4 | Receptacle, Male, 2-Pin In-line | 417-4004 | 1 |
| Q1, Q2 | Modulator, FET MTY55N20E, 200V, 55 Amperes | 210-0550 | 2 |
| R1 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R2 | Resistor, 470 Ohm $\pm 5 \%$, 1/2W | 110-4733 | 1 |
| R3 | Resistor, $332 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3323 | 1 |
| R4 | Resistor, $1 \mathrm{Ohm} \pm 5 \%$, 1/4W | 100-1013 | 1 |
| R5 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R7 | Resistor, 12k Ohm, 2W, $\pm 5 \%$ | 130-1253 | 1 |
| R8 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R9 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R10 | Resistor, $3.65 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3641 | 1 |
| R11 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R12 | Resistor, 453 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-4561 | 1 |
| R13 | Resistor, 130 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1306 | 1 |
| R14 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |

TABLE 3-3. MODULATOR CIRCUIT BOARD ASSEMBLY 917-0302
(Sheet 3 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R15 | Resistor, 332 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3326 | 1 |
| R16 | Resistor, $69.8 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-6985 | 1 |
| R17 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R18 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R19 | Resistor, $3.65 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3641 | 1 |
| R20 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R21 | Resistor, 27 k Ohm $\pm 5 \%$, 1W | 120-2753 | 1 |
| R22 | Resistor, $22.1 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2211 | 1 |
| R23 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R24 | Resistor, 332 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3326 | 1 |
| R25 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R26 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R27 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R28 | Resistor, $69.8 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-6985 | 1 |
| R29 | Resistor, $3.65 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3641 | 1 |
| R30 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R31 | Resistor, 332 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3326 | 1 |
| R32 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R33 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R34 | Resistor, 121 Ohm $\pm 1 \%$, 1/4W | 100-1231 | 1 |
| R35 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R38 | Resistor, 47.5 k Ohm $\pm 1 \%$, 1/4W | 103-4755 | 1 |
| R39 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R40 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R41 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R42 | Resistor, $8.66 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-8641 | 1 |
| R43 | Resistor, 499 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4996 | 1 |
| R44 | Resistor, $8.25 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8254 | 1 |
| R45 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R46 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R47 thru R49 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R51 | Resistor, 15.4 k Ohm $\pm 1 \%$, 1/4W | 103-1551 | 1 |
| R52 | Resistor, $39 \mathrm{Ohm} \pm 5 \%$, 1/2W | 110-3923 | 1 |
| R53 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R54, R55 | Resistor, $100 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1031 | 2 |
| R56, R57 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 2 |
| R58 | Resistor, 453 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-4561 | 1 |
| TP1 thru TP4 | Terminal, Test Point, Oval, Red | 413-0106 | 4 |
| TP5, TP6 | Jack, Test, Right Angle Printed Circuit Board Mount | 417-0004 | 2 |
| U1 | Integrated Circuit, Opto-Isolator, 6N137 | 220-6137 | 1 |
| U2 | Driver, TC4421CAT, 2 Ampere, 5-Pin, TO-220 Case | 220-4421 | 1 |
| U3 | Integrated Circuit, LM339AN, Quad Comparator, 14-Pin DIP | 221-0339 | 1 |
| U4 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6- | 229-0033 | 1 |

TABLE 3-3. MODULATOR CIRCUIT BOARD ASSEMBLY 917-0302
(Sheet 4 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| U5 | Integrated Circuit, ULN2004, 7 NPN Darlington Driver Pack, 16-Pin DIP | 226-2004 | 1 |
| U6 | Integrated Circuit, MC14093B, Quad 2-Input NAND Schmitt Trigger, CMOS, 14-Pin DIP | 220-4093 | 1 |
| U7 | Integrated Circuit, MC14044BP, Quad NAND R-S Latch, CMOS, 16-Pin DIP | 228-4044 | 1 |
| U8, U9 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 2 |
| U10 | Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 V to 37 V , 1.5 Ampere, TO-220 Case | 227-0317 | 1 |
| U11 | Integrated Circuit, 14505, Hex Level Shifter, TTL to CMOS, 16-Pin DIP | 228-4504 | 1 |
| U12 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 1 |
| U13 | Driver, TC4421CAT, 2 Ampere, 5-Pin, TO-220 Case | 220-4421 | 1 |
| XF1, XF2 | Fuse Clips, AGC | 415-2068 | 2 |
| XU1 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU3 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU4 | Socket, 6-Pin DIP | 417-0600 | 1 |
| XU5 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU6 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU7 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU8, XU9 | Socket, 6-Pin DIP | 417-0600 | 2 |
| XU11 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU13 | Socket, 6-Pin DIP | 417-0600 | 1 |
| ---- | Coil, 36 uH , MOD PWM | 360-0108 | 2 |
| ---- | Coil, 9.2 uH, MOD PWM | 360-0109 | 1 |
| ---- | Coil, 14 uH , MOD PWM | 360-0110 | 1 |
| ---- | Blank, Modulator Circuit Board | 517-0302 | 1 |

TABLE 3-4. POWER AMPLIFIER CIRCUIT BOARD ASSEMBLY - 917-0304
(Sheet 1 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C2 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C3 thru C6 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $003-1041$ | 4 |
| C8 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C10 | Capacitor, Electrolytic, $100 \mathrm{uF}, 35 \mathrm{~V}$ | $023-1084$ | 1 |
| C11 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C12 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $003-1041$ | 1 |
| C13 | Capacitor, Electrolytic, $100 \mathrm{uF}, 63 \mathrm{~V}$ | $015-1084$ | 1 |
| C15 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |

TABLE 3-4. POWER AMPLIFIER CIRCUIT BOARD ASSEMBLY - 917-0304 (Sheet 2 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C16 thru C18 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 3 |
| C19 thru C21 | Capacitor, Monolytic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C23 | Capacitor, Mylar Film, $0.01 \mathrm{uF} \pm 10 \%, 200 \mathrm{~V}$ | 030-1043 | 1 |
| C24 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C25 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C26 | Capacitor, Ceramic, $0.001 \mathrm{uF}, 1 \mathrm{kV}$ | 002-1034 | 1 |
| C27, C28 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 200V | 003-1065 | 2 |
| $\begin{aligned} & \text { C29 thru } \\ & \text { C32 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | 003-1041 | 4 |
| C33 | Capacitor, Electrolytic, $10 \mathrm{uF}, 50 \mathrm{~V}$ | 023-1076 | 1 |
| C34 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 100V | 003-1041 | 1 |
| C36 ,C37 | Capacitor, Mica, $39 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3912 | 2 |
| C38, C39 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 2 |
| C40 thru C43 | Capacitor, Electrolytic, $1 \mathrm{uF}, 50 \mathrm{~V}$ | 024-1064 | 4 |
| C45 thru C55 | Refer To Power Module Frequency Dependant Kit Tables After This | ection. |  |
| C58 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 1 |
| C59 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| D1 thru D6 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 6 |
| D9, D10 | Transzorb Diode, 1N6281A, 27BV, 1.5KE27CA | 206-0027 | 2 |
| D11 | Diode, Zener 1N5229, 4.3V, 0.5W | 201-0035 | 1 |
| D16 | Diode, Transzorb, Diode, 300BV, 1.5FE300CA | 206-0300 | 1 |
| D17 | Transzorb Diode, 250BV, 1.5KE250CA | 206-0250 | 1 |
| D18 | Diode, Transzorb, Diode, 300BV, 1.5FE300CA | 206-0300 | 1 |
| D19 | Transzorb Diode, 250BV, 1.5KE250CA | 206-0250 | 4 |
| D20, D21 | Diode, Zener, 1N4749, 24V, 10.5 Amperes | 200-0024 | 2 |
| D22, D23 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D25, D26 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D29, D30 | Diode, Zener, 1N4742A, 12V $\pm 5 \%$, 1W | 200-4742 | 2 |
| D31 | Diode, Zener, 1N4737A, 7.5V, 1W, 34 mA | 200-4737 | 1 |
| D32 thru D35 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 4 |
| DS1 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 1 |
| DS2 | Indicator, LED, Red, 521-9212, 1.7V @ 50 mA Maximum | 323-9217 | 1 |
| F1 | Fuse, 3AB, 15 Amperes, 65V, Very Fast | 330-1502 | 1 |
| F2, F3 | Fuse, 5 X 20MM, 1.5 Ampere, Slow-Blow | 334-1150 | 2 |
| FC1, FC2 | Fuse Clips, AGC | 415-2068 | 2 |
| FC3 thru FC6 | Fuse Clips, Littlefuse, 111501 | 415-2069 | 4 |
| L1, L2 | Coil, 4uH | 360-0112 | 2 |
| L3 thru L7 | Refer To Power Module Frequency Dependant Kit Tables After This S | Section. |  |
| P2 | Connector, 15-Pin Sub-D, Male, Right Angle | 417-0374 | 1 |
| Q1, Q2 | RF FET, APT6018, 600V | 210-6018 | 2 |
| Q3 thru Q6 | Hexfet Power Mosfet, IRFI520G, TO-220 Fullpak | 210-0520 | 4 |
| Q7 | Transistor, TIP120, NPN Darlington-Connected Silicon Power, 65W @ 25\#C Case | 210-0120 | 1 |
| Q11 | Transistor, 2N3906, PNP, Silicon, TO-92 Case | 210-3906 | 1 |
| Q12 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |

TABLE 3-4. POWER AMPLIFIER CIRCUIT BOARD ASSEMBLY - 917-0304
(Sheet 3 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| Q13 | Silicon Controlled Rectifier, GE6CA, 100V @ 1.6 Ampere | 237-0006 | 1 |
| R1 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 5 \%, 1 \mathrm{~W}$ | 120-1043 | 1 |
| R2, R3 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R4 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R5 | Resistor, $1.10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1104 | 1 |
| R6, R7 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R8 thru R11 | Resistor, 27 Ohm $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-2723 | 4 |
| R12 | Resistor, 15k Ohm $\pm 5 \%$, 2 W | 130-1553 | 1 |
| R13 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R14 | Resistor, 1.10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1104 | 1 |
| R15 | Resistor, 1 k Ohm $\pm 5 \%$, 1 W | 120-1043 | 1 |
| R16 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R18 | Resistor, $1.10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1104 | 1 |
| R20 | Resistor, $1.96 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1964 | 1 |
| R21, R22 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R23 | Resistor, $10 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-1083 | 1 |
| R24 | Resistor, 1.96 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1964 | 1 |
| R25 | Resistor, 680 Ohm $\pm 5 \%, 1 / 2 \mathrm{~W}$ | 110-6833 | 1 |
| R26 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R27, R28 | Resistor, 332 Ohm $\pm 1 \%$, 1/4W | 103-3323 | 1 |
| R29 | Resistor, $300 \mathrm{Ohm} \pm 5 \%$, 2W, W/W | 130-3004 | 1 |
| R30, R31 | Resistor, 2.67 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2674 | 2 |
| R32, R33 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 2 |
| R34, R35 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R36, R37 | Resistor, $300 \mathrm{Ohm} \pm 5 \%$, 2W, W/W | 130-3004 | 2 |
| R38 | Resistor, $562 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5623 | 1 |
| R39, R40 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| U1 | Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 V to 37 V , 1.5 Ampere, TO-220 Case | 227-0317 | 1 |
| U2 thru U4 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo <br> Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 3 |
| U5 | Integrated Circuit, MC14584, 14-Pin Schmitt | 228-4584 | 1 |
| U7, U8 | Driver High and Low Side, IR2110 | 227-2110 | 2 |
| XU2 thru XU4 | Socket, 6-Pin DIP | 417-0600 | 3 |
| $\begin{aligned} & \text { XU5, XU7, } \\ & \text { XU8 } \end{aligned}$ | Socket, 14-Pin DIP | 417-1404 | 3 |
| ---- | Blank, Power Amplifier Circuit Board Assembly | 517-0304 | 1 |

TABLE 3-5. POWER MODULE FREQUENCY DEPENDANT KIT, 522 - 650 KHZ -957-1015-001

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C45, C56 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 4 |
| C46 thru C55 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1832$ | 20 |
| L3, L4 | Inductor, PA Drive | $360-0113-\mathrm{XXX}$ | 4 |
| --- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| ---- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

TABLE 3-6. POWER MODULE FREQUENCY DEPENDANT KIT, 651 - 770 KHZ -
957-1015-002

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C46, C55 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 4 |
| C47 thru C54 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1832$ | 16 |
| L3, L4 | Inductor, PA Drive | $360-0113-\mathrm{XXX}$ | 4 |
| ---- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| --- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

TABLE 3-7. POWER MODULE FREQUENCY DEPENDANT KIT, 771 - 920 KHZ -957-1015-003

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C47 thru C54 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ |  |  |
| L3, L4 | Inductor, PA Drive | $042-1832$ | 16 |
| ---- | Blank, PA Capacitor Board Circuit Board | $360-0113-\mathrm{XXX}$ | 4 |
| ---- | Blank, PA Inductor Board Circuit Board | $517-0318-001$ | 2 |
|  |  | $517-0319-001$ | 2 |

TABLE 3-8. POWER MODULE FREQUENCY DEPENDANT KIT, 921 - 1080 KHZ -

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C48, C53 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 4 |
| C49 thru C52 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1832$ | 8 |
| C47, C54 | Capacitor, Mica, $910 \mathrm{pF}, 1 \mathrm{kV}$ | $042-9122$ | 4 |
| L5, L7 | Inductor, PA Drive | $360-0113-X X X$ | 4 |
| ---- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| --- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

TABLE 3-9. POWER MODULE FREQUENCY DEPENDANT KIT, 1081-1300 KHZ -957-1015-005

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C48, C53 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 4 |
| C49 thru C52 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1832$ | 8 |
| L5, L7 | Inductor, PA Drive | $360-0113-\mathrm{XXX}$ | 4 |
| ---- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| --- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

TABLE 3-10. POWER MODULE FREQUENCY DEPENDANT KIT, 1301-1580 KHZ -957-1015-006

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C48, C53 | Capacitor, Mica, $910 \mathrm{pF}, 1 \mathrm{kV}$ | $042-9122$ | 4 |
| C49 thru C52 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 8 |
| L5, L6, L7 | Inductor, PA Drive | $360-0113-X X X$ | 6 |
| ---- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| --- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

TABLE 3-11. POWER MODULE FREQUENCY DEPENDANT KIT, 1581 - 1700 KHZ -957-1015-007

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C49, C52 | Capacitor, Mica, $1600 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1622$ | 4 |
| C50, C51 | Capacitor, Mica, $1800 \mathrm{pF}, 1 \mathrm{kV}$ | $042-1832$ | 4 |
| L5, L6, L7 | Inductor, PA Drive | $360-0113-\mathrm{XXX}$ | 6 |
| ---- | Blank, PA Capacitor Board Circuit Board | $517-0318-001$ | 2 |
| --- | Blank, PA Inductor Board Circuit Board | $517-0319-001$ | 2 |

## SECTION IV RF POWER MODULE DRAWINGS

## 4-1. INTRODUCTION.

4-2. This section provides assembly drawings, wiring diagrams, and schematic diagrams as listed below for the Broadcast Electronics AM-10A/AM-6A transmitter RF power module.

FIGURE
4-1
4-2
4-3

4-4

TITLE
NUMBER

SB917-0302
AD917-0302
SB917-0304

AD917-0304





## TABLE OF CONTENTS

| PARAGRAPH |  | PAGE NO. |
| :---: | :---: | :---: |
| SECTION I | OUTPUT NETWORK THEORY OF OPERATION |  |
| 1-1 | Introduction | 1-1 |
| 1-3 | Functional Description | 1-1 |
| SECTION II | OUTPUT NETWORK MAINTENANCE |  |
| 2-1 | Introduction | 2-1 |
| 2-3 | Safety Considerations | 2-1 |
| 2-6 | First Level Maintenance | 2-1 |
| 2-8 | Cleaning and Inspection | 2-1 |
| 2-10 | Second Level Maintenance | 2-2 |
| 2-12 | Electrical Adjustments | 2-2 |
| 2-13 | Modulation Calibration Controls | 2-2 |
| 2-14 | Directional Coupler Null Controls | 2-2 |
| 2-15 | Troubleshooting | 2-2 |
| 2-16 | Safety Considerations | 2-2 |
| 2-17 | Output Network Assembly Component Locations | 2-2 |
| 2-18 | Troubleshooting Procedures | 2-3 |
| 2-19 | Component Replacement Procedure | 2-3 |
| SECTION III | OUTPUT NETWORK ASSSEMBLY PARTS LIST |  |
| 3-1 | Introduction | 3-1 |
| SECTION IV | OUTPUT NETWORK ASSEMBLY DRAWINGS |  |
| 4-1 | Introduction | 4-1 |
|  | LIST OF TABLES |  |
| TABLE | TITLE | PAGE NO. |
| 2-1 | DIRECTIONAL COUPLER CIRCUIT BOARD TROUBLESHOOTING | 2-3 |
| 2-2 | LIGHTNING DETECTION CIRCUIT BOARD/ SPARK GAP TROUBLESHOOTING | 2-3 |
| 2-3 | LIGHTNING PROTECTION CIRCUIT BOARD TROUBLESHOOTING | 2-3 |
| 3-1 | REPLACEABLE PARTS LIST INDEX | 3-1 |

## SECTION I OUTPUT NETWORK THEORY OF OPERATION

## 1-1. INTRODUCTION.

1-2. This section presents the theory of operation for the AM-10A/AM-6A output network assembly.

## 1-3. FUNCTIONAL DESCRIPTION.

1-4. The output network assembly contains the: 1) harmonic band-pass filter, 2) directional coupler circuit board, 3) lightning protection circuit board, 4) T-matching network, 5) lightning detection circuit board, and 6) spark gap. The theory of operation for the output network assembly components is presented in PART I SECTION IV, THEORY OF OPERATION. Refer to SECTION IV as required for a description of the output network assembly components.

# SECTION II OUTPUT NETWORK MAINTENANCE 

## 2-1. INTRODUCTION.

2-2. This section provides maintenance information for the AM-10A/AM-6A transmitter output network assembly.

2-3. SAFETY CONSIDERATIONS.
WARNING THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

2-4. The AM-10A/AM-6A transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents.
$2-5$. In addition to high voltages and currents, the transmitters contain multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.

2-6. FIRST LEVEL MAINTENANCE.
2-7. First level maintenance consists of precautionary procedures applied to the equipment to prevent future failures. The procedures are performed on a regular basis and the results recorded in a performance log.

## 2-8. CLEANING AND INSPECTION.

## DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE ATTEMPTING ANY EQUIPMENT MAINTENANCE.

2-9. Ensure all transmitter primary power is disconnected and clean the output network assembly of accumulated dust using a nylon bristle brush and vacuum cleaner. Inspect the components for damage by overheating and arcing. In addition, check the components for loose hardware.

## 2-10. SECOND LEVEL MAINTENANCE.

2-11. Second level maintenance is the performance of procedures required to restore the ECU to operation after a fault has occurred. The procedures are divided into electrical adjustments procedures and troubleshooting.
2-12. ELECTRICAL ADJUSTMENTS.
2-13. MODULATION CALIBRATION CONTROLS. Modulation calibration controls R201 through R205 calibrate the modulation sample for each power level. A complete description of the procedure to adjust the power level controls is presented in SECTION II, INSTALLATION. Refer to POWER LEVEL AND MODULATION CALIBRATION ADJUSTMENT in SECTION II for the adjustment procedure.
2-14. DIRECTIONAL COUPLER NULL CONTROLS. Directional coupler null controls R223, R224, R234, and R235 null the directional coupler sampling circuit. Due to the critical nature of the directional coupler null controls, the controls are not considered field adjustable. If the controls are required to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the directional coupler null controls.
2-15. TROUBLESHOOTING.
WARNING

WARNING
WARNING
WARNING

> THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

2-16. SAFETY CONSIDERATIONS. The AM-10A/AM-6A transmitters are equipped with extensive indicator and meter circuitry to allow the operator to isolate problems to a specific area within the transmitter. Due to the hazardous voltages and currents contained in the equipment, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.
2-17. OUTPUT NETWORK ASSEMBLY COMPONENT LOCATIONS. Component locations for the output network assembly are presented in PART I SECTION V, MAINTENANCE. Refer to TRANSMITTER COMPONENT LOCATIONS in SECTION V to locate components within the output network assembly.

2-18. TROUBLESHOOTING PROCEDURES. The output network assembly troubleshooting procedures are presented in Tables 2-1 through 2-3. Table 2-1 presents the directional coupler circuit board troubleshooting. Table 2-2 presents the lightning detection circuit board and spark gap troubleshooting. Table 2-3 presents the lightning protection circuit board troubleshooting. Refer to Tables 2-1 through 2-3 to isolate the problem to a specific circuit. Once the trouble is isolated, refer to the circuit board theory of operation presented in PART I SECTION IV and the schematic diagrams presented in this section to assist in problem resolution.

TABLE 2-1. DIRECTIONAL COUPLER CIRCUIT BOARD TROUBLESHOOTING

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| HIGH REFLECTED POWER | 1. Check diode D201 through D210. |
| METER INDICATION WHEN |  |
| ACTUAL REFLECTED POWER |  |
| IS LOW |  |

TABLE 2-2. LIGHTNING DETECTION CIRCUIT BOARD/SPARK GAP TROUBLESHOOTING

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| HIGH REFLECTED POWER | 1. Check the lightning detection circuit board for a <br> short circuit condition. |
| CONDITION | 1. Check the spark gap. <br> NO LIGHTNING DETECTION <br> OPERATION |
|  |  |

TABLE 2-3. LIGHTNING PROTECTION CIRCUIT BOARD TROUBLESHOOTING

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :---: |
| HIGH REFLECTED POWER | 1. Check the circuit board for a short circuit condition. |
| OR SHORTED OUTPUT |  |
| CONDITION |  |

2-19. COMPONENT REPLACEMENT PROCEDURE. Component replacement procedures for the output network assembly are presented in PART I SECTION V. Refer to COMPONENT REPLACEMENT in SECTION V as required for the replacement procedures.

# SECTION III <br> OUTPUT NETWORK ASSEMBLY PARTS LIST 

## 3-1. INTRODUCTION.

3-2. This section provides descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance of the output network assembly. Each table entry in this section is indexed by reference designators appearing on the applicable schematic.

## TABLE 3-1. REPLACEABLE PARTS LIST INDEX (Sheet 1 of 2)

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :---: | :---: | :---: | :---: |
| 3-2 | Output Network Assembly, AM-10A/AM-6A | $\begin{aligned} & 957-0030 / \\ & 957-0032 \end{aligned}$ | 3-3 |
| 3-3 | Lightning Protection Circuit Board, AM-10A/AM-6A | $\begin{array}{r} 917-0216-001 / \\ -002 \end{array}$ | 3-3 |
| 3-4 | Harness Output Network Assembly | 947-0154 | 3-3 |
| 3-5 | Directional Coupler Circuit Board Assembly | 917-0306-002 | 3-4 |
| 3-6 | Lightning Detection Circuit Board Assembly | 917-0306-004 | 3-5 |
| 3-7 | Output Network Frequency Dependant Parts, 522-650 KHZ, AM-10A | 957-1035-101 | 3-5 |
| 3-8 | Output Network Frequency Dependant Parts, 522-650 KHZ, AM-6A | 957-1035-061 | 3-6 |
| 3-9 | Output Network Frequency Dependant Parts, 651-770 KHZ, AM-10A | 957-1035-102 | 3-6 |
| 3-10 | Output Network Frequency Dependant Parts, 651-770 KHZ, AM-6A | 957-1035-062 | 3-6 |
| 3-11 | Output Network Frequency Dependant Parts, 771-920 KHZ, AM-10A | 957-1035-103 | 3-7 |
| 3-12 | Output Network Frequency Dependant Parts, 771-920 KHZ, AM-6A | 957-1035-063 | 3-7 |
| 3-13 | Output Network Frequency Dependant Parts, 921-1080 KHZ, AM-10A | 957-1035-104 | 3-8 |
| 3-14 | Output Network Frequency Dependant Parts, 921-1080 <br> KHZ, AM-6A | 957-1035-064 | 3-8 |
| 3-15 | Output Network Frequency Dependant Parts, 1081-1300 KHZ, AM-10A | 957-1035-105 | 3-8 |
| 3-16 | Output Network Frequency Dependant Parts, 1081-1300 KHZ, AM-6A | 957-1035-065 | 3-9 |
| 3-17 | Output Network Frequency Dependant Parts, 1301-1580 KHZ, AM-10A | 957-1035-106 | 3-9 |
| 3-18 | Output Network Frequency Dependant Parts, 1301-1580 KHZ, AM-6A | 957-1035-066 | 3-10 |

TABLE 3-1. REPLACEABLE PARTS LIST INDEX (Sheet 2 of 2)

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :--- | :---: | :---: | :---: | :---: |
| $3-19$ | Output Network Frequency Dependant Parts, 1581-1700 <br> KHZ, AM-10A | $957-1035-107$ | $3-10$ |
| $3-20$ | Output Network Frequency Dependant Parts, 1581-1700 <br> KHZ, AM-6A | $957-1035-067$ | $3-10$ |

TABLE 3-2. OUTPUT NETWORK ASSEMBLY, AM-10A/AM-6A - 957-0030/957-0032

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| L4, L6 | Coil, Variable, $16 \mathrm{uH}, 20$ Amperes | 360-0088 | 1 |
|  | - FOR 957-0030 ASSEMBLY, AM-10A |  |  |
| ---- | Spark Gap, 2.7 kV | 140-0022 | 1 |
| ---- | Lightning Protection Circuit Board Assembly | 917-0216-002 | 1 |
| FOR 957-0032 ASSEMBLY, AM-6A |  |  |  |
| ---- | Spark Gap, 2.1 kV | 140-0024 | 1 |
| ---- | Lightning Protection Circuit Board Assembly | 917-0216-001 | 1 |
| ---- | BNC Receptacle, Bulkhead, UG492A/U | 417-0017 | 1 |
| ---- | Harness Output Network Assembly | 947-0154 | 1 |
| ---- | Directional Coupler Circuit Board Assembly | 917-0306-002 | 1 |
| ---- | Lightning Detector Circuit Board Assembly | 917-0306-004 | 1 |

TABLE 3-3. LIGHTNING PROTECTION CIRCUIT BOARD, AM-6A, AM-10A -917-0216-001/-002

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
|  | FOR 957-0216-001 ASSEMBLY, AMM-6A |  |  |
| D2 thru D6 | Transzorb, 1.5KE300CA, 300BV | $206-0300$ | 5 |
| D1, D7 | Transzorb, 1.5KE400CA, 400BV | $206-0400$ | 2 |
|  | FOR 957-0216-002 ASSEMBLY, AMM-10A |  |  |
| D1 thru D8 | Transzorb, 1.5KE400CA, 400BV | $206-0400$ | 8 |
| $--\quad$ | Blank, Lightning Protection Circuit Board | $517-0216$ | 1 |

TABLE 3-4. HARNESS OUTPUT NETWORK ASSEMBLY - 947-0154

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| --- | Contact Housing, 4-Pin In-line | $417-0138$ | 2 |
| --- | Pins, Connector | $417-0142$ | 15 |
| --- | Plug, Housing, 2-Pin | $417-0499$ | 1 |
| --- | Plug, Housing, 14-Pin | $417-1401$ | 1 |
| ---- | Connector, 15-Pin, D-Type | $417-1500$ | 1 |
| --- | Pins, Crimp Type | $417-8766$ | 23 |
| --- | Plug, BNC, Dual Crimp | $418-0034$ | 1 |

TABLE 3-5. DIRECTIONAL COUPLER CIRCUIT BOARD ASSEMBLY - 917-0306-002 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C201 | Capacitor, Mylar Film, $0.01 \mathrm{uF} \pm 10 \%$, 200V | 030-1043 | 1 |
| C202 thru <br> C217 | Capacitor, Ceramic, Monolythic, . $1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 16 |
| C218 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C219, C220 | Capacitor, Polyester, $0.0022 \mathrm{uF} \pm 10 \%$, 100V | 031-2033 | 2 |
| $\begin{aligned} & \text { D201 thru } \\ & \text { D204 } \end{aligned}$ | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 4 |
| $\begin{aligned} & \text { D205 thru } \\ & \text { D208 } \end{aligned}$ | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 4 |
| D209, D210 | Diode, Zener, 1N4749, 24V, 10.5 Amperes | 200-0024 | 2 |
| D211, D212 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D213, D214 | Diode, Zener, 1N4749, 24V, 10.5 Amperes | 200-0024 | 2 |
| D215, D216 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| $\begin{aligned} & \text { E202 thru } \\ & \text { E208 } \end{aligned}$ | Turret, Double Shoulder | 413-0025 | 7 |
| $\begin{aligned} & \text { E209 thru } \\ & \text { E211 } \end{aligned}$ | Terminal, Male Disconnect | 410-0025 | 3 |
| E212 thru E217 | Turret, Double Shoulder | 413-0025 | 6 |
| $\begin{aligned} & \text { E219 thru } \\ & \text { E221 } \end{aligned}$ | Turret, Double Shoulder | 413-0025 | 3 |
| J201 | Receptacle, Male, 20-Pin In-Line | 417-0200 | 1 |
| J202, J203 | Receptacle, Male, 8-Pin In-Line, Right Angle | 417-0080-001 | 2 |
| $\begin{aligned} & \text { J204 thru } \\ & \text { J206 } \end{aligned}$ | Receptacle, Male, 20-Pin In-Line | 417-0200 | 3 |
| $\begin{aligned} & \text { K201 thru } \\ & \text { K205 } \end{aligned}$ | Relay, SPST, 5V dc, 500 Ohm, Reed | 270-0062 | 5 |
| L201 | Coil, Molded, Shielded, 5.6 uH | 364-0056 | 1 |
| L202 | Coil, Molded, Shielded, 56 uH | 360-0093 | 1 |
| L203, L204 | RF Choke, $10 \mathrm{mH} \pm 10 \%$, 6.3 Ohms DC Resistance, 220 mA Maximum | 364-0670 | 2 |
| P203, P204 | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P204, P205 | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P205, P206 | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| $\begin{aligned} & \text { R201 thru } \\ & \text { R205 } \end{aligned}$ | Potentiometer, 250 Ohm, 2W, Double, 1-Turn | 192-2533 | 5 |
| R206 | Resistor, 30.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3011 | 1 |
| $\begin{aligned} & \text { R207 thru } \\ & \text { R209 } \end{aligned}$ | Resistor, $18 \mathrm{Ohm} \pm 1 \%, 3 \mathrm{~W}$ | 130-1821 | 3 |
| $\begin{aligned} & \text { R210 thru } \\ & \text { R214 } \end{aligned}$ | Resistor, 30.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3011 | 5 |
| $\begin{aligned} & \text { R215 thru } \\ & \text { R222 } \end{aligned}$ | Resistor, 200 Ohm $\pm 1 \%$, 1W | 120-2031 | 8 |
| R223, R224 | Potentiometer, $20 \mathrm{k} \pm 10 \%$, 1W, Horizontal, 22 Turn | 178-2056 | 2 |
| $\begin{aligned} & \text { R226 thru } \\ & \text { R229 } \end{aligned}$ | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 4 |
| $\begin{aligned} & \text { R230 thru } \\ & \text { R233 } \end{aligned}$ | Resistor, 150 Ohm $\pm 1 \%$, 1W | 120-1531 | 4 |
| R234, R235 | Potentiometer, $20 \mathrm{k} \pm 10 \%$, 1W, Horizontal, 22 Turn | 178-2056 | 2 |
| $\begin{aligned} & \text { R236 thru } \\ & \text { R239 } \end{aligned}$ | Resistor, 200 Ohm $\pm 1 \%$, 1W | 120-2031 | 4 |

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TABLE 3-5. DIRECTIONAL COUPLER CIRCUIT BOARD ASSEMBLY - 917-0306-002
(Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| S201 | Switch, SPST, 4- Position, 8-Pin DIP Dual In-line | $340-0002$ |  |
| T201, T202 | Transformer, Current, AM-1/5 | $370-0040$ | 1 |
| T203 | Transformer, Voltage, AM-1/5 | $370-0041$ | 2 |
| ---- | Blank, Directional Coupler Circuit Board | $517-0306-002$ | 1 |

TABLE 3-6. LIGHTNING DETECTION CIRCUIT BOARD ASSEMBLY - 917-0306-004

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| C401 thru | Capacitor, Mica, $1000 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | $042-3913$ | 20 |
| C420 |  |  |  |
| E201, E202 | Terminal, Male Disconnect | $410-0025$ | 2 |
| E403 | Terminal, Male Disconnect | $410-0025$ | 1 |
| J401, J402 | Receptacle, Male, 20-Pin In-Line | $417-0200$ | 2 |
| J403 thru | Receptacle, Male, 2-Pin In-line | $417-4004$ | 3 |
| J405 |  |  |  |
| P403 thru | Jumper, Programmable, 2-Pin | $340-0004$ | 3 |
| P405 |  | $215-0001$ |  |
| Q401 | Phototransistor, 1.8 mA, IC AT 5V | $469-0369$ | 1 |
| S401 | Finger Contact Strip | $517-0306-004$ | 1 |
| ---- | Blank, Lightning Detector Circuit Board |  |  |

## TABLE 3-7. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 522 - 650 KHZ , AM-10A - 957-1035-101

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica, $2700 \mathrm{pF}, 12 \mathrm{kV}, 22$ Amperes | $044-2723-293$ | 2 |
| C2A, C2B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $2700 \mathrm{pF}, 12 \mathrm{kV}, 22$ Amperes | $044-2723-293$ | 2 |
| C4 | Capacitor, Mica, $8200 \mathrm{pF}, 10 \mathrm{kV}, 36$ Amperes | $044-8223-293$ | 1 |
| C5A, C5B, | Capacitor, Mica, $1100 \mathrm{pF}, 10 \mathrm{kV}, 10$ Amperes | $044-1123-292$ | 3 |
| C5C |  |  | $360-1111-\mathrm{XXX}$ |
| L1 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1115-\mathrm{XXX}$ | 1 |
| L5 | Coil, Output Network |  |  |

TABLE 3-8. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 522 - $\mathbf{6 5 0} \mathbf{~ K H Z , ~}$ AM-6A - 957-1035-061

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $3300 \mathrm{pF}, 12 \mathrm{kV}, 24$ Amperes |  |  |
| C4 | Capacitor, Mica, $8200 \mathrm{pF}, 4 \mathrm{kV}, 20$ Amperes | $044-3323-293$ | 1 |
| C1A, C3A | Capacitor, Mica, $2700 \mathrm{pF}, 8 \mathrm{kV}, 15$ Amperes | $044-8223-291$ | 1 |
| C1B, C3B | Capacitor, Mica, $2700 \mathrm{pF}, 8 \mathrm{kV}, 15$ Amperes | $044-2723-292$ | 2 |
| C5A | Capacitor, Mica, $2400 \mathrm{pF}, 6 \mathrm{kV}, 13.0$ Amperes | $044-2723-292$ | 2 |
| C5B | Capacitor, Mica, $1500 \mathrm{pF}, 6 \mathrm{kV}, 9.1$ Amperes | $044-2423-291$ | 1 |
| L1 | Coil, All Frequency | $044-1523-291$ | 1 |
| L2 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-0602-\mathrm{XXX}$ | 1 |
| L5 | Coil, All Frequency | $360-0603-\mathrm{XXX}$ | 1 |
|  |  | $360-0605-\mathrm{XXX}$ | 1 |

TABLE 3-9. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 651 - 770 KHZ, AM-10A - 957-1035-102

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica $2200 \mathrm{pF}, 12 \mathrm{kV}, 20$ Amperes | $044-2223-293$ | 2 |
| C2A | Capacitor, Mica $1100 \mathrm{pF}, 20 \mathrm{kV}, 15$ Amperes | $044-1123-293$ | 1 |
| C2B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 1 |
| C3A, C3B | Capacitor, Mica $2200 \mathrm{pF}, 12 \mathrm{kV}, 20$ Amperes | $044-2223-293$ | 2 |
| C4 | Capacitor, Mica $6800 \mathrm{pF}, 10 \mathrm{kV}, 33$ Amperes | $044-6823-293$ | 1 |
| C5A, C5B, | Capacitor, Mica $910 \mathrm{pF}, 10 \mathrm{kV}, 9.1$ Amperes | $044-9113-292$ | 3 |
| C5C |  |  | $360-1111-\mathrm{XXX}$ |
| L1 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-10. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 651 - 770 KHZ, AM-6A - 957-1035-062 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $2700 \mathrm{pF}, 12 \mathrm{kV}, 22$ Amperes | $044-2723-293$ | 1 |
| C4 | Capacitor, Mica, $6800 \mathrm{pF}, 4 \mathrm{kV}, 18.0$ Amperes | $044-6823-291$ | 1 |
| C1A, C1B | Capacitor, Mica, $2200 \mathrm{pF}, 8 \mathrm{kV}, 13$ Amperes | $044-2223-292$ | 2 |
| C3A | Capacitor, Mica, $2200 \mathrm{pF}, 8 \mathrm{kV}, 13$ Amperes | $044-2223-292$ | 1 |
| C3B | Capacitor, Mica, $2200 \mathrm{pF}, 8 \mathrm{kV}, 13$ Amperes | $044-2223-292$ | 1 |
| C5A | Capacitor, Mica, $1500 \mathrm{pF}, 6 \mathrm{kV}, 9.1$ Amperes | $044-1523-291$ | 1 |
| C5B | Capacitor, Mica, $1800 \mathrm{pF}, 6 \mathrm{kV}, 11$ Amperes | $044-1823-291$ | 1 |
| L1 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-0602-\mathrm{XXX}$ | 1 |

TABLE 3-10. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 651 - 770 KHZ , AM-6A - 957-1035-062 (Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
| L3 | Coil, All Frequency |  | $360-0603-\mathrm{XXX}$ |
| L5 | Coil, All Frequency | $360-0605-\mathrm{XXX}$ | 1 |

TABLE 3-11. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 771 - 920 KHZ, AM-10A - 957-1035-103

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica $2200 \mathrm{pF}, 12 \mathrm{kV}, 20$ Amperes | $044-2223-293$ | 2 |
| C2A, C2B | Capacitor, Mica, $1100 \mathrm{pF}, 20 \mathrm{kV}, 15$ Amperes | $044-1123-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $1800 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1823-293$ | 2 |
| C4 | Capacitor, Mica, $5600 \mathrm{pF}, 10 \mathrm{kV}, 33$ Amperes | $044-5623-293$ | 1 |
| C5A, C5B | Capacitor, Mica, $820 \mathrm{pF}, 10 \mathrm{kV}, 9.1$ Amperes | $044-8213-292$ | 2 |
| C5C | Capacitor, Mica, $620 \mathrm{pF}, 10 \mathrm{kV}, 8.2$ Amperes | $044-6213-292$ | 1 |
| C7 | Capacitor, Mica $6800 \mathrm{pF}, 4 \mathrm{kV}, 18$ Amperes | $044-6823-291$ | 1 |
| L1 | Coil, All Frequency | $360-1111-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L5 | Coil, Output Network | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-12. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 771 - 920 KHZ, AM-6A - 957-1035-063

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $2200 \mathrm{pF}, 12 \mathrm{kV}, 20$ Amperes | $044-2223-293$ | 1 |
| C4 | Capacitor, Mica, $5600 \mathrm{pF}, 4 \mathrm{kV}, 18$ Amperes | $044-5623-291$ | 1 |
| C1A, C1B | Capacitor, Mica, $1800 \mathrm{pF}, 10 \mathrm{kV}, 13$ Amperes | $044-1823-292$ | 2 |
| C3A, C3B | Capacitor, Mica, $1800 \mathrm{pF}, 10 \mathrm{kV}, 13$ Amperes | $044-1823-292$ | 2 |
| C5A | Capacitor, Mica, $1500 \mathrm{pF}, 6 \mathrm{kV}, 9.1$ Amperes | $044-1523-291$ | 1 |
| C5B | Capacitor, Mica, $1200 \mathrm{pF}, 6 \mathrm{kV}, 8.2$ Amperes | $044-1223-291$ | 1 |
| L1 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-0602-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-0603-\mathrm{XXX}$ | 1 |
| L5 | Coil, All Frequency | $360-0605-\mathrm{XXX}$ | 1 |

TABLE 3-13. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 921-1080 KHZ, AM-10A - 957-1035-104

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica $4300 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-1823-293$ | 2 |
| C2A, C2B | Capacitor, Mica $910 \mathrm{pF}, 20 \mathrm{kV}, 13$ Amperes | $044-9113-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 2 |
| C4 | Capacitor, Mica, $4700 \mathrm{pF}, 10 \mathrm{kV}, 27$ Amperes | $044-4723-293$ | 1 |
| C5A, C5B | Capacitor, Mica, $620 \mathrm{pF}, 10 \mathrm{kV}, 27$ Amperes | $044-6213-292$ | 3 |
| C5C |  |  | $044-4323-291$ |
| C7 | Capacitor, Mica, $4300 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $360-1111-\mathrm{XXX}$ | 1 |
| L1 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-14. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 921-1080 KHZ, AM-6A - 957-1035-064

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, 2000PF,15KV,20A, $5 \%$ |  |  |
| C4 | Capacitor, Mica, 4700PF,6KV,16A,5\% | $044-2023-293$ | 1 |
| C1A, C1B | Capacitor, Mica, 1600PF,10KV,12.0A,5\% | $044-4723-291$ | 1 |
| C3A, C3B | Capacitor, Mica, 1600PF,10KV,12.0A,5\% | $044-1623-292$ | 2 |
| C5A, C5B | Capacitor, Mica, 1100PF,6KV,8.2A,5\% | $044-1623-292$ | 2 |
| L1 | Coil, All Frequency | $044-1123-291$ | 2 |
| L2 | Coil, All Frequency | $360-0601-X X X$ | 1 |
| L3 | Coil, All Frequency | $360-0602-X X X$ | 1 |
| L5 | Coil, All Frequency | $360-0603-X X X$ | 1 |
|  |  | $360-0605-X X X$ | 1 |

TABLE 3-15. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1081 - 1300 KHZ , AM-10A - 957-1035-105 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 2 |
| C2A, C2B | Capacitor, Mica, $820 \mathrm{pF}, 20 \mathrm{kV}, 12$ Amperes | $044-8213-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 2 |
| C4 | Capacitor, Mica, $3900 \mathrm{pF}, 12 \mathrm{kV}, 27$ Amperes | $044-3923-293$ | 1 |
| C5A, C5B | Capacitor, Mica, $560 \mathrm{pF}, 10 \mathrm{kV}, 7.5$ Amperes | $044-5613-292$ | 2 |
| C5C | Capacitor, Mica, $620 \mathrm{pF}, 10 \mathrm{kV}, 8.2$ Amperes | $044-6213-292$ | 1 |
| C6, C7 | Capacitor, Mica, $4300 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-4323-291$ | 2 |
| C8 | Capacitor, Mica, $8200 \mathrm{pF}, 4 \mathrm{kV}, 20$ Amperes | $044-8223-291$ | 1 |
| L1 | Coil, All Frequency | $360-1111-\mathrm{XXX}$ | 1 |

TABLE 3-15. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1081 - 1300 KHZ , AM-10A - 957-1035-105 (Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L2 | Coil, All Frequency |  | $360-1112-\mathrm{XXX}$ |
| L3 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L5 | Coil, Output Network | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-16. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1081 - 1300 KHZ , AM-6A - 957-1035-065

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 1 |
| C4 | Capacitor, Mica, $3900 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-3923-291$ | 1 |
| C1A, C1B | Capacitor, Mica, $1300 \mathrm{pF}, 10 \mathrm{kV}, 11.0$ Amperes | $044-1323-292$ | 2 |
| C3A, C3B | Capacitor, Mica, $1300 \mathrm{pF}, 10 \mathrm{kV}, 11.0$ Amperes | $044-1323-292$ | 2 |
| C5A, C5B | Capacitor, Mica, $910 \mathrm{pF}, 6 \mathrm{kV}, 7.5$ Amperes | $044-9113-291$ | 2 |
| L1 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-0602-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-0603-\mathrm{XXX}$ | 1 |
| L5 | Coil, All Frequency | $360-0605-\mathrm{XXX}$ | 1 |

TABLE 3-17. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1301 - 1580 KHZ, AM-10A - 957-1035-106

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1A, C1B | Capacitor, Mica, $1800 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1823-293$ | 2 |
| C2A, C2B | Capacitor, Mica, $620 \mathrm{pF}, 20 \mathrm{kV}, 11$ Amperes | $044-6213-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $910 \mathrm{pF}, 20 \mathrm{kV}, 13$ Amperes | $044-9113-293$ | 2 |
| C4 | Capacitor, Mica, $3300 \mathrm{pF}, 12 \mathrm{kV}, 24$ Amperes | $044-3323-293$ | 1 |
| C5A, C5B | Capacitor, Mica $4300 \mathrm{pF}, 10 \mathrm{kV}, 6.2$ Amperes | $044-4313-292$ | 2 |
| C5C | Capacitor, Mica, $620 \mathrm{pF}, 10 \mathrm{kV}, 8.2$ Amperes | $044-6213-292$ | 1 |
| C6, C7 | Capacitor, Mica, $3300 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-3323-291$ | 2 |
| C8 | Capacitor, Mica, $3900 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-3923-291$ | 1 |
| L1 | Coil, All Frequency | $360-1111-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L5 | Coil, Output Network | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-18. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1301 - 1580 KHZ , AM-6A - 957-1035-066

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $1200 \mathrm{pF}, 15 \mathrm{KV}, 16.0$ Amperes | $044-1223-293$ | 1 |
| C4, C6 | Capacitor, Mica, $3300 \mathrm{pF}, 6 \mathrm{KV}, 15$ Amperes | $044-3323-291$ | 2 |
| C1A, C1B | Capacitor, Mica, $1100 \mathrm{pF}, 10 \mathrm{KV}, 10$ Amperes | $044-1123-292$ | 2 |
| C3A, C3B | Capacitor, Mica ,1100 pF, 10KV, 10 Amperes | $044-1123-292$ | 2 |
| C5A, C5B | Capacitor, Mica, $820 \mathrm{pF}, 6 \mathrm{KV}, 6.8$ Amperes | $044-8213-291$ | 2 |
| L1 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-0602-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-0603-\mathrm{XXX}$ | 1 |
| L5 | Coil, All Frequency | $360-0605-\mathrm{XXX}$ | 1 |

TABLE 3-19. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1581 - 1700 KHZ , AM-10A - 957-1035-107

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| C1A, C1B | Capacitor, Mica, $1600 \mathrm{pF}, 15 \mathrm{kV}, 18$ Amperes | $044-1623-293$ | 2 |
| C2A, C2B | Capacitor, Mica, $620 \mathrm{pF}, 20 \mathrm{kV}, 11$ Amperes | $044-6213-293$ | 2 |
| C3A, C3B | Capacitor, Mica, $1100 \mathrm{pF}, 20 \mathrm{kV}, 15$ Amperes | $044-1123-293$ | 2 |
| C4 | Capacitor, Mica, $2700 \mathrm{pF}, 12 \mathrm{kV}, 22$ Amperes | $044-2723-293$ | 1 |
| C5A, C5B | Capacitor, Mica, $430 \mathrm{pF}, 10 \mathrm{kV}, 6.2$ Amperes | $044-4313-292$ | 3 |
| C5C |  |  | $044-2223-291$ |
| C6 | Capacitor, Mica, $2200 \mathrm{pF}, 6 \mathrm{kV}, 12$ Amperes | $044-1823-291$ | 1 |
| C7 | Capacitor, Mica, $1800 \mathrm{pF}, 6 \mathrm{kV}, 11$ Amperes | $044-3623-291$ | 1 |
| C8 | Capacitor, Mica, $3600 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $360-1111-\mathrm{XXX}$ | 1 |
| L1 | Coil, All Frequency | $360-1112-\mathrm{XXX}$ | 1 |
| L2 | Coil, All Frequency | $360-1113-\mathrm{XXX}$ | 1 |
| L3 | Coil, All Frequency | $360-1115-\mathrm{XXX}$ | 1 |

TABLE 3-20. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1581 - 1700 KHZ , AM-6A - 957-1035-067 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C2 | Capacitor, Mica, $1100 \mathrm{pF}, 20 \mathrm{kV}, 15$ Amperes | $044-1123-293$ | 1 |
| C4 | Capacitor, Mica, $2700 \mathrm{pF}, 6 \mathrm{kV}, 13$ Amperes | $044-2723-291$ | 1 |
| C6 | Capacitor, Mica, $3300 \mathrm{pF}, 6 \mathrm{kV}, 15$ Amperes | $044-3323-291$ | 1 |
| C1A, C1B | Capacitor, Mica, $910 \mathrm{pF}, 10 \mathrm{kV}, 9.1$ Amperes | $044-9113-292$ | 2 |
| C3A, C3B | Capacitor, Mica, $910 \mathrm{pF}, 10 \mathrm{kV}, 9.1$ Amperes | $044-9113-292$ | 2 |
| C5A, C5B | Capacitor, Mica, $620 \mathrm{pF}, 6 \mathrm{kV}, 6.2$ Amperes | $044-6213-291$ | 2 |
| L1 | Coil, All Frequency | $360-0601-\mathrm{XXX}$ | 1 |

TABLE 3-20. OUTPUT NETWORK FREQUENCY DEPENDANT PARTS, 1581 - 1700 KHZ , AM-6A - 957-1035-067 (Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| L2 | Coil, All Frequency |  | $360-0602-\mathrm{XXX}$ |
| L3 | Coil, All Frequency |  | 1 |
| L5 | Coil, All Frequency |  | $360-0603-\mathrm{XXX}$ |
|  |  |  | 1 |
|  |  |  |  |

## SECTION IV OUTPUT NETWORK ASSEMBLY DRAWINGS

## 4-1. INTRODUCTION.

4-2. This section provides assembly drawings, wiring diagrams, and schematic diagrams as listed below for the Broadcast Electronics AM-10A/AM-6A transmitter output network assembly.

FIGURE

4-1
4-2

4-3

4-4
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4-5

TITLE

SCHEMATIC DIAGRAM, AM-10A OUTPUT NETWORK ASSEMBLY
SCHEMATIC DIAGRAM, AM-6A OUTPUT NETWORK ASSEMBLY
SCHEMATIC DIAGRAM, DIRECTIONAL COUPLER CIRCUIT BOARD
SCHEMATIC DIAGRAM, LIGHTNING DETECTOR CIRCUIT BOARD
REFER TO PART I, SECTION VII FOR THE ECU AD917-0306-001/ DISPLAY CIRCUIT BOARD ASSEMBLY

ASSEMBLY DIAGRAM, LIGHTNING PROTECTION BOARD

## NUMBER

SB957-0030
SB957-0032

SB917-0306-002

SB917-0306-004
-002/-003/-004/-005
AB917-0216-001
/-002






## TABLE OF CONTENTS

## SECTION I

1-1
1-3
1-5
1-6
1-9
1-10
1-11
1-12
1-13
1-14
1-16
1-17
1-19
1-21
1-24
1-26

1-31
1-33
1-36
1-38
1-43
1-46
1-50
1-51
1-55
1-57
1-71
1-73
1-74
1-82
1-84
1-88
1-91
1-93
1-95
1-97
1-99
1-100
1-104
1-105
1-106
1-107
1-109
1-110
1-111
1-117
1-118

ECU THEORY OF OPERATION
Introduction 1-1
General Description 1-1
Functional Description $\quad 1-1$
ECU Display Circuit Board
1-1
Exciter Monitor Mode Control Circuit 1-1
Autorange Circuit 1-2
Polarity Control Circuit 1-2
Half-Wave Rectifier Circuit 1-2
Meter Circuitry 1-2
Indicator Circuitry 1-2
Reset Switch 1-2
ECU Switch Circuit Board 1-2
ECU Meter Switch Circuit Board 1-3
Motherboard 1-3
Controller Circuit Board 1-3
Cabinet/External Interlock and Remote Control 1-3
Fail-Safe
External Mute 1-4
Antenna Interlock 1-4
Remote Control 1-9
Power On 1-9
Power Control Circuit 1-10
Power Control Trim Circuit 1-11
Transmitter Off 1-11
AC Power Interruptions 1-12
Forward and Reflected Power Circuitry 1-12
Foldback Protection 1-13
Attack Signal Operation 1-16
1.2: 1 VSWR Conditions 1-16

Foldback Recovery 1-16
Exciter Monitoring 1-17
Power Supply Monitoring $\quad 1-18$
RF Power Module Monitoring 1-18
Fault Circuit 1-19
Oscillator Circuit 1-19
Over-Cycle Off Circuit 1-19
Power Supply Circuit 1-19
Exciter Circuit Board $1-20$
Left/Right Channel Input Circuit 1-20
Mono Mode Switching 1-23
24 uS Delay Circuit 1-23
Negative Limiter 1-23
IPM Correction Circuit 1-23
PWM Circuit 1-23
PWM Driver Circuit 1-24
Frequency Synthesizer 1-24
PWM Reference Circuit 1-24
Lock Detector Circuit 1-25

1-120
1-124
1-125
1-128
1-129
1-130
1-131
1-132
1-134
1-135
1-136
1-137
1-138
1-142
1-146
1-147
1-148
1-149
1-150
1-155
1-158
1-160
1-161
SECTION II
2-1
2-3
2-6
2-9
2-11
2-13
2-15
2-17
2-19
2-20
2-21
2-22
2-23
2-24
2-25
2-26
2-27
2-28
2-29
2-30
2-31
2-32
2-33
2-34
2-35
2-48

Stereo Detection Circuit 1-25
IPM Wave Shape Circuit 1-25
Phase Modulator Circuit 1-25
RF Drive Circuit 1-26
Exciter Failure Detector Circuit 1-26
Power Supply Circuits 1-26
Stereo Circuit Board 1-26
Equalization Circuitry 1-26
8 Microsecond Delay Circuit 1-29
4 Microsecond Delay Circuit 1-29
All-Pass Filter 1-29
Equalization Selection Circuit 1-29
$L+R$ and L-R Matrix Circuit 1-29
Phase Modulator Circuit 1-30
Band-Pass Filter 1-31
Transistor Amplifier Circuit 1-31
Amplitude Limiter Circuit 1-31
Output Network 1-31
Operating Mode Selection and Indication Circuit 1-31
Equalization Selection 1-32
Pilot Signal $\quad 1-32$
Power Supply Filter Network 1-32
ECU Power Supply Assembly 1-32
TRANSMITTER ECU MAINTENANCE
Introduction $2-1$
Safety Considerations $\quad 2-1$
ECU Circuit Board Installation/Removal 2-1
First Level Maintenance 2-2
Cleaning and Inspection $\quad 2-2$
Second Level Maintenance 2 2-2
Electrical Adjustments 2-2
ECU Extender Circuit Board Operation 2-3
Controller Circuit Board Adjustments 2-3
P1 Set - P5 Set Controls 2-3
FWD and RFL Calibrations 2-3
ECU Meter Switch Circuit Board Adjustments 2-3
Forward Power Meter Low and High Scale 2-3
Calibrations
Reflected Power Meter Low and High Scale 2-3
Calibrations
FWD and RFL Calibrations 2-4
Stereo Circuit Board Adjustments 2-4
Stereo Adjustment 2-4
Exciter Circuit Board Adjustments 2-4
Modulation Calibration 2-4
Phase Modulator Calibration $\quad 2-4$
Symmetry Control 2-4
IPM Correction Circuit Controls 2-4
Single Chan Mono Level Control 2-4
Average Modulation Limit Control $\quad 2-4$
Neg Limit Control $\quad 2-4$
Frequency Calibration Control $\quad 2-5$

| PARAGRAPH |  | PAGE NO. |
| :---: | :---: | :---: |
| 2-58 | Display Circuit Board Adjustments | 2-6 |
| 2-59 | $\mathrm{L} / \mathrm{L}+\mathrm{R}$ and R/L-R Display Calibration Control | 2-6 |
| 2-66 | Troubleshooting | 2-6 |
| 2-67 | Safety Considerations | 2-6 |
| 2-68 | Troubleshooting Procedures | 2-7 |
| 2-69 | Component Replacement Procedure | 2-11 |
| SECTION III | ECU ASSEMBLY PARTS LIST |  |
| 3-1 | Introduction | 3-1 |
| SECTION IV | ECU ASSEMBLY DRAWINGS |  |
| 4-1 | Introduction | 4-1 |
|  | LIST OF ILLUSTRATIONS |  |
| FIGURE | TITLE | PAGE NO. |
| 1-1 | CONTROLLER CIRCUIT BOARD | 1-5 |
|  | SIMPLIFIED SCHEMATIC |  |
| 1-2 | EXCITER CIRCUIT BOARD | 1-21 |
|  | SIMPLIFIED SCHEMATIC |  |
| 1-3 | STEREO CIRCUIT BOARD | 1-27 |
|  | SIMPLIFIED SCHEMATIC |  |
|  | LIST OF TABLES |  |
| TABLE | TITLE | PAGE NO. |
| 2-1 | EXCITER CIRCUIT BOARD TROUBLESHOOTING | 2-7 |
| 2-2 | STEREO CIRCUIT BOARD TROUBLESHOOTING | 2-9 |
| 2-3 | CONTROLLER CIRCUIT BOARD | 2-10 |
|  | TROUBLESHOOTING |  |
| 2-4 | ECU POWER SUPPLY TROUBLESHOOTING | 2-11 |
| 3-1 | REPLACEABLE PARTS LIST INDEX | 3-1 |

# SECTION I ECU THEORY OF OPERATION 

## 1-1. INTRODUCTION.

1-2. This section presents a general description of the Broadcast Electronics AM-10A/AM-6A transmitter ECU (Exciter/Controller unit).

1-3. GENERAL DESCRIPTION.
1-4. The AM-10A/AM-6A transmitter control, status/monitoring circuitry, audio/power PWM generation, stereo generation circuitry, and meter display circuitry is contained in the ECU (Exciter/Controller unit) assembly. The ECU is a modular control center designed for the installation of the: 1) controller circuit board assembly, 2) ECU display and switch circuit boards, 3) transmitter forward/reflected power meter displays, 4) exciter circuit board assembly, 5) stereo generator circuit board assembly, and 6) ECU power supply assembly.

## 1-5. FUNCTIONAL DESCRIPTION.

## 1-6. ECU DISPLAY CIRCUIT BOARD.

1-7. The ECU display circuit board contains the controller status display indicators, the power control switch/indicators, and meter display circuitry (refer to schematic diagram SD917-0206-001/-008). The circuit board is equipped with the following display indicators: 1) exciter, 2) power supply, 3) power module, 4) antenna, 5) interlock, 6) remote control, 7) lightning, 8) antenna interlock, 9) foldback, and 10) over-temperature. Control switches include power level 1, power level 2, power level 3 , power level 4, power level 5, raise power, and lower power switch/indicators. The meter display circuitry consists of a driver circuit and a stereo 30 -segment LED bar-graph display.

1-8. The ECU display circuit board also contains left/L+R and right/L-R audio metering circuits. The left/L+R and right/L-R metering circuits are identical. Therefore, only the left/L+R metering circuit will be discussed in the following text.

1-9. EXCITER MONITOR MODE CONTROL CIRCUIT. Left, right, and L+R metering samples from the exciter circuit board and an L-R meter sample from the stereo circuit board are applied to integrated circuit U1. U1 is controlled by latch U5A and mode switch S1. When S1 is depressed, a LOW is applied to inverter U4B. U4B outputs a HIGH to clock latch U5A. The Q output of U5A will respond by routing a HIGH to: 1) U1 and 2) bias Q3 on to illuminate the $\mathrm{L}+\mathrm{R} / \mathrm{L}-\mathrm{R}$ switch LED. U1 will select $\mathrm{L}+\mathrm{R} / \mathrm{L}-\mathrm{R}$ information for application to the autorange circuitry. When S1 is depressed again, a HIGH from U4B will clock latch U5A. The $\bar{Q}$ output of U5A will respond by routing a HIGH to: 1) U1 and 2) bias Q4 on to illuminate the left/right switch LED. U1 will select left/right channel audio for application to the autorange circuit.

1-10. AUTORANGE CIRCUIT. The autorange circuit consists of integrated circuits U2A, U3A, and U3B. An output of U1 is routed to integrated circuit U2A and U3A. U3A is configured as an amplifier stage. U2A is configured as an amplifier/buffer stage. When audio is applied to the circuit, U3A amplifies the audio. The output of U3A is half-wave rectified by diode D1. The output of D1 is applied to integrated circuit U3B. U3B is configured as a comparator. When the audio level is above the threshold at U3B, U3B will output a HIGH to transistor Q1. The HIGH biases Q1 off to configure U2A as a buffer. When the audio level is below the threshold at U3B, U3B will output a LOW to: 1) bias Q1 on to configure U2A as an amplifier with a gain of 10 and 2) illuminate X10 indicator DS1. The output of U2A is routed for application to the polarity control circuit.

1-11. POLARITY CONTROL CIRCUIT. Positive or negative signal monitoring is controlled by polarity switch S2. Audio from the mode control circuit is applied to integrated circuit U6A and U7. U6A is configured as an inverting buffer. When S 1 is depressed, a LOW is applied to inverter U4C. U4C outputs a HIGH to clock latch U5B. The Q output of U5B will respond by routing a HIGH to: 1) U7 and 2) bias Q 6 on to illuminate the negative switch LED. U7 will select inverted audio from U6A for application to a rectifier circuit. When S1 is depressed again, a HIGH from U4C will clock latch U5B. U5B will respond by routing a HIGH to: 1) U7 and 2) bias Q5 on to illuminate the positive switch LED. U7 will select non-inverted audio for application to a rectifier circuit.

1-12. HALF-WAVE RECTIFIER CIRCUIT. Integrated circuit U8A and U8B function as a half-wave rectifier circuit. Audio from integrated circuit U7 is applied to U8A/U8B. U8A/U8B half-wave rectify the audio for application to the meter display circuitry. Resistor R38 and capacitor C21 establish the meter ballistics.

1-13. METER CIRCUITRY. The output of the half-wave rectifier circuit is applied to a meter circuit consisting of: 1) integrated circuits U9, U10, and U11, and 2) 10 -segment LEDs DS7, DS8, and DS9. The output from U8B is applied to meter drivers U9, U10, and U11. U9/U10/U11 control 10-segment LED sections DS7, DS8 and DS9. Drivers U9/U10/U11 function to illuminate the required segments of DS7/DS8/DS9 to display the left/L+R levels. One-shot U12 is provided to identify short modulation peaks.

1-14. INDICATOR CIRCUITRY. The display circuit board is equipped with several indicators. DS22, DS23, DS24, and DS25 are bi-color LEDs providing status indications for the exciter, power supply, RF power modules, and antenna. The indicators are controlled by drivers on the controller circuit board. When activated, the drivers will output a HIGH to illuminate the indicators. A yellow display is generated when the red and green LEDs are illuminated simultaneously.
1-15. Indicators DS15 through DS20 provide status indications for over-temperature, foldback, antenna conflict, lightning, remote control, and interlock conditions. The indicators are controlled by drivers on the controller circuit board. When activated, the drivers will output a LOW to illuminate the indicators.

1-16. RESET SWITCH. The reset of fault conditions is provided by switch S3. When S3 is depressed, a HIGH is routed to the controller circuit board to reset the fault conditions. The switch LED will illuminate when one of the following fault condition occurs: 1) over-temperature, 2) exciter, 3) power supply, 4) RF power module, 5) reflected power high, 6) reflected power emergency, 7) lightning conditions, or 8) $1.2: 1$ VSWR.
1-17. ECU SWITCH CIRCUIT BOARD.
1-18. ECU power level switches S803 through S807, raise switch S801, lower switch S802, and off switch S 808 are located on the controller switch circuit board (refer to schematic diagram SD917-0206-001/-008). The switches output +15 volts to activate a function.

## 1-19. ECU METER SWITCH CIRCUIT BOARD.

1-20. ECU meter switches S501 and S502 are located on the ECU meter switch circuit board (refer to schematic diagram SD917-0206-005). The switches control the signals applied to the forward and reflected power meters. Low scale control R501 and high scale control R503 calibrate the forward power meter. Low scale control R505, high scale control 506, and ac sample control R511 calibrate the reflected power meter.

1-21. MOTHERBOARD.
1-22. The interfacing of transmitter status signals, audio, PWM/RF drive signals, and operating commands to/from the ECU circuit boards is provided by the ECU motherboard assembly (refer to schematic diagram SB917-0201). Connectors J4, J5, and J6 route status inputs and control commands to/from the ECU assembly. 80-pin connector J101 is provided for the exciter circuit board. $50-$ pin connector J201 is provided for the stereo exciter circuit board. 80-pin connector J302 and 50-pin connector J301 are provided for the controller circuit board. Connector J8 routes status signals to/from the display circuit board. Connector J10 routes control and status signals to/from the switch circuit board.

1-23. The motherboard also contains RFI filters for the ECU remote inputs and outputs. The filter circuitry consists of single PI-section low-pass RC and LC networks. The networks prevent RFI from entering the exciter and controller circuitry.

1-24. CONTROLLER CIRCUIT BOARD.
1-25. All transmitter operations are directed by the controller circuit board (refer to Figure $1-1$ ). The controller circuit board is a digital CMOS logic assembly containing control and parameter monitoring/display circuitry. The control circuitry includes an antenna interlock circuit, a power control network, and a foldback control circuit. The monitor/display circuitry includes exciter, power supply, power module, antenna, interlock, remote control, lightning, antenna interlock, foldback, and over-temperature networks. The circuitry determines the transmitter output power control operating characteristics and responses to fault conditions such as an ac power failure, load failure, power supply failure, or remote control unit failure.

1-26. CABINET/EXTERNAL INTERLOCK AND REMOTE CONTROL FAIL-SAFE. The controller circuit board monitors: 1) an external interlock and 2) a remote control fail-safe interlock. The external interlock is any interlock external to the transmitter such as a test load interlock. The remote control fail-safe is an input requiring a +5 to +15 volt signal to indicate the remote control unit is operational. If the external interlock and the remote control fail-safe are closed, the ECU interlock indicator will illuminate and the transmitter may be energized. If the external interlock opens or the remote control fail-safe signal is removed, the transmitter will immediately de-energize and the interlock indicator will extinguish.

1-27. External Interlock. The transmitter external interlock is an optically coupled input designed to accept the output of a series interlock switch circuit external to the transmitter. The circuit accepts a +5 volt to +15 volt output of an interlock circuit external to the transmitter such as from a test load. Optical coupling of the external interlock input to the controller circuitry is provided by U11. Diode D17 protects the circuit from a reverse polarity potential applied to the input.

1-28. A HIGH is required at the input of coupler U11 when the external interlock is closed. U11 will output a HIGH to OR gate U69B in the transmitter enable circuit. The HIGH will configure U69B to output a HIGH to AND gate U71B. U71B will output a HIGH cabinet command to allow the transmitter to be energized. U71B also outputs a HIGH to NAND gate U71D. With a HIGH fail-safe command, U71D will output a HIGH to illuminate the interlock indicator. When the external interlock is opened, a LOW is applied to U11. The output of U11 will go LOW. OR gate U69B will respond by outputting a LOW to AND gate U71B. U71B will output a LOW cabinet command. A LOW cabinet command configures a power control circuit to operate the transmitter to off. U71D will output a LOW to: 1) extinguish the interlock indicator and 2) generate a LOW operate command. A LOW operate command mutes: 1) the exciter PWM signal and 2) the power supply circuit board(s).

1-29. Remote Control Fail-safe. The remote control fail-safe input is designed to accept a +5 to +15 volt output from the remote control unit fail-safe connection. The signal is optically coupled to the controller circuitry by integrated circuit U56. Diode D23 protects the circuit from a reverse polarity potential applied to the input.

1-30. A HIGH is required at the input of U56 to indicate when the remote control unit is operational. The output of coupler U56 will go HIGH. The HIGH will configure OR gate U45C to output a HIGH fail-safe signal. The fail-safe signal is applied to AND gate U71D. With a HIGH cabinet signal, U71D will output a HIGH to illuminate the interlock indicator. The HIGH will also bias driver transistor Q48 on to illuminate remote fail-safe indicator DS2. When the remote control fail-safe signal is removed, a LOW is applied to U56. The output of U56 will go LOW. The LOW generates a LOW transmitter operate command to mute: 1) the exciter PWM signal, 2) the power supply circuit board(s), and 3) extinguish remote fail-safe indicator DS2. The LOW from U56 will generate a LOW fail-safe command. The LOW is applied to U71D. U71D will output a LOW to extinguish the interlock indicator.

1-31. EXTERNAL MUTE. The controller circuit board monitors the transmitter mute signal. The external mute input is designed to accept a +5 to +15 volt output from an antenna switch controller RF mute circuit. The signal is optically coupled to the controller circuitry by U10. Diode D16 protects the circuit from a reverse polarity potential applied to the input.
1-32. A HIGH is required at the input of coupler U10 when the external mute circuit is required to mute the transmitter RF power output. U10 will output a HIGH to OR gate U13C and NOR gate U24A. U13C will output a HIGH to inverter U25A. U25A will output a LOW to U22B. The LOW will configure U22B to output a LOW operate command to mute: 1) the exciter PWM signal and 2) the power supply circuit board(s). U24A will output a LOW to disable the antenna conflict indicator operations.

1-33. ANTENNA INTERLOCK. The controller circuit board is equipped with an antenna interlock circuit. The circuit accepts: 1) control signals from power levels 2 through 5 , and 2) status inputs from three antenna systems. The antenna interlock circuit consists of: 1) programming switches $S 1$ through $\mathrm{S} 3,2$ ) OR gates U12A/B and U21A/B, and 3) NAND gates U20A through U20D. The circuit analyzes the information and determines if a correct antenna system and power level is selected for operation.



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1-34. To provide an operational example, antenna 1 is designed to operate with power level 2. When antenna 1 is connected to the transmitter, a HIGH status signal is applied to optical coupler U7. U7 outputs a HIGH to switch S1. S1 is a four-section SPST switch. The S1 switch sections are assigned the following power levels: 1) power level 2, 2) power level 3,3 ) power level 4, and 4) power level 5 . The switch is programmed by closing the switch sections for the power levels which are acceptable for the antenna 1 system. The outputs of programming switch S1 are applied to a control network consisting of: 1) a power level 2 circuit, 2) a power level 3 circuit, 3) a power level 4 circuit, and 4) a power level 5 circuit. Each power level control circuit contains an OR gate to monitor the status of the antenna systems and an AND gate to monitor the status of the selected power level.

1-35. With S1 programmed to operate with power level 2, the HIGH from U7 is applied to OR gate U12A. U12A will output a HIGH to NAND gate U20A. With power level 2 selected, a HIGH from BCD-to-decimal decoder U18 will be applied to U20A. U20A will respond by routing a HIGH to OR gate U21C. U21C will output a HIGH to OR gate U13B. Programmable jumper J1 is provided to disable the antenna interlock circuit. With the antenna interlock circuit enabled, U13B will output a HIGH to NOR gate U24A and AND gate U22B. With no mute or off commands present, U24A will output a LOW to disable antenna conflict indicator driver Q16. With a closed interlock system and no ac failures or fail-safe conditions present, U22B will output a HIGH operate command to enable the transmitter.

1-36. REMOTE CONTROL. The transmitter control functions, status indications, and metering signals are designed for remote operation. Control functions require a +5 volt to +15 volt dc signal to activate the function. Status indications will output a LOW ( 0 volts) when active. The remote meter indications can be programmed for +5 volt or +2.5 volt full-scale meter operations. The circuitry may be interfaced to any type of remote control unit.

1-37. Remote control of the transmitter is enabled or disabled by remote/local switch S4. S4 enables remote control operation by applying a positive voltage to optical couplers U1 through U6, U32/U33, and U53. S4 disables remote control operation by applying a ground to the couplers. The remote position allows both local and remote transmitter control. The local position allows only local control of the transmitter. The remote control inputs and outputs are RFI filtered on the motherboard for maximum reliability.

1-38. POWER ON. A transmitter power on operation initiates a sequence to determine if all the interlocks are closed and the remote control unit is operational. RF output power from the transmitter is enabled by commands from the power level 1 through power level 5 switch/indicators. Each power level switch/indicator provides a one-button power on start command and configures the transmitter for a specific power output level. Each switch/indicator will illuminate as selected to indicate the command has been received and stored by the controller power control circuit.

1-39. Transmitter power is enabled when a power level switch/indicator is activated. For example, when the ECU power level 2 switch/indicator is depressed, a HIGH is applied to priority encoder U14. When a remote power level 2 command activated, a HIGH is applied to optical coupler U4. U4 will output a HIGH to U14. U14 analyzes power level and off commands to determine priorities when two switches are operated simultaneously. The off command is assigned the highest priority. When the power level 2 command is received, U14 will output a binary number to latch U 15 . U15 outputs the binary number to latch U17. U15 and U17 operate in association to provide the appropriate output timing of the binary number to the antenna interlock circuit and to the power control circuit.

1-40. The binary power level 2 command from latch U17 is routed to: 1) BCD-to-decimal decoder U18 and 2) multiplexer U39. U18 is designed to decode the binary number from U17 and output a HIGH on the appropriate control line to indicate the selected power level. With the power level 2 selected, a HIGH from BCD-to-decimal decoder U18 is applied to AND gate U20A. With antenna 1 switch S1 programmed to operate with power level 2, a HIGH from OR gate U12A is also applied to U20A. U20A will respond by routing a HIGH to OR gate U21C. U21C will output a HIGH to OR gate U13B. U13B will output a HIGH to U22B.

1-41. AND gates U69B, U71B, and U71D monitor the status of the external interlock, the remote control fail-safe input, and the external/exciter mute commands. The circuit functions to determine if all the interlocks are closed, the remote control unit is operational, and the exciter is operational. If the external interlock is closed and the remote control unit is operational, U71D will output a HIGH to U22B. If no external or exciter mute commands are present, U13C will output a LOW to inverter U25A. U25A will output a HIGH to U22B. With a HIGH antenna interlock signal from U13B indicating a proper antenna/power level selection, U22B will output a HIGH operate command to the power control circuit, an exciter/power supply mute circuit, and a high reflected power circuit.
1-42. The HIGH operate signal is routed to the power control circuit to allow the transmitter to be energized. If the remote control unit fails, or the external or exciter mute signal is activated, U22B will output a LOW operate command. The LOW operate command mutes: 1) the exciter PWM signal and 2) the power supply circuit board(s). If the cabinet or external interlock is opened, AND gate U71B will output a LOW cabinet command. A LOW cabinet command configures the power control circuit to operate the transmitter to off. U71D will output a LOW to: 1) extinguish the interlock indicator and 2) generate a LOW operate command. A LOW operate command mutes: 1) the exciter PWM signal and 2) the power supply circuit board(s).

1-43. POWER CONTROL CIRCUIT. Binary power level information from latch U17 is applied to multiplexer U39. U39 decodes the power level number and selects a reference voltage from a potentiometer network. Potentiometers R2 through R6 provide a voltage reference proportional to output power for power levels 1 through 5 . For example, power level 2 selected for operation. With power level 2 selected, U39 will select a reference voltage from potentiometer R5. The voltage is routed through buffer U40B to digital-to-analog converter U42.

1-44. U42 is designed to output a reference voltage to a power control driver circuit. U42 is controlled by up/down counters U30 and U31, multiplexer U27, priority encoder U28, and divider U26. The up/down counters, multiplexer, and priority encoder function to output clock signals to U42 in response to fault conditions. U42 will respond by increasing/decreasing the power reference voltage in response to foldback and release commands from U27. With no foldback or release signals, U42 will output the power level 2 reference voltage without change to a power control driver circuit.

1-45. Power Control Driver Circuit. The power control driver circuit consists of: 1) operational amplifiers U40B and U44A, 2) switch U41A, and 3) AND gate U36C. The power level reference voltage from U42 is applied to integrated circuit U40B. U40B is configured as an inverting amplifier. The output of U40B is applied to comparator U44A and switch U 41 A . U 41 A is controlled by the sample from the output of U 44 A . U41A is a feedback control network designed to convert the reference voltage from U40B to a voltage proportional to power. U44A compares the power level reference to a ramp signal generated by integrated circuit U40C. U44A produces a square-wave PWM (pulse-width-modulated) signal which varies in response to the power level. The signal is ANDed at U36C with the operate signal from U22B. With a HIGH operate signal from U22B, the PWM signal is routed through carrier control driver Q22 to the power supply circuit board.

1-46. POWER CONTROL TRIM CIRCUIT. The transmitter RF output power level can be trimmed to a desired level by the raise/lower switch/indicators. When a raise or lower switch/indicator is depressed, a HIGH is applied to the raise/lower power adjust circuit. The circuit consists of: 1) logic gates U24B, U31D, U16B, U23C, and U19C, 2) up/down counters U34 and U35, and 3) digital-to-analog converter U43. The circuit is designed to increase or decrease RF output power by increasing/decreasing the reference voltage.

1-47. Logic gates U24B, U31D, U16B, U23C, and U19C control up/down counters U34 and U35. NOR gate U24B and OR gate U31D monitor raise, lower, and foldback signals. NOR gate U24B is designed to configure counters U34/U35 to count up or down. U24B will output a HIGH to configure U34/U35 to count up. U24B will output a LOW to configure U34/U35 to count down. For example, when the raise switch/indicator is depressed, a HIGH is applied to U34/U35. The HIGH configures U34/U35 to count up. U34/U35 will output binary numbers to digital-to-analog converter U43. U43 decodes the numbers from $\mathrm{U} 34 / \mathrm{U} 35$ and increases the power control reference voltage generated from power control D-to-A converter U42. U42 outputs the increased reference voltage to the power control driver circuit to increase the RF output power.

1-48. Logic gates U16B, U23C, and U19C control the loading of counters U34/U35. The logic gates monitor: 1) high reflected power conditions, 2) reset conditions, and 3) trim reset operations. Trim reset is when the power control trim is reset to mid-range when a power level switch/indicator is depressed. If a trim reset condition, a reset condition, or a high reflected power condition occurs, U19C will output a HIGH to counters U34/U35. The HIGH resets counters U34/U35 to mid-range.

1-49. Trim Reset. Trim reset is a function which resets the power control trim function to mid-range when a power level switch/indicator is depressed. When a power level switch is depressed, a HIGH trim reset command from U14 is applied through jumper P12 to OR gate U19C. U19C will output a HIGH to up/down counters U34/U35. The HIGH configures U34/U35 to mid-range. With U34/U35 at mid-range, the power trim circuit can be raised or lowered an equal amount. Jumper P12 allows the trim reset function to be disabled if required.

1-50. TRANSMITTER OFF. RF output power is immediately terminated when the ECU off switch is depressed. When the off switch/indicator is depressed, a HIGH is applied to OR gate U13A. U13A will output a HIGH to priority encoder U14. U14 will output a binary number through latches U15/U17 to BCD-to-decimal decoder U18 and to multiplexer U39. U18 will output a HIGH to NOR gate U23A. U23A will output a HIGH to bias power contactor driver Q13 off to disable the fans and the power supplies. U39 will respond by terminating the power control reference voltage to terminate the power control PWM signal

1-51. AC POWER INTERRUPTIONS. The AM-10A/AM-6A transmitters are designed to respond to two different types of ac power interruptions: 1) momentary and 2) extended. The transmitter will respond to a momentary power interruption by automatically returning to on-air operation immediately after power is returned to the transmitter. Automatic return of the transmitter to on-air operation is provided by the controller circuit board battery backup circuit which maintains the transmitter configuration information. In the event of an extended ac power interruption, the controller circuit board is equipped with a programmable ac loss/auto-off circuit. The circuit is designed to output an off command once power is returned to the transmitter. The ac loss circuit may be programmed to output an off command after a 1 minute, 4.5 minute, 17 minute, or 68 minute ac power interruption. The circuit primarily designed to be used to prevent the transmitter from automatically returning to an incorrect antenna or power level after a power failure.
1-52. The ac loss detection/auto-off circuit consists of: 1) one-shots U57A/U68B, 2) divider U58, 3) OR gate U62C, 4) NOR gate U52A, and inverter U54C. When ac power is applied to the unit, 120 Hz pulses from an ac detection circuit on the power supply circuit board are applied to integrated circuit U68B. U68B will respond by routing a LOW pulse to: 1) one-shot U57A, 2) OR gate U62C, and 3) inverter U54C. One-shot U57A responds by providing a one second delay to allow the circuitry to stabilize. U54C responds by inverting the LOW to provide a HIGH reset pulse to counter U58. The HIGH disables counter U58 and prevents the counter from generating an ac fail command.

1-53. When ac power interruption is detected, U68B: 1) routes a HIGH pulse to one-shot U57A, OR gate U62C, and inverter U54C and 2) outputs a LOW ac fail command. U57A will output a HIGH to U62C. U62C will output a a HIGH ac fail command. U54C inverts HIGH to output a LOW to counter U58. U58 will begin a count operation. 0.5 Hz clock pulses for U58 are provided by U52A and an battery backed-up oscillator. Programmable jumper P6 programs the counter to provide a $1,4.5,17$, or 68 minute shutdown command. When the programmed time has elapsed, U58 will output a HIGH shutdown command to OR gate U37A. The HIGH is routed through U37A and U31A to priority encoder U14 to automatically operate the transmitter to off.

1-54. The shutdown signal is also applied to AND gate U71C. If fault conditions have occurred, U71C will AND a LOW from NOR gate U55 to output a LOW to latch U49D. U49D will output a LOW to bias transistor Q52 on to maintain the battery supply and the fault indication circuitry. If no fault conditions exist, U71C will AND a HIGH from NOR gate U55. U71C will output a HIGH to latch U49D. U49D will output a HIGH to bias transistor Q52 off to terminate battery operation.

1-55. FORWARD AND REFLECTED POWER CIRCUITRY. Transmitter forward and reflected power voltage samples are processed by forward and reflected power monitoring circuits. The circuits are identical therefore, only the forward power circuit will be described.

1-56. A voltage sample of the forward power is applied through potentiometer R56 and resistor R183 to integrated circuit U63D. Potentiometer R56 allows the forward power circuit to be calibrated. U63D operates in association with diodes D35/D36 as a full-wave rectifier. The full-wave rectified output from U63D is applied to a third order high-pass filter consisting of U63A, R60, R61, R67, C63, C64, and C88. The dc output of the filter is applied to comparator U61D. U61D compares the forward power sample to a ramp voltage generated by integrated circuit U40C. U61D will output a square-wave signal equal to the forward power voltage sample. The output of U63D is applied to switch U41B. U41B functions as a feedback control device designed to convert the forward power voltage sample into a signal proportional to power. The square-wave output from U41B is applied to a low-pass filter consisting of resistor R70 and capacitor C89. The output of the low-pass filter generates a dc voltage which is proportional to the forward power. The voltage is amplified by operational amplifier U64A. The output of U64A is applied to: 1) the fault detection circuitry, 2 ) a +5 volt full-scale meter output, and 3) buffer U64B. Buffer U64B operates in association with programmable jumper P2 to provide a +2.5 volt full-scale meter output. Jumper P2 enables or disables the +2.5 volt full-scale meter output.

1-57. FOLDBACK PROTECTION. The controller circuit board is designed to monitor several operating parameters for problem conditions. Several of the monitored conditions are routed to a foldback circuit. The foldback circuit will automatically reduce the transmitter RF output power to an acceptable operating level to prevent damage to the transmitter. The controller monitors: 1) the cabinet temperature for over-temperature conditions, 2) reflected power for a high reflected power condition, 3) forward power for high forward power conditions, and 4) lightning detector for lightning conditions. When an over-temperature, high reflected power, or a high VSWR condition occurs, the foldback indicator will illuminate to indicate the transmitter is in a foldback condition.

1-58. If the controller detects a high reflected/forward power, a high VSWR, lightning, or an over-temperature condition, the foldback circuit will automatically reduce the transmitter RF output power to an acceptable operating level to prevent damage to the transmitter. If the controller detects a high reflected power or VSWR condition, the antenna status indicator will illuminate as described below to indicate the problem.

## ANTENNA STATUS INDICATOR

CONDITION

YELLOW
RED

FLASHING RED
1.2:1 VSWR or greater.

High reflected power condition. A reflected power condition equal to 400 watts for AM-10A models or 240 watts for AM-6A models.

Reflected power emergency condition. A reflected power condition equal to 2000 watts for AM-10A models or 1200 watts for AM-6A models.

1-59. High Forward Power Circuitry. High forward power conditions are monitored by a high forward power fault detection circuit. Integrated circuits U66A and U66B are configured as comparators designed to monitor forward power conditions. U66B functions as an output power monitor. Integrated circuit U66B compares a forward power sample from U64A to a power control sample. U66A compares a forward power sample from U41B to a voltage reference.

1-60. Comparators U66A/U66B operate in association to monitor high forward power conditions. U66A/U66B use the high reflected power attack circuitry to reduce the transmitter power when a high forward power condition occurs. When the transmitter power is greater than $90 \%$, U66B will output a HIGH. When a high forward power conditions results in the forward power sample to increase above the voltage reference by approximately $20 \%$, the output of U66A will go HIGH. The HIGH is applied to AND gate U47B. With a HIGH from U66B, U47B will output a HIGH to OR gate U62A. U62A will output a HIGH to AND gate U47A. With a HIGH enable failure signal, U47A will output: 1) a HIGH reflected power high attack signal to priority encoder U28 and 2) a HIGH to latch U67A. The HIGH reflected power attack signal is used by U28 to initiate an attack sequence to reduce the transmitter output power. The HIGH to U67A will configure U67A to output a HIGH reflected power signal to enable latch U48D. U48D will output a HIGH to bias: 1) alarm status indicator driver transistors Q34 and Q35 on and 2) antenna indicator driver Q28 on. When the transmitter power is reduced to approximately $90 \%$, the output of U66B will go LOW. The LOW is applied to U47B. U47B will output a LOW through U62A to U47A. U47A will respond by routing a LOW to terminate the high reflected power attack signal. The indicators will remain illuminated until the alarm reset switch is depressed.

1-61. High Reflected Power Circuitry. Integrated circuit U65C monitors reflected power conditions. U65C compares a reflected power sample from U64C to a voltage reference. When the reflected power sample increases above the voltage reference, the output of U65C will go HIGH. The HIGH is applied through OR gate U62A to AND gate U47A. With a HIGH enable failure signal, U47A will output: 1) a HIGH reflected power high attack signal to priority encoder U28 and 2) a HIGH to latch U67A. The HIGH reflected power attack signal is used by U28 to initiate an attack sequence to reduce the transmitter output power. The HIGH to U67A will configure U67A to output a HIGH reflected power signal to enable latch U48D. U48D will output a to HIGH to bias: 1) alarm status indicator driver transistors Q34 and Q35 on and 2) antenna mismatch indicator driver Q28 on.

1-62. Over-temperature Circuitry. Over-temperature conditions are monitored by an over-temperature fault detection circuit. A dc voltage representing the transmitter temperature is applied to: 1) integrated circuits U65A/U65B and 2) integrated circuit U61A. When the temperature voltage increase above a reference voltage, the output of U65A will go HIGH. The HIGH is routed to AND gate U51D. With a HIGH enable failure signal, U51D will output: 1) a HIGH over-temperature attack signal to priority encoder U28 and 2) a HIGH to latch U67C. The HIGH over temperature attack signal is used by U28 to initiate an attack sequence to reduce the transmitter output power. The HIGH to U67C will configure U67C to output a HIGH: 1) over-temperature signal to latch U49B and 2) to AND gate U47D. The output of U49B will go HIGH to bias: 1) alarm status indicator driver transistors Q34 and Q35 on and 2) over-temperature indicator drivers Q32 and Q36 on. When the transmitter temperature is reduced to 70 degrees C, the output of U65A will go LOW and the output of U65B will go HIGH. The LOW is applied to U51D. U51D will output a LOW to terminate the over-temperature attack signal. The indicators will remain illuminated until the alarm reset switch is depressed. The from HIGH from U65B is also applied to U47D. With the HIGH from U67C, U47D will output a over temperature release signal to encoder U28.

1-63. U61A is configured as a comparator designed to monitor extreme temperature conditions. When the temperature voltage increases above the reference voltage, the output of U61A will go HIGH. U61A will output a HIGH temperature shutdown command to U13A of the transmitter off control circuit.

1-64. Reflected Power Emergency. Reflected power emergency conditions are monitored by comparator U66D. U66D compares a reflected power sample to a fast voltage reference from U63C. When a reflected power emergency causes the sample to increase above the reference, the output of U66D will go LOW. The LOW is applied to OR gate U62B. U62B will output a LOW reflected power emergency attack signal to NAND gate U60D. With a HIGH lightning detector signal indicating no lightning activity, U60D will output a HIGH to latch U59A and OR gate U45B. U45B will output a HIGH: 1) to AND gate U47C, 2) to OR gate U19A, and 3) emergency mute command. With a HIGH enable failure signal, U47C will output a HIGH fast foldback attack signal to priority encoder U28. U19A will output a HIGH to: 1) bias driver transistor Q50 on to illuminate PWM mute indicator DS3 and 2) inverter U54A. U54A will output a LOW to bias driver transistor Q51 off to mute the PWM signal.
1-65. A LOW reflected power emergency attack signal is also applied to inverter U60C. U60C will output a HIGH to OR gate U69C. U69C is designed as a latching gate. When a reflected power emergency attack signal is present, a LOW foldback reset command will bias transistor Q56 off. This allows the output of U69C to be latched HIGH to maintain the indicator circuitry when the condition is removed.

1-66. The HIGH from U69C is applied to reflected power emergency latch U49A. The output of U49A will go HIGH. The HIGH is applied to: 1) OR gate U50B, 2) NOR gate U55, 3) AND gate U51A, and 4) transistor Q29. OR gate U50B will output a HIGH to bias Q39 off to disable the green antenna status indicator. NOR gate U55 will output a LOW which is inverted at U54F. U54F will output a HIGH to bias Q34 and Q35 on to enable the alarm indicator. U51A ANDs a 2 Hz signal with the HIGH from U49A to generate a flashing signal to OR gate U50C. U50C will output the signal through U51 and U50 to transistor Q38. The output of Q38 will flash to generate a flashing red antenna status indicator. Transistor Q29 will be biased on to provide a LOW remote reflected power emergency signal.

1-67. Lightning Conditions. Lightning conditions are monitored by NAND gate U60D. When lightning is detected at the transmitter output, the lightning detector status input will go LOW. The LOW is applied to NAND gate U60D and inverter U46B. U60D will output a HIGH to latch U59A and to OR gate U45B. With a HIGH from U60D, U45B will output a HIGH: 1) to AND gate U47C, 2) to OR gate U19A, and 3) emergency mute command. With a HIGH enable failure signal, U47C will output a HIGH fast foldback attack signal to priority encoder U28. U19A will output a HIGH to: 1) bias driver transistor Q50 on to illuminate PWM mute indicator DS3 and 2) inverter U54A. U54A will output a LOW to bias driver transistor Q51 off to mute the PWM signal.
1-68. Inverter U46B will respond by routing a HIGH to latch U49C. The output of U49C will go HIGH. The HIGH is applied to NOR gate U55 and to transistors Q33 and Q37. The HIGH will bias Q33 and Q37 on to illuminate the lightning status indicators. NOR gate U55 will output a LOW which is inverted at U54F. U54F will output a HIGH to bias Q34 and Q35 on to enable the alarm indicator.

1-69. Foldback Indication. Two circuit functions are monitored to indicate when the transmitter is in a foldback condition: 1) when the Q2 output of U28 is HIGH and 2) when the carryout signal of U31 is HIGH. When priority encoder U28 outputs a binary number in response to an attack signal, the Q2 output of U28 will be HIGH. The HIGH is applied to latch U67D. The Q output of U67D will go HIGH. The HIGH is inverted at U25C and applied to NAND gate U16C.

1-70. When a foldback condition, counter U31 will not be clocked to a maximum number resulting in a HIGH carryout signal. The HIGH is inverted at U25B. U25B will output a LOW to U16C. With a LOW from U25B or U25C, U16C will output a HIGH to foldback indicator driver transistors Q20 and Q21. The transistors will be biased on to indicate the transmitter is in a foldback condition.

1-71. ATTACK SIGNAL OPERATION. During high reflected/forward power, reflected power emergency, over-temperature, or lightning conditions, an attack signal is applied to priority encoder U28. U28 is designed to determine priorities if two attack signals occur simultaneously. U28 will respond by routing a binary number to multiplexer U27. U27 will respond by selecting a clock signal from integrated circuit U26. U26 is a divider designed to generate several clock signals. The clock signals are used to drive the power control circuit up/down counters up or down as determined by the type of attack or release signal applied to U28. For example, a high reflected power condition selects a 4 Hz clock signal. An over-temperature signal will select a $1 / 16 \mathrm{th} \mathrm{Hz}$ clock signal.

1-72. The signal from U27 is applied to up/down counters U30/U31. U30/U31 will respond by counting down and routing binary numbers to digital-to-analog converter U42. U42 will respond by routing a reduced voltage reference to U43. U43 will output a reduced reference voltage to reduce the transmitter output power.

1-73. $1.2: 1$ VSWR CONDITIONS. $1.2: 1$ VSWR conditions are monitored by a VSWR detection circuit. The detection circuit consists of comparator U66C. U66C compares a forward power sample to a reflected power sample. When the reflected power sample increases above a forward power sample at approximately 1.2: 1, the output of U66C will go LOW. The LOW is inverted at U54E. U54E will output a HIGH 1.2:1 VSWR signal to OR gate U50C. U50C will output a HIGH to AND gate U51B and NAND gate U52C. With a LOW reflected power emergency signal from U51A, U51B will output a LOW to AND gate U50D. With a HIGH from U50C and a LOW from U51A, AND gate U52C will output a LOW to U50D. U50D will respond by routing a LOW to antenna status red indicator driver Q38. The output of Q38 will go LOW to bias the red antenna indicator on. With no reflected power conditions, the output of OR gate U50B will be LOW. The LOW biases the green antenna indicator on. This will result in a yellow antenna LED indication.

1-74. FOLDBACK RECOVERY. When the foldback circuit is activated in response to a problem, the controller will initiate a recovery sequence. The following text describes the reflected power recovery, over temperature recovery, and reflected power emergency/lightning recovery.

1-75. High Reflected Power Recovery. When the reflected power is reduced to a level below the reference at U65C, U65C will output a LOW to U62A. With a LOW from U47B, U62A will output a LOW to U47A. U47A will output a LOW reflected power high attack signal to terminate foldback operation. Once the problem which caused the high reflected power condition is removed, the transmitter will output a high reflected power release signal (refer to the following text).

1-76. High Forward Power Recovery. High forward power conditions use the high reflected power circuitry to reduce/recover the transmitter output power. When the transmitter power is reduced to approximately $90 \%$, the output of comparator U66B will go LOW. The LOW is applied to AND gate U47B. U47B will output a LOW through U62A to AND gate U47A. U47A will respond by routing a LOW to terminate the high reflected power attack signal. Once the problem which caused the high forward power condition is removed, the transmitter will output a high reflected power release signal (refer to the following text).

1-77. High Reflected Power Release Signal. A reflected power release signal is controlled by AND gate U38A. When condition causing the high forward/reflected power condition is removed, a HIGH operate signal, a HIGH 1.2 : 1 VSWR signal from comparator U66C, and a HIGH from latch U67A will be ANDed at U38A. U38A will respond by routing a HIGH reflected power release signal to priority encoder U28. U28 will respond by routing a binary number to multiplexer U27. U27 will respond by selecting a clock signal from integrated circuit U26. U26 is a divider designed to generate several clock signals. The clock signals are used to drive the power control circuit up/down counters up as determined by the type of release signal applied to U28. For example, a high reflected power release condition selects a 2 Hz clock signal. The 2 Hz clock signal from U27 is applied to up/down counters U30/U31. U30/U31 will respond by counting up and routing binary numbers to digital-to-analog converter U42. U42 will respond by routing an increased voltage reference to U43. U43 will output an increased reference voltage to increase the transmitter output power.

1-78. Over-Temperature Recovery. When the condition which caused the over-temperature problem is removed, the transmitter will initiate a recovery sequence. The output of comparator U65A will go LOW. The LOW is applied to AND gate U51D. With a HIGH enable failure signal, U51D will output a LOW to terminate the over-temperature attack signal.

1-79. When the temperature is reduced to approximately 55 degrees C , the output of comparator U65B will go HIGH. The HIGH is applied to AND gate U47D. With the HIGH from latch U67C, U47D will output a HIGH over-temperature release signal to priority encoder U28. U28 will respond by routing a binary number to multiplexer U27. U27 will respond by selecting a $1 / 16 \mathrm{~Hz}$ clock signal from integrated circuit U26. The $1 / 16 \mathrm{~Hz}$ clock signal from U27 is applied to up/down counters U30/U31. U30/U31 will respond by counting up and routing binary numbers to digital-to-analog converter U42. U 42 will respond by routing an increased voltage reference to U43. U43 will output an increased reference voltage to increase the transmitter output power.

1-80. Reflected Power Emergency/Lightning Recovery. When the condition which caused the reflected power emergency/lightning problem is removed, the transmitter will initiate a recovery sequence. The sequence is initiated by comparator U65D. U65D compares a fast reflected power voltage sample to a reference voltage. When the sample voltage is below the reference, the output of U65D will go HIGH. The HIGH is applied to AND gate U71A. With a HIGH from latch U67B, U71A will output a fast foldback release signal to priority encoder U28. U28 will respond by routing a binary number to multiplexer U27. U 27 will respond by selecting a 512 Hz clock signal from integrated circuit U26. The 512 Hz clock signal from U27 is applied to up/down counters U30/U31. U30/U31 will respond by counting up and routing binary numbers to digital-to-analog converter U42. U42 will respond by routing an increased voltage reference to U43. U43 will output an increased reference voltage to increase the transmitter output power.

1-81. In addition to the sequence initiated by U65D, a HIGH foldback reset command is applied to transistor Q56. The HIGH biases Q56 on to unlatch OR gate U69C. U69C will output a LOW to latch U49A to allow the latch to be reset.

1-82. EXCITER MONITORING. The operating condition of the exciter is monitored by a exciter status circuit. During an exciter fault condition, the exciter fault status input will go HIGH. The HIGH is applied to AND gate U36D. With a HIGH enable failure signal, U36D will output a HIGH to latch U48A. U48A will output a HIGH to: 1) bias driver transistor Q45 off to extinguish the exciter indicator green LED and 2) inverter U46A. U46A will output a LOW to bias driver transistor Q44 on. This will illuminate the exciter indicator red LED.

1-83. A HIGH exciter fault signal is also applied to OR gate U13C. U13C will output a HIGH to inverter U25A. U25A will output a LOW to AND gate U22B. U22B will output a LOW transmitter operate command to mute: 1) the exciter PWM signal and 2) the power supply circuit board(s).

1-84. POWER SUPPLY MONITORING. The power supply(s) operating condition is monitored by a power supply status circuit. The following text presents the power supply monitoring operations.

1-85. Power Supply Fault. During a power supply fault condition, the power supply fault status input will go LOW. The LOW is applied to OR gate U45A. With a LOW ac fail signal present, U45A will output a LOW to NAND gate U60A. With a HIGH power supply emergency signal present from U46D, U60A will output a HIGH to latch U48B. U48B will output a HIGH to: 1) bias driver transistor Q43 off to extinguish the power supply indicator green LED and 2) NOR gate U52D. U52D will output a LOW to bias driver transistor Q42 on. This will illuminate the power supply indicator red LED.

1-86. Power Supply Emergency Condition. During a power supply emergency condition, the power supply emergency fault status input will go HIGH. The HIGH is applied to AND gate U36B. With a HIGH enable failure signal present, U36B will output a HIGH to: 1) inverter U46D and 2) OR gate U37B. U46D will output a LOW to NAND gate U60A. U60A will output a HIGH to latch U48B. U48B will output a HIGH to: 1) bias driver transistor Q43 off to extinguish the power supply indicator green LED and 2) NOR gate U52D. U52D will output a LOW to bias driver transistor Q42 on to illuminate the power supply indicator red LED. With a HIGH from U36B applied to U37B, U37B will output a HIGH emergency off signal to OR gate U37A. This configures U37A and OR gate U13A to generate a transmitter off signal.

1-87. Power Supply Maintenance Condition. During a power supply maintenance condition, the power supply maintenance fault status input will go HIGH. The HIGH is applied to NOR gate U52D. U52D will output a LOW to bias transistor Q42 on. This will illuminate the power supply indicator red LED. With no power supply fault indications, the output of U48B will be LOW. The LOW bias driver transistor Q43 on to illuminate the power supply indicator green LED. The simultaneous illumination of the indicator green and red LEDs will produce a yellow maintenance indication.

1-88. RF POWER MODULE MONITORING. The RF power module operating condition is monitored by an RF power module status circuit. The following text presents the RF power module monitoring operations.

1-89. RF Power Module Fault. During an RF power module fault, the power supply fault status input will go LOW. The LOW is applied to inverter U46F. U46F will output a HIGH to latch U48C. U48C will output a HIGH to: 1) bias driver transistor Q41 off to extinguish the RF power module indicator green LED and 2) NOR gate U52B. U52B will output a LOW to bias driver transistor Q40 on. This will illuminate the RF power module indicator red LED.

1-90. RF Power Module Maintenance Condition. During an RF power module maintenance condition, the RF power module maintenance fault status input will go HIGH. The HIGH is applied to NOR gate U52B. U52B will output a LOW to bias transistor Q40 on. This will illuminate the RF power module indicator red LED. With no RF power module fault indications, the output of U48C will be LOW. The LOW will bias driver transistor Q41 on to illuminate the RF power module indicator green LED. This simultaneous illumination the indicator green and red LEDs will produce a yellow maintenance indication.

1-91. FAULT CIRCUIT. Exciter, power supply, RF power module, reflected power high, reflected power emergency, over-temperature, lightning, or a $1.2: 1$ VSWR conditions are monitored for faults by individual status circuits. In the event of a fault, the appropriate circuit will latch the fault for display by the controller circuit board indicators. If a circuit detects a fault condition, a HIGH signal will be applied to NOR gate U55. U55 will output a LOW to inverter U54F. U54F will output a HIGH to bias alarm driver transistors Q34 and Q35 on to illuminate the alarm indicator.

1-92. When a fault condition is removed, the fault circuit latch must be manually reset using the reset switch. When the reset switch is depressed, a HIGH reset command is applied to OR gate U12C. U12C will output a HIGH reset command to latches U48A, U48B, U48C, U48D, U49A, U49B, and U49C. The Q output of each latch will go LOW. The LOWs are applied to NOR gate U55. U55 will output a HIGH to inverter U54F. U54F will output a LOW to bias driver transistors Q34 and Q35 off to extinguish the alarm indicator.

1-93. OSCILLATOR CIRCUIT. Reference frequencies for controller circuit operation are provided by an oscillator circuit. The oscillator circuit consists of: 1) comparators U40C and U44B, 2) resistors R24, R28, R27, R29, R30 and R31, 3) capacitor C38, and 4) inverter U46A. The oscillator is designed to output a 1 kHz square wave signal. Oscillator symmetry control is provided by resistors R24 and R27. The oscillator frequency is controlled by resistor R29 and capacitor C38.

1-94. Integrated circuit U40C compares a 1 kHz signal to a reference voltage. As a result, U40C will output a ramp signal to comparator U44A. U44A uses the signal to generate the power control PWM signal. The ramp symmetry is controlled by R30 and R31.

1-95. OVER-CYCLE OFF CIRCUIT. The controller circuit board is equipped with an over-cycle circuit. The circuit is designed to prevent damage to the crowbar resistors on the power supply circuit board during 7 transmitter on/off cycles within 15 seconds. Conditions causing the transmitter to over-cycle off include ac failure and manual on/off control operation. The circuit consists of AND gate U22A, inverter U25F, pulse generator U59B, capacitor C132, and comparator U44D.

1-96. The circuit monitors the transmitter off, power supply mute, and ac fail conditions. AND gate U22B provides off signals during manual off operations. NOR gate U23A provides an off signal during power supply mute conditions. AC fail provides an off signal during ac fail conditions. During a transmitter off operation, a LOW from AND gate U22B, NOR gate U23A, or $\overline{\mathrm{AC} \text { fail }}$ is applied to AND gate U22A. U22A will output a LOW to inverter U25F. U25F will output a HIGH: 1) to pulse generator U59B and 2) power inhibit signal. U59B will output a HIGH to capacitor C132. If the transmitter is operated to off 7 times within 15 seconds, capacitor C132 will charge and provide a HIGH to comparator U44D. When the voltage increases above the reference, U44D will output a HIGH over-cycle off command to OR gate U37B. U37B will output a HIGH emergency off command to operate the transmitter to off if one of the following conditions occur: 1) open cabinet or external interlock, 2) power supply emergency, 3) over-cycle off, or 4) the ac line is above 260 Volts. The emergency off signal is routed to the remote panel by transistor Q56.

1-97. POWER SUPPLY CIRCUIT. The controller circuit board operates from $\pm 15$ volt dc supplies. The +15 volt supply is equipped with a battery backup system. A nine volt battery provides a dc supply to maintain the controller logic during an ac power failure. Switch S5 allows the battery to be tested. When switch S5 is depressed, the battery voltage is applied to comparator U44C. If the battery voltage is above the reference, the output of U44C will go LOW to illuminate battery ok indicator DS1.

1-98. The battery backup system is equipped with a battery save function. If no fault conditions have occurred during a power failure, NOR gate U55 will output a HIGH to AND gate U71C. With a HIGH shutdown signal, U71C will output a HIGH to latch U49D. U49D will output a HIGH to bias transistor Q52 off to terminate battery operation.

## 1-99. EXCITER CIRCUIT BOARD.

1-100. LEFT/RIGHT CHANNEL INPUT CIRCUIT. Left/right channel audio from the studio or audio processing equipment is applied to the exciter circuit board left and right channel input circuits (refer to Figure 1-2). The input circuits consist of: 1) RFI filters, 2) high-pass filter networks, 3) instrumentation amplifiers, 4) high frequency boost circuitry, and 5) active PWM filter equalizers. The left and right channel input circuits are identical. Therefore, only the left channel input circuit is discussed.

1-101. Left channel audio is applied to a balanced 600 Ohm resistive impedance network and an 80 kHz RFI filter network. The impedance and RFI filter networks are located on the motherboard assembly. The output of the circuitry on the motherboard is applied to a defeatable 10 Hz high-pass filter network consisting of capacitors C147 through C150 and jumpers P12A and P12B. The 10 Hz high-pass filter is provided to remove low frequency residual products from specific audio processing units. Jumpers P12A and P12B are provided to bypass the high-pass filter networks. The output from the high-pass filter network is applied to an instrumentation amplifier.

1-102. Integrated circuits U1A, U1B, and U2A are configured as an instrumentation amplifier circuit. The circuit is designed to provide balanced-to-unbalanced signal conversion. The output of the instrumentation amplifier is applied to a defeatable high frequency boost circuit. The high frequency boost circuit is designed to increase high frequency response to compensate for a Bessel filter in the pulse-width-modulation (PWM) modulator circuit. If the high frequency boost circuit is enabled, the circuit will result in a compromise between the frequency and transient response performance. If the high frequency boost circuit is enabled, the transmitter frequency response will increase approximately 2 dB at 10 kHz and the transient response will degrade. If the high frequency boost circuit is disabled, the transmitter frequency response will decrease 2 dB at 10 kHz and the transient response will improve. Programmable jumper P2 is provided to bypass the left channel high frequency boost circuit if required. The output of the high frequency boost circuit is routed to an active PWM filter/equalizer and a mono mode switching circuit.

1-103. Integrated circuits U3A and U3B are configured as an active PWM filter/equalizer. The PWM filter/equalizer is a fifth order low-pass filter. The filter is incorporated into the circuit to match the characteristics of a filter contained in the pulse-width-modulation (PWM) circuitry. The filter is required to provide: 1) accurate left and right channel metering and 2) superior stereo equalization. The output from the PWM filter/equalizer is routed for application to the stereo circuit board.

1-104. MONO MODE SWITCHING. Left and right channel audio from the input circuit is applied to monophonic mode selection integrated circuit U39. U39 is controlled by: 1) mono $L$, mono $R$, and mono SC signals from the stereo circuit board and 2) mono left or mono right channel select jumper P4. If the transmitter is equipped with the stereo circuit board and monophonic operation is required, LOW control signals from the following control lines are applied to configure U39 to select the desired monophonic audio: 1) mono SC control line and 2 ) mono L or mono R control lines. If the transmitter is not equipped with the stereo circuit board, jumper P4 is installed in the left or right channel position to configure U39 to select left or right channel audio for monophonic operation. The output of U39 is applied to single channel monophonic boost amplifier U8A. The monophonic boost circuit is designed to provide up to 6 dB of additional gain for monophonic operations. This level allows the transmitter to operate at 100\% modulation. Potentiometer R41 allows the adjustment of the monophonic boost level. A monophonic boost control in most audio processing equipment also provides additional gain for monophonic conditions. If the transmitter is configured for stereo operation, U39 sums the left and right channels to produce the stereo $\mathrm{L}+\mathrm{R}$ information. The $\mathrm{L}+\mathrm{R}$ information is applied through monophonic boost circuit U8A to the 24 uS delay circuit.

1-105. 24 uS DELAY CIRCUIT. Integrated circuits U8B, U9A, and U9B are configured as a 24 uS delay circuit. The delay circuit is incorporated into the $\mathrm{L}+\mathrm{R}$ audio path to ensure all required stereo equalization will be performed in the L-R audio path. This eliminates the requirement for complex adjustable delay circuitry in the $\mathrm{L}+\mathrm{R}$ path.

1-106. NEGATIVE LIMITER. The output from the delay circuit is applied to a negative limiter circuit. The circuit consists of integrated circuit U14A, diodes D1 and D2, and negative limit control R76. The circuit is designed to prevent the loss of carrier during negative modulation. Potentiometer R76 allows the circuit to be adjusted from $90 \%$ to $100 \%$. The output of the limiter is applied a incidental-phase-modulation (IPM) correction circuit and a PWM circuit. A sample from the negative limiter circuit is applied to comparator U43. When the negative limiter circuit is enabled, the output of U 43 will go high to illuminate negative limiter indicator DS5.

1-107. IPM CORRECTION CIRCUIT. L+R audio from negative limiter U14A is applied through buffer U15A to a low-pass filter. The filter is a fifth order low-pass filter consisting of integrated circuits U15B and U16A. The filter is designed to provide: 1) the correct time delay for IPM correction and 2) the correct frequency response for $\mathrm{L}+\mathrm{R}$ metering. The output from the filter: 1) is applied to inverting buffer U16B and 2) provides an IPM adjust signal to the IPM corrector circuit. Buffer U16B inverts the L+R signal and removes a dc sample introduced by the negative limiter. The output of U16B is applied to the $\mathrm{L}+\mathrm{R}$ metering circuitry.

1-108. A power control PWM signal from the controller circuit board is applied to low-pass filter U17B. U17B is designed to convert the power control PWM signal to a dc control voltage. The output of U17B is applied to inverting amplifier U17A. The output of U17A provides an IPM power reference signal to the IPM wave shape circuit.

1-109. PWM CIRCUIT. L+R audio from the negative limiter circuit is applied to amplifier U14B. U14B amplifies the L+R signal to a 4 volt peak-to-peak level with a -0.5 volt dc potential. This provides a $40 \%$ nominal duty cycle at the output of a PWM comparator to allow the circuitry to modulate the transmitter from $-100 \%$ to $+150 \%$. The output of U14B is applied to high-speed PWM comparator U22A. U22A compares the L+R signal with a reference signal from integrator U12 to generate a square-wave PWM control signal. The square wave duty cycle varies in response to the $\mathrm{L}+\mathrm{R}$ audio level. The output of U22A is applied to the PWM driver circuit and an exciter failure detector circuit.

1-110. PWM DRIVER CIRCUIT. The PWM control signal from PWM comparator U22A is applied a PWM driver circuit. The circuit consists of: 1) inverters U21A through U21F, 2) line drivers U19, U20, and U45, and 3) diodes D6 through D21 and D47 through D50. The PWM control signal is applied to inverters U21A through U21F. The inverted PWM signals from U21A through U21F are applied to inverting line drivers U19, U20, and U45. U19, U20, and U45 operate in parallel to lower the output impedance. The outputs from U19, U20, and U45 are applied to each RF amplifier module modulator circuit board. Diodes D6 through D21 and D47 through D50 protect U19/U20/U45 from latch-up conditions. The PWM circuit is protected from over-modulation conditions by an over-modulation PWM mute circuit consisting of transistor Q23, capacitor C173, and diode D65. If the modulation level increases above $150 \%$, the circuit will output a HIGH to mute line drivers U19, U20, and U45.
1-111. FREQUENCY SYNTHESIZER. The exciter circuit board frequency synthesizer is a phase-locked-loop circuit which generates and maintains the phase and frequency of a voltage-controlled-oscillator (VCO) to a high level of precision. The circuit is designed with the ability to synthesize: 1) 119 frequencies within the 522 kHz to 1705 kHz AM broadcast band in 10 kHz increments or 2) 123 frequencies within the 522 kHz to 1705 kHz AM broadcast band in 9 kHz increments.
1-112. The synthesizer operates from binary coded carrier frequency information entered into frequency programming switch S2. The binary formatted frequency is applied to frequency synthesizer integrated circuit U25. U25 operates from 10.24 MHz reference oscillator Y1. Capacitor C108 allows the reference to be calibrated. Regulator U24 provides a stable voltage supply for frequency synthesizer U25.
1-113. Once programmed, U25 will output a series of rectangular-wave pulses to loop filter U26B and low-pass filter U26A. U26A and U26B function together to generate a stable dc control voltage for application to a voltage-controlled-oscillator (VCO) module. The control voltage is used by the VCO module to generate a precision frequency reference. A constant current source for the VCO module is provided by transistor Q3.

1-114. Precision alignment of the VCO output is maintained by the phase-locked-loop design. Feedback samples are monitored by a lock detector circuit. If the VCO frequency shifts from the programmed operating state, the output of U25 will change to adjust the control voltage and maintain a stable VCO output.
1-115. The output of the VCO module is applied through transistor amplifier Q4 to inverter U30A. The output of U30A is applied to NAND gate U30B. A sample of U30A is applied to U25 for feedback.

1-116. The output of U30B is applied to a synchronous divider consisting of integrated circuits U29, U31A, U31B, U42A, and U42B. Depending on the carrier frequency: 1) the original synthesizer frequency or a divide-by-2 frequency is used to generate a 4XFc (four times carrier frequency) signal for application to the stereo circuit board and 2) a divide-by-4 or a divide-by- 8 signal is used to generate the carrier frequency. The carrier frequency is applied to NAND gate U30C. Jumpers P6A and P6B program the divider as determined by the carrier frequency.
1-117. PWM REFERENCE CIRCUIT. The PWM frequency is generated by oscillator Y2, binary counter U44, and switch S1. The PWM frequency generator outputs a 115.4 kHz to 138.5 kHz signal to an integrator circuit. The PWM frequency is: 1) generated by one of four different crystals and 2) determined by several operating parameters. The output of U44 is applied to Integrator U12. U12 is designed to generate a precision triangle-wave signal for application to PWM comparator U22A. Programming switch S1 is used to program the PWM frequency generator circuit. The PWM frequency, crystal, and switch programming are recorded in the final test data sheets.


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1-118. LOCK DETECTOR CIRCUIT. The frequency synthesizer circuit is monitored for proper operation by a lock detector circuit. Integrated circuits U28A, U28B, and U36A function as a lock detector circuit. The circuit monitors an output sample signal and a divided VCO sample signal from U25. If the VCO and the reference phases are within $\pm 180$ degrees, the VCO is locked to the correct frequency. If the phases are out of tolerance, the output of U36A will go LOW. The LOW is applied to comparator U27. The output of U27 will go HIGH to extinguish lock indicator DS4 and is inverted at U33A. U33A will output a LOW to U30B which mutes the output of the frequency synthesizer.

1-119. A sample from the lock detector circuit is applied to divide-by- 3600 circuit. The circuit consists of integrated circuits U34, U35A, U35B, U35C, and U36B. The divider circuit is designed to generate a 25 Hz pilot signal for application to the stereo circuit board.

1-120. STEREO DETECTION CIRCUIT. The presence of a stereo signal is detected by a stereo detection circuit. This circuit allows the transmitter to be: 1) converted to monophonic operation by removing the stereo circuit board or 2) converted to stereophonic operation by inserting the stereo circuit board. The circuit will also detect the presence of an external stereo signal.

1-121. Stereo signals from the stereo circuit board are applied to programmable jumper P7. P7 selects a stereo signal from the internal stereo circuit board or from an external source. The external source is applied to a processing circuit consisting of integrated circuit U32C and the associated circuitry. The processing circuit provides ac coupling, over-voltage limiting, and square-wave generation.

1-122. Either an external or internal stereo signal from P7 is applied to an RF detector circuit. The RF detector consists of: 1) resistors R151 through R155, 2) capacitors C124 and C125, and 3) diode D27. The detector rectifies the signal for application to an automatic mono/stereo select circuit consisting of integrated circuits U32A, U30B, U32C, and U32D.

1-123. The mono/stereo select circuit will route a stereo or mono signal to an RF drive circuit in response to the presence of stereo. If a stereo signal is present, the output of U32A will be LOW. The LOW will disable mono on gate U30C and enable stereo on gate U32B. The stereo signal from U32B will be applied through NAND gate U32D to a phase modulator circuit. If a stereo signal is not present, the output of U32A will be HIGH. The HIGH will enable U30C and disable U32B to allow the monophonic RF signal to be applied to the phase modulator circuit.

1-124. IPM WAVE SHAPE CIRCUIT. The IPM adjust and IPM power reference signals from the IPM correction circuit are applied to an IPM wave shape circuit. The signals are amplified at U41A. The output of U41A is applied to an IPM wave shape circuit consisting of integrated circuit U41B and diodes D30 and D31. The circuit is designed to output a phase modulated signal which is equal in amplitude and out-of-phase with the phase modulation component in the RF amplifier section. Potentiometer R198 controls the shape of the IPM correction signal. Potentiometer R189 controls the amplitude of the IPM correction signal. Diodes D32 through D37 provide over-voltage protection. The output of the IPM wave shape circuit is applied to the phase modulator circuit.

1-125. PHASE MODULATOR CIRCUIT. A phase modulator circuit is incorporated into the exciter circuitry to cancel incidental-phase-modulation (IPM) in the RF amplifier section of the transmitter. The circuit is designed to insert a phase modulation component which is equal in amplitude and out of phase with the phase modulation in the RF amplifier section. This feedforward approach is designed to effectively cancel (IPM) in the transmitter.

1-126. The phase modulator circuit accepts a mono or stereo signal from NAND gate U32D. The signal is applied to a frequency doubler circuit consisting of integrated circuits U38A, U38B, U38C, and U38D. The output of the frequency doubler is applied to the gates of transistors Q6 and Q7. An IPM correction signal from the IPM wave shape circuit is applied to the drains of Q6 and Q7.

1-127. Transistors Q6 and Q7 function to produce a triangle-shaped waveform which is equal in amplitude and out-of-phase with the IPM in the RF amplifier section. The output from Q6 and Q7 is converted to a square-wave at U33C and U33D. The signal from U33C/U33D is applied to a divider circuit consisting of integrated circuits U39A, U39B, and U33E. The output of the divider is used to clock the RF carrier signal from the frequency doubler circuit at latch U40. U40 outputs a phase compensated carrier frequency to the RF drive circuit. Potentiometer R170 is provided to adjust the symmetry of the RF carrier signal.

1-128. RF DRIVE CIRCUIT. The RF drive circuit consists of high/low side driver U46 and transistors Q13 through Q22. Complementary phase compensated square-wave signals at the carrier frequency are applied to U46. U46 outputs high and low driver signals for application to a transistor array consisting of transistors Q13 through Q20. The transistors output a +15 volt peak-to-peak square-wave signal at the carrier frequency for application to the power block motherboard.

1-129. EXCITER FAILURE DETECTOR CIRCUIT. The exciter circuitry is equipped with an exciter failure detector circuit. The circuit consists of integrated circuits U22B, U23A, and U23B. Two signals are routed to the detector circuit: 1) the PWM control signal and 2) an RF present signal from transistor Q8 and latch U40. The circuit is designed to output a HIGH during the following conditions: 1) the loss of the PWM signal or 2) the loss of the RF signal. The HIGH is routed to the circuitry on the controller circuit board.
1-130. POWER SUPPLY CIRCUITS. The exciter circuit board operates from three power supplies: 1) a +5 volt supply, 2 ) a +15 volt supply, and 3 ) a -15 volt supply. Each supply is equipped with a filter network. The +5 volt supply filter consists of inductor L1 and capacitors C31/C32. The output of the filter is applied to: 1$)+5$ volt indicator DS1 and 2) the exciter circuit board components. The +15 volt supply filter consists of inductor L2 and capacitors C34/C35. The output of the filter is applied to: 1$)+15$ volt indicator DS2 and 2 ) the exciter circuit board components. The -15 volt supply filter consists of inductor L3 and capacitors C36/C37. The output of the filter is applied to: 1$)-15$ volt indicator DS3 and 2) the exciter circuit board components.

1-131. STEREO CIRCUIT BOARD.
1-132. EQUALIZATION CIRCUITRY. The stereo circuit board is equipped with two equalization circuits: 1) equalization circuit 1 and 2) equalization circuit 2 (refer to Figure 1-3). The circuits are designed to provide equalization for two antenna patterns such as: 1) a day pattern and 2) a night pattern. The equalization circuits are identical and contain identical left and right channel circuitry. Therefore, only the left channel of equalization circuit 1 will be discussed.


BEB Beapacass

1-133. Left channel audio from the exciter circuit board is applied to a left channel high frequency equalizer network in the equalization 1 circuit. The high frequency equalizer consists integrated circuits U1A, U2, U1B, U3, U4A, and U6A. The equalizer circuit is a second order state variable low-pass filter designed to compensate for high frequency and phase problems caused by antenna/phasor units. The filter is equipped with an adjustable corner frequency. The corner frequency is established by a voltage generated by potentiometer R20 and buffer U6A. The voltage is applied to voltage-controlled-amplifiers U2 and U3 which control the corner frequency of the equalizer circuit. In addition to the variable corner frequency, the filter is equipped with a variable peak level. Potentiometer R6 controls the signal peak near the corner frequency. Potentiometer R1 controls the left channel level. The output of the circuit is applied to an 8 microsecond delay circuit.

1-134. 8 MICROSECOND DELAY CIRCUIT. Integrated circuit U4B is configured as an 8 microsecond delay circuit. The delay circuit is a third order low-pass filter designed to provide 8 microseconds of delay to match low and mid frequency delay equalization requirements. The output of the circuit is routed to 8 microsecond delay select jumper P1A. P1A allows the delay circuit to be bypassed if 8 microseconds of delay is not required for equalization operation.

1-135. 4 MICROSECOND DELAY CIRCUIT. Integrated circuit U5A is configured as a 4 microsecond delay circuit. The delay circuit is a third order low-pass filter designed to provide 4 microseconds of delay to match low and mid frequency delay equalization requirements. The output of the circuit is routed to 4 microsecond delay select jumper J1B. J1B allows the delay circuit to be bypassed if 4 microseconds of delay is not required for equalization operation.

1-136. ALL-PASS FILTER. Integrated circuit U5B is configured as an all-pass filter circuit. The circuit is designed to provide a continuously adjustable 0-6 microsecond delay for equalization operation. Potentiometer R26 controls the amount of delay.

1-137. EQUALIZATION SELECTION CIRCUIT. The outputs of equalization circuits 1 and 2 are applied to an equalization selection circuit consisting of integrated circuits U23 and U28. U23 and U28 are single-pole switch arrays designed to select audio from the equalization 1 or equalization 2 circuit. U23 and U28 are controlled by: 1) HIGH equalization 1 and equalization 2 control signals from latch U44A and 2) a HIGH stereo signal from the mono/stereo mode decoder circuit. The circuit is designed to select audio in response to the antenna pattern and mode of operation. For example, stereo audio from equalization circuit 1 is required. A HIGH from latch U44A will enable the equalization 1 switches in U23 and U28. U23 and U28 respond by routing audio to an $\mathrm{L}+\mathrm{R}$ and $\mathrm{L}-\mathrm{R}$ matrix circuit.

1-138. L+R AND L-R MATRIX CIRCUIT. Left and right channel audio from the equalization selection circuit is applied to an $\mathrm{L}-\mathrm{R}$ and $\mathrm{L}+\mathrm{R}$ matrix circuit. The circuit consists of integrated circuits U24A, U24B, U25A, U26A, U26B, U27A, U29A, U29B, U25B, U31B, U27B, U27A, and U32. The circuit is designed to generate $\mathrm{L}+\mathrm{R}$ and $\mathrm{L}-\mathrm{R}$ audio for application to a phase modulator circuit.

1-139. To provide an example of circuit operation, stereo audio is required from equalization circuit 1. Left channel audio from the equalization circuit 1 input of U23 is applied to buffer U24A. Right channel audio from the equalization circuit 1 input of U28 is applied to buffer U29A. U24A and U29A will output audio which is summed with a pilot signal from pilot on/off switch S1. The audio/pilot signal is applied to the inputs of U23/U28. With a HIGH from the stereo control line of mono/stereo mode decoder circuit: 1) U23 will route the left channel audio/pilot signal to amplifier U24B and 2) U28 will route the right channel audio/pilot signal to amplifier U29B. U24B/U29B amplify the signal to approximately 2.1 volts peak-to-peak. The outputs of U24B/U29B are applied to L+R summing amplifier U25A and L-R summing amplifier U25B.

1-140. A dc voltage for application to $\mathrm{L}+\mathrm{R}$ summing amplifier U25A is provided by regulator U32. U32 provides a bias voltage for the $\mathrm{L}+\mathrm{R}$ audio to generate a $1+\mathrm{L}+\mathrm{R}$ audio signal. The output of summing amplifier U25A is applied to a negative limiter circuit consisting of integrated circuit U26A and diodes D1 and D2. The circuit is designed to limit negative modulation to $-95 \%$. This prevents the loss of carrier during negative modulation. The output of negative limiter U26A is routed through buffer U26B to a phase modulator circuit as a $\overline{1+\mathrm{L}+\mathrm{R}}$ signal and inverter U27B. U27B generates a $1+\mathrm{L}+\mathrm{R}$ signal for application to a phase modulator circuit.

1-141. Left and right channel are summed at U25B to produce an L-R signal. The L-R signal is applied to: 1) a phase modulator circuit as an L-R signal, 2) to inverter U27B, and 3) buffer U31B. U27B generates a $\overline{\mathrm{L}-\mathrm{R}}$ signal for application to a phase modulator circuit. U31B is designed to buffer the L-R signal for application to an L-R metering circuit on the ECU display circuit board.

1-142. PHASE MODULATOR CIRCUIT. $1+\mathrm{L}+\mathrm{R}, \overline{1+\mathrm{L}+\mathrm{R}}, \mathrm{L}-\mathrm{R}$, and $\overline{\mathrm{L}-\mathrm{R}}$ signals are applied to a phase modulator circuit. The phase modulator circuit consists of: 1) phase modulator U36, 2) a synchronous divider consisting of integrated circuits U33, U34A, and U34B, and 3) latches U35A and U35B.

1-143. The phase modulator circuit operates from four phase references generated by a synchronous divider and latches U35A/U35B. A reference at four times the carrier frequency from the exciter circuit board is applied to a synchronous divider circuit. The circuit divides the signal by four and generates two outputs which are 90 degrees out-of-phase. The outputs are applied to latches U35A/U35B. U35A/U35B generate four reference signals: 1) 0 degrees, 2) 90 degrees, 3) 180 degrees, and 4) 270 degrees. The reference signals are used to drive phase modulator U36.

1-144. Integrated circuit U36 is a switch array configured as a phase modulator. The four reference signals from latches U35A/U35B are used to drive the $1+\mathrm{L}+\mathrm{R}, \overline{1+\mathrm{L}+\mathrm{R}}, \mathrm{L}-\mathrm{R}$, and $\overline{\mathrm{L}-\mathrm{R}}$ signals at U36. The output of U36 produces two signals: 1) a normal AM modulated signal reference to a 0 degree carrier containing the $\mathrm{L}+\mathrm{R}$ information (I modulator) and 2) a double side-band suppressed carrier signal referenced to a 90 degree carrier containing the $\mathrm{L}-\mathrm{R}$ information ( Q modulator). The signals are summed to produce a quadrature AM signal.

1-145. The quadrature AM signal is applied to integrated circuit U37. U37 is a high-speed operational amplifier designed to amplify the quadrature signal to a 1 volt peak-to-peak level with no modulation. The output of the amplifier is applied to a band-pass filter.

1-146. BAND-PASS FILTER. The output of amplifier U37 is applied to a forth order linear phase band-pass filter. The band-pass filter consists of: 1) inductors L4, L5, L6, and L7, 2) capacitors C110 and C115, and 3) programming switches S2, S3, and S4. The filter provides proper amplitude limiting during high single channel conditions. Programming switches S2, S3, and S4 select resistor and capacitor combinations to program the filter for specific groups of frequencies within the AM broadcast band. Inductors L4, L5, L6, and L7 tune the filter for proper operation. The output of the filter is applied to a transistor amplifier array.

1-147. TRANSISTOR AMPLIFIER CIRCUIT. The output of the band-pass filter is applied to a transistor array consisting of transistors Q1, Q2, U38B, U38C, U38D, and U38E. The signal is amplified to a 2 volt peak-to-peak level by transistors U38B, U38C, U38D, and U38E. The transistors also perform unbalanced-to-balanced signal conversion. The balanced signal from transistors U38B, U38C, U38D, and U38E are buffered by transistors Q1 and Q2 for application to the amplitude limiter circuit.
1-148. AMPLITUDE LIMITER CIRCUIT. The balanced quadrature signal from the transistor amplifier circuit is applied to an amplitude limiter circuit. The amplitude limiter circuit consists of integrated circuits U39A, U39B, and U39C. The circuit produces phase modulation containing the L-R information. The output of the limiter is applied to an output network.

1-149. OUTPUT NETWORK. The 1 volt peak-to-peak phase modulated signal from the amplitude limiter circuit is applied to transformer T1. T1 is provided to increase the voltage to a 5 volt peak-to-peak level. The output of T1 is buffered by inverters U40A and U40B. Potentiometer R193 adjusts the symmetry of the signal to null the second harmonic frequency. The output of U40B is routed for application to the exciter circuit board.

1-150. OPERATING MODE SELECTION AND INDICATION CIRCUIT. The stereo circuit board can be configured for stereo, mono left, mono right, or mono $L+R$ operation. The circuit board is configured for the desired mode of operation by a mode selection and indication circuit. HIGH remote mono left, mono right, mono $\mathrm{L}+\mathrm{R}$, and stereo commands are applied to optical couplers U45 through U48. The outputs of U45 through U48 are applied to OR gates U49A through U49D.

1-151. Local control operations are directed by mode select switch S5. S5 controls a mode counter circuit consisting of integrated circuits U53, U54A, U54B, U54C, and U54D. The switch operates by advancing the counter each time the switch is depressed. This results in the circuit advancing through the modes of operation in the following order: 1) stereo, 2) mono left, 3) mono right, or 4) mono L+R. The mode counter circuit selects a mode by routing a HIGH control command to the OR gates U49A through U49D.

1-152. OR gates U49A through U49D select a command from the remote control optical couplers or the local mode counter circuit. For example, the circuit board is desired to be configured for stereo operation. A HIGH from remote stereo optical coupler U48 or the local mode control circuit is applied to OR gate U49D. U49D outputs a HIGH through OR gate U52A to priority encoder U50. U50 monitors the OR gates for additional commands and determines the highest priority mode of operation. Once the mode of operation is determined, U50 will output a two bit binary code to a mono/stereo decoder circuit.

1-153. The mono/stereo mode decoder circuit consists of: 1) latches U44B, U51A, and U51B and 2) mono/stereo decoder logic U41D, U43B, U43C, U52C, and U52D. Latches U51A and U51B latch the two bit binary code and produce complementary outputs for application to the mono/stereo decoder logic. Latch U44B operates as a clock for U51A/U51B. The mono/stereo decoder logic decodes the binary code and outputs a HIGH to: 1) transistors Q5, Q9, and Q14 and 2) equalization select integrated circuits U23 and U28. Transistor Q14 will respond by generating a LOW internal stereo status signal. Transistor Q5 will output a LOW to bias stereo indicator DS3 to on. Transistor Q9 will respond by generating a LOW remote stereo status signal.

1-154. Selection and indication of the mono left, mono right, and mono $L+R$ modes of operation are performed in an identical manner. When the mono left or mono right mode is selected, a HIGH will be routed to NAND gate U43D. The output of U43D will go HIGH. The HIGH is inverted at U55D to produce a LOW mono single channel signal for application to the exciter circuit board. When the mono left, mono right, or mono $\mathrm{L}+\mathrm{R}$ mode is selected a HIGH is applied to transistor Q13. Q13 will respond by generating a LOW remote mono status signal.

1-155. EQUALIZATION SELECTION. Equalization circuit selection is determined by the antenna connected to the transmitter. Antenna A selects equalization circuit 1. Antenna B selects equalization circuit 2. Antenna $C$ can be programmed to select equalization circuit 1 or equalization circuit 2 .

1-156. Antenna A, B, and C status signals are applied to AND gates U41A and U41B. Programmable jumper P6 selects equalization circuit 1 or equalization circuit 2 for antenna C operations.

1-157. The circuit selects equalization circuit 1 or 2 when a status signal is applied to U41A/U41B. For example, a LOW is applied to U41B when antenna $A$ is selected. U41B will output a LOW to NAND gate U43A. Programmable jumper P7 programs the equalization selection circuit for momentary or continuous signals. With P7 programmed for momentary signals, U43A will output a HIGH to AND gate U41C. With a HIGH from U41A, U41C will output a HIGH to latch U44A. U44A will output a HIGH to: 1) integrated circuits U23 and U28 to select equalization circuit 1 and 2) transistor Q4. Q4 will go LOW to bias equalization 1 indicator DS1 on.

1-158. PILOT SIGNAL. A 25 Hz square-wave signal from the exciter circuit board is applied through potentiometer R132 to a band-pass filter consisting of integrated circuits U30A and U30B. Potentiometer R132 is designed to provide pilot level control. The band-pass filter converts the square-wave signal to a sine-wave signal.

1-159. The output of the band-pass filter is applied through switch S1 to: 1) integrated circuit U23 and 2) inverter U31A. U31A inverts the signal for application to integrated circuit U28. Switch S 1 is provided to disable the pilot signal.

1-160. POWER SUPPLY FILTER NETWORK. The stereo circuit board operates from $\pm 15$ volt power supplies. Each supply is equipped with a filter network. The +15 volt supply filter consists of inductor L1 and capacitor C92. The output of the filter is applied to the stereo circuit board components. The -15 volt supply filter consists of inductor L2 and capacitor C94. The output of the filter is applied to the stereo circuit board components.

1-161. ECU POWER SUPPLY ASSEMBLY.
1-162. The ECU assembly is equipped with a modular 40 W switching power supply assembly. The supply provides regulated $+5 \mathrm{~V},+15 \mathrm{~V}$, and -15 V operating potentials for the ECU circuit boards.

1-163. The power supply for the ECU controller circuit board is back-up by a 9 V battery. During an ac power failure, the battery will maintain the transmitter operating configuration stored in the controller logic circuitry. Once power is returned to the transmitter, the transmitter will automatically resume operation in the configuration appearing prior to the ac failure. If an extended ac power failure occurs, the transmitter will be operated to off by an ac loss/auto shutdown circuit on the controller circuit board.

# SECTION II TRANSMITTER ECU MAINTENANCE 

## 2-1. INTRODUCTION.

2-2. This section provides maintenance information for the AM-10A/AM-6A transmitter ECU (exciter/control unit).

2-3. SAFETY CONSIDERATIONS.
WARNING
WARNING
WARNING

WARNING

> THE TRANSMITTER CONTAINS MULTIPLE CIRCUIT GROUNDS WITH HIGH AC AND DC POTENTIALS WITH RESPECT TO THE CABINET WHICH IS AT EARTH POTENTIAL. DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CONNECTED TO THE TRANSMITTER OUTPUT NETWORK, RF POWER MODULE, RF COMBINER, OR POWER SUPPLY COMPONENTS.

2-4. The AM-10A/AM-6A transmitters contain high voltages and currents. If safety precautions are not practiced, contact with the high voltages and currents could cause serious injury or death. The transmitter is equipped with many built-in safety features, however good judgement, care, and common sense must be practiced to prevent accidents.
$2-5$. In addition to high voltages and currents, the transmitters contain multiple circuit grounds with high ac and dc potentials with respect to the cabinet which is at earth potential. The potentials could cause serious injury or death if maintenance personnel simultaneously touch a circuit ground and the cabinet. As a result, operation of the transmitter with test equipment connected to transmitter output network, RF power module, RF combiner, or power supply components is extremely dangerous and must not be attempted. Therefore, never energize the transmitter with test equipment connected to the transmitter output network, RF power module, RF combiner, or power supply components. Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized. The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel.

## 2-6. ECU CIRCUIT BOARD INSTALLATION/REMOVAL.

2-7. The transmitter ECU is equipped with three circuit boards: 1) exciter, 2) stereo, and 3) controller. Each circuit board is equipped with finger holes for the ease of removal and installation. To remove a circuit board, grasp the board using the finger holes and firmly pull the circuit board out of the ECU.

CAUTION
CAUTION

2-8. To install the circuit boards: 1) the boards must be inserted into the proper location in the ECU and 2) the boards must be firmly seated into the ECU motherboard. To install a circuit board, proceed as follows:

1. Refer to Figure 5-4 in PART I, SECTION V MAINTENANCE to determine the circuit board location.
2. Insert the circuit board in the appropriate location.
3. Firmly press the circuit board into the connector to engage the connector housing.
4. Firmly press the circuit board into the connector again to engage the connector pins.
5. Repeat the procedure for each ECU circuit board.

## 2-9. FIRST LEVEL MAINTENANCE.

$2-10$. First level maintenance consists of precautionary procedures applied to the equipment to prevent future failures. The procedures are performed on a regular basis and the results recorded in a performance log.

2-11. CLEANING AND INSPECTION.
WARNING NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED. EN-
WARNING SURE ALL TRANSMITTER PRIMARY POWER IS DISCONNECTED BEFORE ATTEMPTING MAINTENANCE ON ANY AREA WITHIN THE TRANSMITTER.

2-12. Clean the ECU circuit boards of accumulated dust as required using a nylon bristle brush and vacuum cleaner. Inspect the circuit boards for improperly seated semiconductors and components damage by overheating. In addition, inspect the ECU for loose hardware. Ensure all ECU interconnecting cables are secure.

## 2-13. SECOND LEVEL MAINTENANCE.

2-14. Second level maintenance is the performance of procedures required to restore the ECU to operation after a fault has occurred. The procedures are divided into electrical adjustments procedures and troubleshooting.

2-15. ELECTRICAL ADJUSTMENTS.
$2-16$. The following text provides electrical adjustment procedures for the transmitter ECU. The procedures are presented in the following order.

1. ECU Extender Circuit Board Operation.
2. Controller Circuit Board Adjustments.
3. ECU Meter Switch Circuit Board Adjustments.
4. Stereo Circuit Board Adjustments.
5. Exciter Circuit Board Adjustments.
6. Display Circuit Board Adjustments.

## 2-17. ECU EXTENDER CIRCUIT BOARD OPERATION.

$2-18$. The ECU is equipped with an extender circuit board. The circuit board is designed to allow access to the ECU circuit board components for maintenance procedures. To use the circuit board for maintenance procedures, proceed as follows:

1. Refer to Figure 5-4 in PART I, SECTION V MAINTENANCE and locate the extender circuit board assembly in the ECU.
2. Remove the extender circuit board from the ECU.
3. Loosen the extender circuit board locking nut.
4. Completely extend the circuit board.
5. Tighten the extender circuit board locking nut.
6. Remove the circuit board required for maintenance and place the extender circuit board in the location in the ECU.
7. Place the desired circuit board onto the extender circuit board.
8. Firmly press the circuit board into the extender circuit board connectors.

2-19. CONTROLLER CIRCUIT BOARD ADJUSTMENTS.
2-20. P1 SET - P5 SET CONTROLS. The P1 SET through P5 SET controls adjust the ECU POWER CONTROL 1 through 5 controls to desired levels. A complete description of the procedure to adjust the power level controls is presented in SECTION II, INSTALLATION. Refer to POWER LEVEL AND MODULATION CALIBRATION ADJUSTMENT in SECTION II for the adjustment procedure.

2-21. FWD AND RFL CALIBRATIONS. FWD CAL control R56 and RFL CAL control R143 calibrate the transmitter forward and reflected power samples. Due to the critical nature of the FWD CAL and RFL CAL controls, the controls are not considered field adjustable. If the controls are required to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the FWD and RFL CAL controls.

2-22. ECU METER SWITCH CIRCUIT BOARD ADJUSTMENTS.
2-23. FORWARD POWER METER LOW AND HIGH SCALE CALIBRATIONS. Low scale control R501 and high scale control R504 calibrate the forward power meter. Due to the critical nature of the low scale and high scale meter calibrate controls, the controls are not considered field adjustable. If the controls are required to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the low and high scale forward power meter controls.
2-24. REFLECTED POWER METER LOW AND HIGH SCALE CALIBRATIONS. Low scale control R505, high scale control R506, and ac sample control R511 calibrate the reflected power meter. Due to the critical nature of the low scale, high scale, and ac sample meter calibrate controls, the controls are not considered field adjustable. If the controls are required to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the low scale, high scale, and ac sample reflected power meter controls.

2-25. FWD AND RFL CALIBRATIONS. FWD CAL control R56 and RFL CAL control R143 calibrate the transmitter forward and reflected power samples. Due to the critical nature of the FWD CAL and RFL CAL controls, the controls are not considered field adjustable. If the controls are required to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the FWD and RFL CAL controls.
2-26. STEREO CIRCUIT BOARD ADJUSTMENTS.
2-27. STEREO ADJUSTMENT. The stereo adjustment consists of configuring the equalization circuitry on the stereo circuit board to obtain the optimum stereo performance. The equalization circuitry consists of the equalization circuit 1 and equalization circuit 2 controls. A complete description of the procedure to adjust the equalization controls is presented in SECTION II, INSTALLATION. Refer to STEREO ADJUSTMENT in SECTION II for the adjustment procedure.
$2-28$. EXCITER CIRCUIT BOARD ADJUSTMENTS.
2-29. MODULATION CALIBRATION. Modulation calibration control R62 calibrates the exciter modulation circuit. Due to the critical nature of the modulation calibration control, the control is not considered field adjustable. If the control is to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the modulation calibration control.
2-30. PHASE MODULATOR CALIBRATION. Phase modulator calibration control R159 calibrates the exciter phase modulator circuit. Due to the critical nature of the phase modulator calibration control, the control is not considered field adjustable. If the control is to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the phase modulator calibration control.
2-31. SYMMETRY CONTROL. Symmetry calibration control R170 adjusts the exciter RF output square-wave signal. Due to the critical nature of the symmetry control, the control is not considered field adjustable. If the control is to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the symmetry control.
2-32. IPM CORRECTION CIRCUIT CONTROLS. IPM GAIN control R189, IPM TRACK control R104, IPM SHAPE CONTROL R198, and IPM ZERO SET control R191 calibrate the IPM correction circuit. Due to the critical nature of the IPM correction circuit controls, the controls are not considered field adjustable. If the controls are to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the IPM correction circuit controls.
2-33. SINGLE CHAN MONO LEVEL CONTROL. SINGLE CHAN MONO LEVEL control R41 is designed to boost a remaining audio channel level in the event of a failure in one channel. A complete description of the procedure to adjust the SINGLE CHAN MONO LEVEL control is presented in SECTION II, INSTALLATION. Refer to SINGLE CHANNEL LEVEL in SECTION II for the adjustment procedure.
$2-34$. AVERAGE MODULATION LIMIT CONTROL. Average modulation limit control R217 limits the average tone modulation. The control is adjusted to limit at $110 \%$ tone modulation. Due to the critical nature of the modulation calibration control, the control is not considered field adjustable. If the control is to be adjusted, contact the Broadcast Electronics Customer Service Department for information and instructions to adjust the average modulation limit control.
2-35. NEG LIMIT CONTROL. NEG LIMIT control R76 limits the negative L+R information to prevent excessive modulation when the $\mathrm{L}+\mathrm{R}$ signal is summed with the pilot tone. The NEG LIMIT control is adjusted in the following procedure.
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2－36．Procedure．To adjust NEG LIMIT control R76，proceed as follows：

## DISCONNECT ALL TRANSMITTER PRIMARY POWER

 BEFORE PROCEEDING．$2-37$ ．Disconnect all transmitter primary power．
$2-38$ ．Connect the audio generator to the TB2 LEFT INPUT and RIGHT INPUT audio terminals on the ECU rear－panel．

2－39．Adjust NEG LIMIT control R76 on the exciter circuit board fully counterclockwise．
$2-40$ ．Adjust the audio generator for a $\mathrm{L}=\mathrm{R} 1 \mathrm{kHz}$ output at +10 dBm ．
2－41．Adjust the AM stereo modulation monitor to indicate positive $\mathrm{L}+\mathrm{R}$ modulation．
$2-42$ ．Energize the transmitter primary power and operate the transmitter．
$2-43$ ．Observe the modulation monitor and ensure the monitor indicates $100 \%$ positive $\mathrm{L}+\mathrm{R}$ modulation．If the monitor does not indicate $100 \% \mathrm{~L}+\mathrm{R}$ modulation，adjust the audio generator level slightly for $\mathrm{a}+100 \% \mathrm{~L}+\mathrm{R}$ modulation indication on the monitor．
2－44．Adjust the AM stereo modulation monitor to indicate negative $\mathrm{L}+\mathrm{R}$ modulation．
2－45．Adjust NEG LIMIT control R76 on the exciter circuit board until the AM stereo Modulation monitor indicates－95\％L＋R modulation．

## DISCONNECT ALL TRANSMITTER PRIMARY POWER

 BEFORE PROCEEDING．WARNING
$2-46$ ．Disconnect all transmitter primary power．
2－47．Remove all test equipment．
2－48．FREQUENCY CALIBRATION CONTROL．Frequency calibration control C108 calibrates the exciter frequency synthesizer．The frequency calibration control is adjusted in the following procedure．

2－49．Procedure．To adjust frequency calibration control C108，proceed as follows：

## WARNING <br> DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING． <br> WARNING

2－50．Disconnect all transmitter primary power．
2－51．Remove the exciter circuit board and install the ECU extender circuit board in the exciter circuit board location．
$2-52$ ．Install the exciter circuit board on the extender circuit board．
$2-53$ ．Connect a frequency counter to test point TP15 on the exciter circuit board．
$2-54$ ．Energize the transmitter primary power and operate the transmitter．
2－55．Adjust frequency calibration control C108 on the exciter circuit board for to the carrier frequency．

WARNING

## DISCONNECT ALL TRANSMITTER PRIMARY POWER

 BEFORE PROCEEDING．
## WARNING

Disconnect all transmitter primary power．
2－57．Remove all test equipment and replace the exciter circuit board．
2－58．DISPLAY CIRCUIT BOARD ADJUSTMENTS．
2－59．L／L＋R AND R／L－R DISPLAY CALIBRATION CONTROL．L／L＋R calibration control R42 and $R / L-R$ calibration control $R 48$ calibrate the $L / L+R$ and $R / L-R$ displays．The $L / L+R$ and $R / L-R$ calibration controls are adjusted in the following procedure．
2－60．Procedure．To adjust $L / L+R$ calibration control $R 42$ and $R / L-R$ calibration control R48， proceed as follows：

## DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING．

## WARNING

2－61．Disconnect all transmitter primary power．
2－62．Connect the audio generator to the TB2 LEFT INPUT and RIGHT INPUT audio terminals on the ECU rear－panel．Operate the transmitter at a normal output power and the EXCITER MONITOR for $\mathrm{L}+\mathrm{R} / \mathrm{L}-\mathrm{R}$ indications．
2－63．Adjust the audio generator for an in－phase $\mathrm{L}=\mathrm{R} 1 \mathrm{kHz}$ output at a level to generate $100 \%$ modulation as indicated by the modulation monitor．Adjust L／L＋R calibration control R42 until the EXCITER MONITOR just indicates $100 \%$ L＋R modulation．
2－64．Adjust the audio generator for an out－of－phase $\mathrm{L}=\mathrm{R} 1 \mathrm{kHz}$ output at a level to generate $100 \% \mathrm{~L}-\mathrm{R}$ modulation as indicated by the modulation monitor．Adjust R／L－R calibration control R48 until the EXCITER MONITOR just indicates $100 \%$ L－R modulation．
WARNING DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING．
WARNING
2－65．Disconnect all transmitter primary power and remove all test equipment． GROUNDS WITH HIGH AC AND DC POTENTIALS
WARNING WITH RESPECT TO THE CABINET WHICH IS AT WARNING EARTH POTENTIAL．DO NOT ENERGIZE THE TRANSMITTER WITH TEST EQUIPMENT CON－ NECTED TO THE TRANSMITTER OUTPUT NETWORK，RF POWER MODULE，RF COMBINER，OR POWER SUPPLY COMPONENTS．

2－67．SAFETY CONSIDERATIONS．The AM－10A／AM－6A transmitters are equipped with extensive indicator and meter circuitry to allow the operator to isolate problems to a specific area within the transmitter．Due to the hazardous voltages and currents contained in the equipment，operation of the transmitter with test equipment connected to transmitter output network，RF power module，RF combiner，or power supply components is extremely dangerous and must not be attempted．Test equipment may be connected to the ECU circuit boards from the front of the transmitter using the supplied extender circuit board with power energized．Therefore，the transmitter indicators and meters must be used to isolate a problem to a specific area．The maintenance procedures presented in this section should be performed only by trained and experienced maintenance personnel．

2-68. TROUBLESHOOTING PROCEDURES. The ECU assembly troubleshooting procedures are presented in Tables 2-1 through 2-4. Table 2-1 presents the exciter circuit board troubleshooting. Table 2-2 presents the stereo circuit board troubleshooting. Table 2-3 presents the controller circuit board troubleshooting. Table $2-4$ presents the ECU power supply troubleshooting. Refer to Tables $2-1$ through $2-4$ to isolate the problem to a specific circuit. Once the trouble is isolated, refer to the circuit board theory of operation and schematic diagrams to assist in problem resolution.

TABLE 2-1. EXCITER CIRCUIT BOARD TROUBLESHOOTING
(Sheet 1 of 3)


TABLE 2-1. EXCITER CIRCUIT BOARD TROUBLESHOOTING
(Sheet 2 of 3)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |

TABLE 2-1. EXCITER CIRCUIT BOARD TROUBLESHOOTING (Sheet 3 of 3)

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| LOW DEMODULATOR LEFT | 1. Defective U2A, U2B, U1A, U1B, U3A, U3B or |
| CHANNEL MODULATION LEVEL | P2 programming. |
| WITH LOW EXCITER |  |
| MONITOR LEFT CHANNEL |  |
| MODULATION LEVEL |  |
|  |  |
| LOW DEMODULATOR RIGHT | 1. Defective U5A, U5B, U4A, U4B, U6A, U6B or |
| CHANNEL MODULATION LEVEL | P3 programming. |
| WITH LOW EXCITER |  |
| MONITOR RIGHT CHANNEL |  |
| MODULATION LEVEL |  |
|  |  |

TABLE 2-2. STEREO CIRCUIT BOARD TROUBLESHOOTING
(Sheet 1 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| RED EXCITER INDICATOR ILLUMINATED ON TRANSMITTER MONITOR | 1. Insert a 1 kHz audio signal at +10 dBm into the left channel and operate the stereo circuit board to stereo. Check for a 3.0 V p-p quadrature AM signal at TP-7. <br> A. If the signal is present, defective U40A, U40B, T1, U39A, U39B, or U39C. <br> B. If the signal is not present, check for a quadrature AM signal at U38 pin 3. <br> 1. If the signal is present, defective U38A, U38B, U38C, U38D, U38E, Q1, or Q2. <br> 2. If the signal is not present, check for a quadrature AM signal at U37 pin 1. <br> a. If the signal is present, defective U37, L4, L5, L6, L7, D3, D4, or the S2, S3, or S4 programming. <br> b. If the signal is not present, defective U36, U35A, U35B, U34A, U34B, U33, U32, or U26. |
| NO L-R MODULATION PRESENT AT THE EXCITER MONITOR METER | 1. Defective U25B, U27B or U31B. | electronics inc

TABLE 2-2. STEREO CIRCUIT BOARD TROUBLESHOOTING
(Sheet 2 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| LOW DEMODULATOR LEFT CHANNEL MODULATION LEVEL WITH NORMAL EXCITER MONITOR LEFT CHANNEL MODULATION LEVEL | 1. Insert a +10 dBm 1 kHz signal into the left channel. Check for a 2 V p-p 1 kHz signal at U 4 pin 1. <br> A. If the signal is present, defective U4B, U5A, U5B, or J1. <br> B. If the signal is not present, defective U1A, U2, U1B, U3, or U4A. |
| LOW DEMODULATOR RIGHT CHANNEL MODULATION LEVEL WITH NORMAL EXCITER MONITOR RIGHT CHANNEL MODULATION LEVEL | 1. Insert a +10 dBm 1 kHz signal into the right channel. Check for a 2 V p-p 1 kHz signal at U10 pin 1. <br> A. If the signal is present, defective U10B, U11A, U11B, or J2. <br> B. If the signal is not present, defective U7A, U8, U7B, U9, or U10A. |

TABLE 2-3. CONTROLLER CIRCUIT BOARD TROUBLESHOOTING
(Sheet 1 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| NO POWER CONTROL PWM SIGNAL | 1. Check for a 1 kHz 15 V p-p square-wave signal at TP-7. <br> A. If the square-wave signal is present, defective Q22. <br> B. If the square-wave signal is not present, check for a $1 \mathrm{kHz} 50 \%$ duty-cycle square-wave signal at TP8. <br> 1. If the square-wave signal is not present, defective U44B, U40C, or U46E. <br> C. If the square-wave signal is not present, check for a dc voltage proportional to power at TP11. <br> 1. If the dc voltage is present, defective U44A, U40B, U41A, U42, or U43. <br> 2. If the dc voltage is not present, contact the Broadcast Electronics Customer Service Department. <br> 2. Check for a HIGH at U36C pin 8. <br> A. If the HIGH is present, defective U36C. <br> B. If the HIGH is not present, contact the Broadcast Electronics Customer Service Department. |

TABLE 2-3. CONTROLLER CIRCUIT BOARD TROUBLESHOOTING
(Sheet 2 of 2)

| SYMPTOM | CIRCUITRY TO CHECK |
| :---: | :---: |
| NO TRANSMITTER ON SIGNAL OUTPUT | 1. Check for a HIGH at U23A pin 3. <br> A. If the HIGH is present, defective Q13. <br> B. If the HIGH is not present, check for a LOW at U23A pin 2. <br> 1. If the LOW is present, defective U23A. <br> 2. If a HIGH is present, contact the Broadcast Electronics Customer Service Department. |
| CONFLICT INDICATOR ILLUMINATED | 1. Check U7, U8, U9, S1, S2, S3, U12A, U12B, U21A, U21B, U21C, U20A, U20B, U20C, U20D, U19, and U13. |

TABLE 2-4. ECU POWER SUPPLY TROUBLESHOOTING

| SYMPTOM | CIRCUITRY TO CHECK |
| :--- | :--- |
| NO OUTPUT POWER | 1. Check the ECU power supply fuse. |
| NO NORMAL/FAULT | 2. Check the ECU power supply assembly. |
| ECU INDICATIONS |  |

2-69. COMPONENT REPLACEMENT PROCEDURE. Component replacement procedures for the ECU assembly circuit boards are presented in PART I SECTION V. Refer to COMPONENT REPLACEMENT in SECTION V as required for the replacement procedures.

# SECTION III ECU ASSEMBLY PARTS LIST 

## 3-1. INTRODUCTION.

3-2. This section provides descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance of the ECU assembly. Each table entry in this section is indexed by reference designators appearing on the applicable schematic.

TABLE 3-1. REPLACEABLE PARTS LIST INDEX

| TABLE | DESCRIPTION | PART NO. | PAGE |
| :--- | :--- | :--- | :--- |
| $3-2$ | Exciter/Controller Assembly | $957-0009-011$ | $3-2$ |
| $3-3$ | ECU Exciter Circuit Board Assembly | $917-0300$ | $3-2$ |
| $3-4$ | VCO Module Circuit Board Assembly | $917-0069$ | $3-11$ |
| $3-5$ | ECU Motherboard Circuit Board Assembly | $917-0301$ | $3-11$ |
| $3-6$ | ECU Controller Circuit Board Assembly | $917-0205$ | $3-13$ |
| $3-7$ | ECU Display/Control Switch Circuit Board Assembly | $917-0306-001$ | $3-22$ |
| $3-8$ | Meter Switch Circuit Board Assembly | $917-0306-005$ | $3-25$ |
| $3-9$ | ECU Extender Circuit Board Assembly | $917-0208$ | $3-26$ |
| $3-10$ | Stereo Circuit Board Assembly | $917-0209$ | $3-26$ |
| $3-11$ | ECU Harness Assembly | $947-0153$ | $3-35$ |

TABLE 3-2. EXCITER/CONTROLLER ASSEMBLY - 957-0009-011

|  |  | DESCRIPTION | PART NO. |
| :--- | :--- | :--- | :--- | QTY.

## TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300 (Sheet 1 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C1, C2 | Capacitor, Electrolytic, $10 \mathrm{uF}, 35 \mathrm{~V}$ | 023-1075 | 2 |
| C3 thru C5 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C6 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C7 | Capacitor, Mica, $150 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1522 | 1 |
| C8 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C9 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C10 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C11 | Capacitor, Mica, $150 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1522 | 1 |
| C12 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C14 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C15 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C16, C17 | Capacitor, Electrolytic, 10 uF, 35V | 023-1075 | 2 |
| C18 thru C20 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C21 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C22 | Capacitor, Mica, $150 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1522 | 1 |
| C23 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C24 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C25 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C26 | Capacitor, Mica, $150 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1522 | 1 |
| C27 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C29 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C30, C31 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C32 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C33 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C34 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 2 of 10)
$\left.\begin{array}{llll}\hline & & & \\ \text { REF. DES. } & & \text { DESCRIPTION } & \text { PART NO. }\end{array}\right]$ QTY.

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300 (Sheet 3 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C104 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C105, C106 | Capacitor, Electrolytic, 22 uF, 100V | 024-2274 | 2 |
| C107 | Capacitor, Monolythic Ceramic, $56 \mathrm{pF} \pm 10 \%$, 200V | 001-5613 | 1 |
| C108 | Capacitor, Variable, Polycarbonate, 2-27 pF | 096-0009 | 1 |
| C109 | Capacitor, Mica, $150 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1522 | 1 |
| C110 | Capacitor, Ceramic Disc, 68 pF $\pm 5 \%$, N1500, 63 V dc | 000-6814 | 1 |
| C111 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C112, C113 | Capacitor, Monolythic Ceramic, $0.0015 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1523 | 2 |
| C114 | Capacitor, Mylar, $0.01 \mathrm{uF} \pm 10 \%$, 100V | 031-1043 | 1 |
| C115 thru C117 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 3 |
| C118 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C119, C120 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C121 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| $\begin{aligned} & \text { C122 thru } \\ & \text { C124 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C125 | Capacitor, Electrolytic, 1 uF, 50V, Non-Polarized | 020-1064 | 1 |
| $\begin{aligned} & \text { C126 thru } \\ & \text { C129 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 4 |
| C130 | Capacitor, Mica, $68 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-6813 | 1 |
| C131 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C132 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C133, C134 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3312 | 2 |
| C135, C136 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C137 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3312 | 1 |
| C138 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C140 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C141 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C143, C144 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C145 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%$, 500 V | 042-3312 | 1 |
| C146 | Capacitor, Electrolytic, 33 uF, 25V | 020-3374 | 1 |
| C147 thru C154 | Capacitor, Polycarbonate, $0.10 \mathrm{uF} \pm 1 \%, 100 \mathrm{~V}$ | 030-1051 | 8 |
| C155 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C156 | Capacitor, Monolythic Ceramic, $0.0047 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-4723 | 1 |
| C157 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C158, C159 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 2 |
| C160 | Capacitor, Mica, $22 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-2213 | 1 |
| C162 | Capacitor, Mica, $22 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-2213 | 1 |
| $\begin{aligned} & \text { C163 thru } \\ & \text { C165 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 3 |
| C166 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-4743 | 1 |
| C167 | Capacitor, Electrolytic, $1 \mathrm{uF}, 50 \mathrm{~V}$, Non-Polarized | 020-1064 | 1 |
| $\begin{aligned} & \text { C168 thru } \\ & \text { C170 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C171, C172 | Capacitor, Electrolytic, 1 uF, 50V, Non-Polarized | 020-1064 | 2 |
| C173 | Capacitor, Monolythic Ceramic, $0.0015 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1523 | 1 |
| C174 | Capacitor, Electrolytic, $2.2 \mathrm{uF} \pm 30 \%$, 50V, Non-Polarized | 020-2264 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300 (Sheet 4 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C175, C176 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| D1, D2 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D4 thru D21 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 18 |
| D22 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D23 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D24 thru <br> D27 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 4 |
| $\begin{aligned} & \text { D29 thru } \\ & \text { D46 } \end{aligned}$ | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 18 |
| D47 thru <br> D50 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 4 |
| $\begin{aligned} & \text { D51 thru } \\ & \text { D67 } \end{aligned}$ | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 17 |
| D68 | Diode, Zener, 1N4739A, 9.1V $\pm 5 \%$, 1W | 200-0009 | 1 |
| D69 | Diode, Zener, 1N4732A, 4.7V $\pm 5 \%$, 1W | 200-4732 | 1 |
| $\begin{aligned} & \text { DS1 thru } \\ & \text { DS5 } \end{aligned}$ | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 5 |
| E1 thru E4 | Terminal Test Point, Oval Red | 413-0106 | 4 |
| J2 thru J5 | Receptacle, Male, 3-Pin In-line | 417-0003 | 4 |
| J6 | Receptacle, Male, 20-Pin In-Line | 417-0200 | 1 |
| J7 | Receptacle, Male, 3-Pin In-line | 417-0003 | 1 |
| J8 thru J11 | Receptacle, Single Pin | 417-0071-001 | 4 |
| J12, J13 | Receptacle, Male, 20-Pin In-Line | 417-0200 | 2 |
| L1 thru L4 | Coil, Toroid, $22 \mathrm{uH} \pm 10 \%$, 34 Turns of No. 30 Enameled Copper Wire on B.E. No. 360-0023 Form | 360-0049 | 4 |
| L5 | Coil, Molded, Shielded, 56 uH | 360-0093 | 1 |
| L6 | Coil, Molded, 2.2 uH | 364-2200 | 1 |
| P2 thru P5 | Jumper, Programmable, 2-Pin | 340-0004 | 4 |
| P6A, P6B | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P7 | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P12A | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P12B | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P13A | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P13B | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P101 | Connector, Female, 80-Pin, Dual In-Line, PCB Mount | 417-0188 | 1 |
| Q3, Q4 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 2 |
| Q5 | Transistor, 2N3906, PNP, Silicon, TO-92 Case | 210-3906 | 1 |
| Q6, Q7 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 2 |
| Q8 | Field Effect Transistor, J3100, RF, N-Channel, TO-92 Case | 212-0310 | 1 |
| $\begin{aligned} & \text { Q13 thru } \\ & \text { Q22 } \end{aligned}$ | Field Effect Transistor, VN88AD, Metal-Oxide/Silicon, N-Channel Enhancement Type, TO-220-AB Case | 210-0088 | 10 |
| Q23 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 1 |
| R1 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R2 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2216 | 1 |
| R3 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 5 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R4 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2216 | 1 |
| R5 | Resistor Network, 10-10 k Ohm 0.5\% Resistors, 0.7W Total Dissipation, 16-Pin DIP | 226-0392 | 1 |
| R8, R9 | Resistor, $26.7 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2675 | 2 |
| R10 thru | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R12 |  |  |  |
| R14 | Resistor, $15 \mathrm{k} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-1551 | 1 |
| R15 | Resistor, 100 Ohm $\pm 1 \%$, 1/4W | 100-1031 | 1 |
| R16 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R17 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2216 | 1 |
| R18 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R19 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2216 | 1 |
| R20 | Resistor Network, $10-10 \mathrm{k}$ Ohm 0.5\% Resistors, 0.7 W Total Dissipation, 16-Pin DIP | 226-0392 | 1 |
| R23, R24 | Resistor, $26.7 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2675 | 2 |
| R25 thru | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R27 |  |  |  |
| R29 | Resistor, $15 \mathrm{k} \mathrm{Ohm} \pm 5 \%$, 1/4W | 100-1551 | 1 |
| R30 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R31 | Resistor, 221 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2213 | 1 |
| R32, R33 | Resistor, 1.24 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1244 | 2 |
| R34 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R35 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R36, R37 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 2 |
| R38, R39 | Resistor, $39.2 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-3951 | 2 |
| R40 | Resistor, $221 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2213 | 1 |
| R41 | Resistor, $3.83 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3841 | 1 |
| R41 | Potentiometer, $20 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 178-2054 | 1 |
| R42 | Resistor, $20.0 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2051 | 1 |
| R43 thru | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 12 |
| R54 |  |  |  |
| R55 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R58 thru | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 4 |
| R61 |  |  |  |
| R62 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 177-1054 | 1 |
| R63 | Resistor, $34 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3405 | 1 |
| R64 | Resistor, 2.2 Meg Ohm $\pm 5 \%$, 1/4W | 100-2273 | 1 |
| R65 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R66 | Resistor, 2.2 Meg Ohm $\pm 5 \%$, 1/4W | 100-2273 | 1 |
| R67 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R68 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R69 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R70 | Resistor, $121 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1231 | 1 |
| R71 | Resistor, 845 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8453 | 1 |
| R72 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R73 | Resistor, $47.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4755 | 1 |
| R74 | Resistor, $453 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-4561 | 1 |
| R75 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2241 | 1 |
| R76 | Potentiometer, $1 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, 1/2W | 178-1044 | 1 |
| R77 | Resistor, 34 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3405 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 6 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R78 | Resistor, $22.1 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2211 | 1 |
| R79 | Resistor, $1.33 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1331 | 1 |
| R80, R81 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R82, R83 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 2 |
| R84 | Resistor, $845 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8453 | 1 |
| R85 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| $\begin{aligned} & \text { R86 thru } \\ & \text { R88 } \end{aligned}$ | Resistor, $9.09 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9041 | 3 |
| R89, R90 | Resistor, $8.45 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8454 | 2 |
| R91 | Resistor, 5.6 Meg Ohm $\pm 5 \%$, 1/4W | 100-5673 | 1 |
| R92, R93 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R94 | Resistor, $100 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1031 | 1 |
| R99 | Resistor, 34 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3405 | 1 |
| R100 | Resistor, 66.5 k Ohm $\pm 1 \%$, 1/4W | 103-6655 | 1 |
| R101, R102 | Resistor, 26.7 k Ohm $\pm 1 \%$, 1/4W | 103-2675 | 2 |
| R112 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R113, R114 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 2 |
| R115 | Resistor, 34 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3405 | 1 |
| R116, R117 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R118 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R119 | Resistor, 121 Ohm $\pm 1 \%$, 1/4W | 100-1231 | 1 |
| R120 | Resistor, 365 Ohm $\pm 1 \%$, 1/4W | 103-3631 | 1 |
| R121 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| $\begin{aligned} & \text { R122 thru } \\ & \text { R125 } \end{aligned}$ | Resistor, 9.53 k Ohm $\pm 1 \%$, 1/4W | 103-9534 | 4 |
| $\begin{aligned} & \text { R126 thru } \\ & \text { R128 } \end{aligned}$ | Resistor, 7.50 k Ohm $\pm 1 \%$, 1/4W | 103-7541 | 3 |
| R129 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R130 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R131 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R132 | Resistor, $221 \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2213 | 1 |
| R133 | Resistor, 26.7 k Ohm $\pm 1 \%$, 1/4W | 103-2675 | 1 |
| R134 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R135 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R136 | Resistor, 2.2 Meg Ohm $\pm 5 \%$, 1/4W | 100-2273 | 1 |
| R137 | Resistor, $100 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1031 | 1 |
| $\begin{aligned} & \text { R138 thru } \\ & \text { R140 } \end{aligned}$ | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R142 | Resistor, 2.2 Meg Ohm $\pm 5 \%$, 1/4W | 100-2273 | 1 |
| R143 | Resistor, 221 Ohm $\pm 1 \%$, 1/4W | 103-2213 | 1 |
| R144 | Resistor, $3.83 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3841 | 1 |
| R145 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R146 | Resistor, 221 Ohm $\pm 1 \%$, 1/4W | 103-2213 | 1 |
| R147 | Resistor, 24.9 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2490 | 1 |
| R148 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R149, R150 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 2 |
| R151 | Resistor, $100 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1031 | 1 |
| R152 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R153 | Resistor, $3.83 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3841 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 7 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R154 | Resistor, $453 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-4561 | 1 |
| R155 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R156 | Resistor, 121 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1231 | 1 |
| R157 | Resistor, $845 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8453 | 1 |
| R158 | Resistor, $221 \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2213 | 1 |
| R159 | Potentiometer, $2 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, 1/2W | 177-2044 | 1 |
| R160 | Resistor, $1.24 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1244 | 1 |
| R161 | Resistor, $3.83 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3841 | 1 |
| R162 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R163 | Resistor, $100 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1031 | 1 |
| R164 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R165 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R166 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R167 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R168 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R169 | Resistor, $15 \mathrm{k} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-1551 | 1 |
| R170 | Potentiometer, $20 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $1 / 2 \mathrm{~W}$ | 178-2054 | 1 |
| R171 | Resistor, 15 k Ohm $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-1551 | 1 |
| R172 thru | Resistor, 22.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2212 | 8 |
| R179 R180 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R181 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R182 | Resistor, 68.1 k Ohm $\pm 1 \%$, 1/4W | 103-6815 | 1 |
| R183 | Resistor, $7.50 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-7541 | 1 |
| R184 | Resistor, 46.4 k Ohm $\pm 1 \%$, 1/4W | 103-4645 | 1 |
| R185 | Resistor, 113 k Ohm $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 103-1136 | 1 |
| R186 | Resistor, 4.75 k Ohm $\pm 1 \%$, 1/4W | 103-4741 | 1 |
| R187 | Resistor, 18.2 k Ohm $\pm 1 \%$, 1/4W | 103-1825 | 1 |
| R188 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R189 | Potentiometer, $1 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 178-1044 | 1 |
| R190 | Resistor, 2.10 k Ohm $\pm 1 \%$, 1/4W | 103-2104 | 1 |
| R191 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| $\begin{aligned} & \text { R192 thru } \\ & \text { R194 } \end{aligned}$ | Resistor, 113 k Ohm $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 103-1136 | 3 |
| R195 | Resistor, 100 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R196 | Resistor, $121 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1231 | 1 |
| R197 | Resistor, $2.94 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2941 | 1 |
| R198 | Potentiometer, $1 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 178-1044 | 1 |
| R199 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R200 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R201 | Resistor, $10 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%$, 1/4W | 100-1083 | 1 |
| R202 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| $\begin{aligned} & \text { R203 thru } \\ & \text { R209 } \end{aligned}$ | Resistor, 22.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2212 | 7 |
| R210, R211 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R212 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R213, R214 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R215 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R216 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 8 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R217 | Potentiometer, $2 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, 1/2W | 178-2044 | 1 |
| R218 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| S1 | Switch, SPST, 4-Position, 8-Pin DIP Dual In-line | 340-0002 | 1 |
| S2 | Switch, SPST, 8-Segment, 16-Pin DIP | 340-0003 | 1 |
| TP1 thru TP19 | Terminal Test Point, Oval Red | 413-0106 | 19 |
| U1, U2 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 2 |
| U3 | Amplifier, Dual Operational, RC4227GNB, Raytheon, 8-Pin DIP | 221-4227 | 1 |
| U4, U5 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 2 |
| U6 | Amplifier, Dual Operational, RC4227GNB Raytheon, 8-Pin DIP | 221-4227 | 1 |
| U7 | Integrated Circuit, DG212CJ, Quad, SPST Switch, 16-Pin DIP | 220-0212 | 1 |
| U8, U9 | Amplifier, Dual Operational, RC4227GNB Raytheon, 8-Pin DIP | 221-4227 | 2 |
| U10 | Integrated Circuit, MC14526BCP, Programmable Divide-by-N 4-Bit Counter, CMOS, 16-Pin DIP | 220-4526 | 1 |
| U11 | Integrated Circuit, MC14013BCP, Dual D-Type Flip-Flop, CMOS, 14-Pin DIP | 228-4013 | 1 |
| U12 | Integrated Circuit, NE5534AN, Low Noise Operational Amplifier, 8-Pin DIP | 221-5534 | 1 |
| U13 | Integrated Circuit, LM317LZ, Adjustable Positive Voltage Regulator, 1.2 to $37 \mathrm{~V} @ 0.1$ Ampere, TO-92 Case | 220-0317 | 1 |
| U14 thru U17 | Amplifier, Dual Operational, RC4227GNB, Raytheon, 8-Pin DIP | 221-4227 | 4 |
| U19, U20 | Integrated Circuit, 74C24ON, Inverting Tri State, 20-Pin DIP | 220-4240 | 2 |
| U21 | Integrated Circuit, CD4069CN, Hex Inverter, CMOS, 14-Pin DIP | 228-4069 | 1 |
| U22 | Integrated Circuit, LM319N, Dual Comparator, 14-Pin DIP | 221-0319 | 1 |
| U23 | Integrated Circuit, MC14538B, Dual Retriggerable, Resettable Monostable Multivibrator, CMOS, 16-Pin DIP | 228-4538 | 1 |
| U24 | Integrated Circuit, LM317LZ, Adjustable Positive Voltage Regulator, 1.2 to 37V @ 0.1 Ampere, TO-92 Case | 220-0317 | 1 |
| U26 | Amplifier, Dual Operational, RC4227GNB, Raytheon, 8-Pin DIP | 221-4227 | 1 |
| U27 | Integrated Circuit, TL311P, JFET-Input Differential Comparator, 8-Pin DIP | 220-0311 | 1 |
| U28 | Integrated Circuit, 74LS123, Schottky Dual Monostable Multivibrator, 16-Pin DIP | 220-2123 | 1 |
| U29 | Integrated Circuit, 74HC4022, Octal Counter/Divider, 16-Pin DIP | 221-4022 | 1 |
| U30 | Integrated Circuit, 74 HC 132 N , Quad Schmitt Nand Gates | 221-4132 | 1 |
| U31 | Integrated Circuit, 74HC4002N, Dual 4 Input NOR Gate 14-Pin DIP | 221-4002 | 1 |
| U32 | Integrated Circuit, 74 HC 132 N , Quad Schmitt Nand Gates | 221-4132 | 1 |
| U33 | Integrated Circuit, MC74HC14, Hex Schmitt Trigger Inverter, | 220-4106 | 1 |
| U34 | Integrated Circuit, MC14040B, CMOS MSI, 12-Bit Binary Counter, 16-Pin DIP | 220-4040 | 1 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 9 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| U35 | Integrated Circuit, MC14073B, Tripple 3-Input AND Gate, CMOS, 14-Pin DIP | 228-4073 | 1 |
| U36 | Integrated Circuit, MC14013BCP, Dual D-Type Flip-Flop, CMOS, 14-Pin DIP | 228-4013 | 1 |
| U37 | Integrated Circuit, LM317LZ, Adjustable Positive Voltage Regulator, 1.2 to 37V @ 0.1 Ampere, TO-92 Case | 220-0317 | 1 |
| U38, U39 | Integrated Circuit, 74HC132N QUAD Schmitt Nand Gates | 221-4132 | 2 |
| U40 | Integrated Circuit, 74HC75N, Quad D Latch | 221-7475 | 1 |
| U41 | Amplifier, Dual Operational, RC4227GNB, Raytheon, 8-Pin DIP | 221-4227 | 1 |
| U42 | Integrated Circuit, 74HC74N Dual D Flip Flop | 221-7474 | 1 |
| U43 | Integrated Circuit, TL311P, JFET-Input Differential Comparator, 8-Pin DIP | 220-0311 | 1 |
| U44 | Integrated Circuit, MC14060B, 14-Bit Binary Counter and Oscillator, CMOS MSI, 16-Pin DIP | 220-4060 | 1 |
| U45 | Integrated Circuit, 74C24ON, Inverting Tri State, 20-Pin DIP | 220-4240 | 1 |
| U46 | Driver, High and Low Side, IR2112, 14-Pin DIP | 227-2112 | 1 |
| U47 | Integrated Circuit, LM319N, Dual Comparator, 14-Pin DIP | 221-0319 | 1 |
| XU1 thru | Socket, 8-Pin DIP | 417-0804 | 6 |
| XU6 |  |  |  |
| XU4 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU7 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU8, XU9 | Socket, 8-Pin DIP | 417-0804 | 2 |
| XU10 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU11 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU12 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU14 thru | Socket, 8-Pin DIP | 417-0804 | 4 |
| XU17 |  |  |  |
| XU19, XU20 | Socket, 20-Pin DIP | 417-2004 | 2 |
| XU21, XU22 | Socket, 14-Pin DIP | 417-1404 | 2 |
| XU23 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU25 | Receptacle, 28-Pin DIP | 417-2804 | 1 |
| XU26, XU27 | Socket, 8-Pin DIP | 417-0804 | 2 |
| XU28 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU29 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU30 thru | Socket, 14-Pin DIP | 417-1404 | 4 |
| XU33 |  |  |  |
| XU34 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU35, XU36 | Socket, 14-Pin DIP | 417-1404 | 2 |
| XU38, XU39 | Socket, 14-Pin DIP | 417-1404 | 2 |
| XU40 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU41 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU42 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU43 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU44 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU45 | Socket, 20-Pin DIP | 417-2004 | 1 |
| XU46, XU47 | Socket, 14-Pin DIP | 417-1404 | 2 |

TABLE 3-3. ECU EXCITER CIRCUIT BOARD ASSEMBLY - 917-0300
(Sheet 10 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| 10 kHz SPACING |  |  |  |
| Y1 | Crystal, 48PD1002, 10.24 MHz, HC-18 Cinox 9 kHz SPACING | 390-0013 | 1 |
| Y1 | Crystal, 9.216 MHz, HC-18 Cinox | 390-0017 | 1 |
| ---- | Integrated Circuit, MC145151P, Parallel Input, PLL Frequency Synthesizer, CMOS, 28-Pin DIP | 220-5151 | 1 |
| ---- | Blank, ECU Exciter Circuit Board | 517-0300 | 1 |
| ---- | VCO Module Circuit Board Assembly | 917-0069 | 1 |

TABLE 3-4. VCO MODULE CIRCUIT BOARD ASSEMBLY - 917-0069

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C1, C2 | Capacitor, Monolythic Ceramic, $0.01 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1013 | 2 |
| C3 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 20 \%, 50 \mathrm{~V}$ | 003-1054 | 1 |
| C4 | Capacitor, Mica, $50 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-5013 | 1 |
| C5 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 20 \%$, 50 V | 003-1054 | 1 |
| D1 | Diode, Varactor, MVAM115, 500 pF at $1 \mathrm{VR}, 25 \mathrm{pF}$ at 15 VR , Motorola Case 182-03 | 200-0115 | 1 |
| D2, D3 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| P32 thru P35 | Plug, Male, Single Pin | 417-0119 | 4 |
| Q1, Q2 | Field Effect Transistor, J3100, RF, N-Channel, TO-92 Case | 212-0310 | 2 |
| R1 | Resistor, 619 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-6193 | 1 |
| R2 | Resistor, 100 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R3 | Resistor, 475 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4753 | 1 |
| R4 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R5 | Resistor, 100 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R6 | Resistor, 475 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4753 | 1 |
| -- | Ferrite Toroid, OD = 0.375 IN, ID $=0.188 \mathrm{IN}, \mathrm{W}=0.125 \mathrm{IN}$ | 360-0023 | 1 |
| ---- | Blank, VCO Module Circuit Board | 517-0069 | 1 |

TABLE 3-5. ECU MOTHERBOARD CIRCUIT BOARD ASSEMBLY - 917-0301
(Sheet 1 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1, C2 | Capacitor, Polyester, $0.0022 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $031-2033$ | 2 |
| C3, C4 | Capacitor, Polyester, $0.015 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $030-1532$ | 2 |
| C5, C6 | Capacitor, Polyester, $0.0022 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $031-2033$ | 2 |
| C7, C8 | Capacitor, Polyester, $0.015 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | $030-1532$ | 2 |
| C9 thru | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 51 |
| C59 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 5 |
| C61 thru |  |  |  |
| C65 |  | $3-11$ |  |
|  |  |  |  |

TABLE 3-5. ECU MOTHERBOARD CIRCUIT BOARD ASSEMBLY - 917-0301

## (Sheet 2 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C66 | Capacitor, Electrolytic, $100 \mathrm{uF}, 35 \mathrm{~V}$ | 020-1084 | 1 |
| C67 thru C84 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 18 |
| C85 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C86, C87 | Capacitor, Mica, $680 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 040-6824 | 2 |
| $\begin{aligned} & \text { C88 thru } \\ & \text { C90 } \end{aligned}$ | Capacitor, Polyester, $0.015 \mathrm{uF} \pm 10 \%, 100 \mathrm{~V}$ | 030-1532 | 3 |
| $\begin{aligned} & \text { C91 thru } \\ & \text { C109 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 19 |
| D1 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| J7 | Receptacle, 6-Pin | 417-0677 | 1 |
| J8 | Connector, AMP 1-87502-8, Header Straight Post Double Row, 40-Pin | 417-4040 | 1 |
| J9, J10 | Receptacle, Male, 13-Pin Dual In-Line | 417-2600 | 2 |
| J11 | Receptacle, BNC | 417-0203 | 1 |
| J12 | Connector, Male, 2-Pin In-Line | 417-4004 | 1 |
| J101 | Connector Header, 80-Pin, Dual In-Line | 417-0254 | 1 |
| J201 | Connector, AMP 102567-6, Header Straight Post Double Row, 50-Pin | 417-0255 | 1 |
| J301 | Connector, AMP 102567-6, Header Straight Post Double Row, 50-Pin | 417-0255 | 1 |
| J302 | Connector Header, 80-Pin, Dual In-Line | 417-0254 | 1 |
| L1 thru L4 | Coil, Shielded, $560 \mathrm{uH} \pm 10 \%$, Molded | 360-0072 | 4 |
| L5, L6 | RF Choke, $910 \mathrm{uH} \pm 5 \%, 79 \mathrm{~mA}$ Maximum, 15.8 Ohms DC Resistance | 360-0047 | 2 |
| P4 thru P6 | Connector, 25-Pin D-Type | 418-2500 | 3 |
| P12 | Switch, Jumper Programmable | 340-0004 | 1 |
| R1 | Resistor, 1.15 k Ohm $\pm 1 \%$, 1/4W | 103-1156 | 1 |
| R2, R3 | Resistor, $442 \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4423 | 2 |
| R4 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1156 | 1 |
| R5 | Resistor, 604 Ohm $\pm 1 \%$, 1/4W | 100-6031 | 1 |
| R6 | Resistor, 1.15 k Ohm $\pm 1 \%$, 1/4W | 103-1156 | 1 |
| R7, R8 | Resistor, $442 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4423 | 2 |
| R9 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1156 | 1 |
| R10 | Resistor, 604 Ohm $\pm 1 \%$, 1/4W | 100-6031 | 1 |
| R11 | Resistor, 47 Ohm $\pm 5 \%$, 1W | 120-4723 | 1 |
| R15 thru R18 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1156 | 4 |
| R19 thru R22 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 4 |
| R23 thru R28 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1156 | 6 |
| R29 thru R34 | Resistor, $51.1 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 6 |
| R35 thru R40 | Resistor, 1.15 k Ohm $\pm 1 \%$, 1/4W | 103-1156 | 6 |
| R41 thru R45 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 5 |
| R47 thru R51 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1156 | 5 |
| R53, R54 | Resistor, $442 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4423 | 2 |
| R55 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R56, R57 | Resistor, 1.15 k Ohm $\pm 1 \%$, 1/4W | 103-1156 | 2 |
| R56 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R58 | Resistor, 200 Ohm $\pm 1 \%$, 1/4W | 103-2003 | 1 |
| R59 | Resistor, $442 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4423 | 1 |

TABLE 3-5. ECU MOTHERBOARD CIRCUIT BOARD ASSEMBLY - 917-0301
(Sheet 3 of 3)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| R60 thru R62 | Resistor, $1.15 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ |  |  |
| R63, R64 | Resistor, $3.92 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1156$ | 3 |
| R65 | Resistor, 47 Ohm $\pm 5 \%, 1 \mathrm{~W}$ | $103-3924$ | 2 |
| R66 thru R72 | Resistor, $51.1 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | $120-4723$ | 1 |
| R73 | Resistor, 47 Ohm $\pm 5 \%, 1 \mathrm{~W}$ | $103-5112$ | 7 |
| R74 | Resistor, 10 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $120-4723$ | 1 |
| R75 | Resistor, 442 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1021$ | 1 |
| R76 | Resistor, 10 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-4423$ | 1 |
| R77 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1021$ | 1 |
| R78 thru R84 | Resistor, 1.15 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-5112$ | 1 |
| R84 | Resistor, 10 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1021$ | 7 |
| R86 thru R95 | Resistor, 10 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1021$ | 1 |
| TB1, TB2 | Barrier Strip, $30-$ Position | $412-3000$ | 10 |
| --- | Blank, ECU Motherboard Circuit Board | $517-0301$ | 2 |
|  |  |  | 1 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 1 of 10)

| REF. DES. |  |  | PART NO. |
| :--- | :--- | :--- | :--- | QTY.

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 2 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C88 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C89 | Capacitor, Electrolytic, $2.2 \mathrm{uF}, 25 \mathrm{~V}$ dc | 013-2064 | 1 |
| C90, C91 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C92 | Capacitor, Ceramic, 0.001 uF $\pm 10 \%$, 200V | 030-1033 | 1 |
| C93 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 20 \%$, 50 V | 003-4743 | 1 |
| C94 | Capacitor, Electrolytic, 2.2 uF, 25 V dc | 013-2064 | 1 |
| C95 | Capacitor, Electrolytic, 10 uF, 25V, Non-Polarized | 023-1075 | 1 |
| C96 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C97 | Capacitor, Electrolytic, 2.2 uF, 25 V dc | 013-2064 | 1 |
| C98, C99 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 20 \%$, 50 V | 003-4743 | 2 |
| C100 | Capacitor, Mylar Film, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C101 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 20 \%$, 50 V | 003-4743 | 1 |
| C102 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C103 | Capacitor, Ceramic, 0.001 uF $\pm 10 \%$, 200V | 030-1033 | 1 |
| C104, C105 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C106 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 1 |
| C107 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C108 | Capacitor, Electrolytic, 1 uF, 50V | 024-1064 | 1 |
| C109 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 20 \%$, 50 V | 003-4743 | 1 |
| C110 | Capacitor, Electrolytic, 10 uF, 25V, Non-Polarized | 023-1075 | 1 |
| $\begin{aligned} & \text { C111 thru } \\ & \text { C114 } \end{aligned}$ | Capacitor, Monolythic Ceramic, 0.1 uF $\pm 10 \%$, 50 V | 003-1066 | 4 |
| C115 | Capacitor, Monolythic Ceramic, . $47 \mathrm{uF} \pm 20 \%$, 50 V | 003-4743 | 1 |
| C116 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 1 |
| C117, C118 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C121 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 1 |
| $\begin{aligned} & \text { C122 thru } \\ & \text { C128 } \end{aligned}$ | Capacitor, Monolythic Ceramic, 0.1 uF $\pm 10 \%$, 50 V | 003-1066 | 7 |
| C129 | Capacitor, Mylar Film, $0.01 \mathrm{uF} \pm 10 \%$, 200V | 030-1043 | 1 |
| C130 | Capacitor, Electrolytic, 10 uF, 25V, Non-Polarized | 023-1075 | 1 |
| C131 | Capacitor, Electrolytic, 1 uF, 50V | 024-1064 | 1 |
| C132 | Capacitor, Electrolytic, $33 \mathrm{uF}, 35 \mathrm{~V}$ | 024-3374 | 1 |
| C133, C134 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C135 | Capacitor, Mica, $270 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 041-2722 | 1 |
| C136, C137 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 2 |
| D1 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D2 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D3 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D4 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D5 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D6 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D7 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D8 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D9 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D10 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D11 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D12 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D13 thru <br> D18 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 6 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 3 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| D19 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D20 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 1 |
| D21 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| $\begin{aligned} & \text { D22 thru } \\ & \text { D29 } \end{aligned}$ | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 8 |
| D30, D31 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 2 |
| D32 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D33 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 1 |
| D34, D35 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D36, D37 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 2 |
| D38 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D39, D40 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 2 |
| D41 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 1 |
| D42 | Diode, HP5082-2800, High Voltage, Schottky Barrier Type, $70 \mathrm{~V}, 15 \mathrm{~mA}$ | 201-2800 | 1 |
| D44, D45 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D47 thru D51 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 5 |
| $\begin{aligned} & \text { D53 thru } \\ & \text { D64 } \end{aligned}$ | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 12 |
| DS1, DS2 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 2 |
| DS3 | Indicator, LED, Yellow, 521-9176, 3V @ 40 mA Maximum | 323-9225 | 1 |
| E10 | Terminal, Turret, Double Shoulder | 413-1597 | 1 |
| J1 thru J3 | Receptacle, Male, 3-Pin In-line | 417-0003 | 3 |
| J4 thru J20 | Receptacle, Male, 2-Pin In-line | 417-4004 | 17 |
| P1 thru <br> P4 | Jumper, Programmable, 2-Pin | 340-0004 | 4 |
| P6 | Jumper, Programmable, 2-Pin | 340-0004 | 1 |
| P8 thru P19 | Jumper, Programmable, 2-Pin | 340-0004 | 12 |
| P301 | Receptacle, 50-Pin Dual In-line | 417-0147 | 1 |
| P302 | Connector, Female, 80-Pin, Dual In-Line PCB Mount | 417-0188 | 1 |
| Q1 thru Q37 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 37 |
| $\begin{aligned} & \text { Q38 thru } \\ & \text { Q45 } \end{aligned}$ | Transistor, VP0106N3, FET, P-Channel, TO-92 Case | 210-0106 | 8 |
| Q46 thru Q51 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 6 |
| Q52 | Transistor, VP0106N3, FET, P-Channel, TO-92 Case | 210-0106 | 1 |
| Q53, Q54 | Transistor, 2N3906, PNP, Silicon, TO-92 Case | 210-3906 | 2 |
| Q55 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |
| $\begin{aligned} & \text { Q57 thru } \\ & \text { Q59 } \end{aligned}$ | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 3 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 4 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R1 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R2 thru | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 5 |
| R6 |  |  |  |
| R7 | Resistor, $301 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3061 | 1 |
| R8 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R9 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R10 | Resistor, $4.42 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4441 | 1 |
| R11, R12 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 2 |
| R13 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R14 | Resistor, $43.2 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4325 | 1 |
| R15 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R16 | Resistor, 20.0 k Ohm $\pm 1 \%$, 1/4W | 103-2051 | 1 |
| R17 | Resistor, $2.32 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2341 | 1 |
| R18 | Resistor, $1.74 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1744 | 1 |
| R19, R20 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R21 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R22 | Resistor, $1.47 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1474 | 1 |
| R23 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R24 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R25 | Resistor, $301 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3061 | 1 |
| R26 thru | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 3 |
| R28 |  |  |  |
| R29 | Resistor, $20.0 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2051 | 1 |
| R30 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R31 | Resistor, $301 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3061 | 1 |
| R32 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R33 thru | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 3 |
| R35 |  |  |  |
| R36 | Resistor, 392 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3923 | 1 |
| R37 | Resistor, 240 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2431 | 1 |
| R38 | Resistor, 240 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2431 | 1 |
| R39 | Resistor, 1 k Ohm $\pm 1 \%$, 1/4W | 100-1041 | 1 |
| R40 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R41 | Resistor, 240 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2431 | 1 |
| R42 | Resistor, 392 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3923 | 1 |
| R43 | Resistor, $182 \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1823 | 1 |
| R44 | Resistor, 392 Ohm $\pm 1 \%$, 1/4W | 103-3923 | 1 |
| R45 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R46 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R47 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R48 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R49 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R50 | Resistor, 47.5 k Ohm $\pm 1 \%$, 1/4W | 103-4755 | 1 |
| R51 | Resistor, 121 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1261 | 1 |
| R52 | Resistor, $301 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3061 | 1 |
| R53, R54 | Resistor, $10 \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 2 |
| R55 | Resistor, $392 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3923 | 1 |
| R56 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 178-5001 | 1 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 5 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R57 | Resistor, $750 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-7503 | 1 |
| R58 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R59 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R60, R61 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 2 |
| R62 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R63, R64 | Resistor, 392 Ohm $\pm 1 \%$, 1/4W | 103-3923 | 2 |
| R65, R66 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R67 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R68 thru | Resistor, $47.5 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4755 | 3 |
| R70 |  |  |  |
| R71 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R72 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R73 | Resistor, 4.7 Meg Ohm $\pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-4773 | 1 |
| R74 | Resistor, $150 \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1531 | 1 |
| R75 | Resistor, $61.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-6195 | 1 |
| R76 | Resistor, $3.92 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3924 | 1 |
| R77 | Resistor, 1.47 k Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1474 | 1 |
| R78 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R79, R80 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| R81, R82 | Resistor, 20.0 k Ohm $\pm 1 \%$, 1/4W | 103-2051 | 2 |
| R83 | Resistor, 4.7 Meg Ohm $\pm 5 \%$, 1/4W | 100-4773 | 1 |
| R84 | Resistor, $47.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4755 | 1 |
| R85 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R86 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R87 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R88 | Resistor, 150 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1561 | 1 |
| R89 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R90 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R91 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-1051 | 1 |
| R92 | Resistor, $25.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2551 | 1 |
| R93 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R94 | Resistor, $10 \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R95 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R96 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R97 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R98 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R99 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R100 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R101 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 1 |
| R102 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R103 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R104 | Resistor, $16.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1695 | 1 |
| R105 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1007 | 1 |
| R106 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R107 | Resistor, 1.47 k Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1474 | 1 |
| R108 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R109 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R110 thru R122 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 13 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 6 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R123 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R124 | Resistor, $5.76 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-5764 | 1 |
| R125 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R126 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 1 |
| $\begin{aligned} & \text { R127 thru } \\ & \text { R130 } \end{aligned}$ | Resistor, 240 Ohm ñ1\%, 1/4W | 103-2431 | 4 |
| R131 thru R133 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 3 |
| R134 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R135 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R136 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R137 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R138 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R139, R140 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R141 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R142 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R143 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 178-5001 | 1 |
| R144 | Resistor, $750 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-7503 | 1 |
| R145 thru R147 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 3 |
| R148 thru <br> R150 | Resistor, $47.5 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4755 | 3 |
| R151 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R152 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R153 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R154, R155 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R156 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R157 | Resistor, $90.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-9095 | 1 |
| R158 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R159 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R160 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R161 | Resistor, $301 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3061 | 1 |
| R162 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R163 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R164, R165 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R166 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R167 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R168 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R169 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R170 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R171 | Resistor, 1 k Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2615 | 1 |
| R172, R173 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| R174 thru R176 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R177 | Resistor, $1 \mathrm{Meg} \mathrm{Ohm} \pm 1 \%$, $1 / 4 \mathrm{~W}$ | 103-1007 | 1 |
| R179, R181 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R183, R184 | Resistor, $392 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-3923 | 2 |
| R187, R188 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 7 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R189 | Resistor, $20.0 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2051 | 1 |
| R190 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R191 | Resistor, 4.7 Meg Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-4773 | 1 |
| R192 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R193, R194 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R195 | Resistor, $26.1 \mathrm{k} \mathrm{Oh} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2615 | 1 |
| R196 | Resistor, $121 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1261 | 1 |
| R197 | Resistor, $10 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1021 | 1 |
| R198 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R199 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R200 | Resistor, 2.2 Meg Ohm $\pm 5 \%$, 1/4W | 100-2273 | 1 |
| $\begin{aligned} & \text { R201 thru } \\ & \text { R205 } \end{aligned}$ | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 5 |
| R206 | Resistor, 475 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4731 | 1 |
| R207 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R208 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R209 | Resistor, $1.47 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1474 | 1 |
| R210 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| RN1, RN2 | Resistor Network, 10 k Ohm $\pm 2 \%$, 1W Resistors, 8-Pin Single In-Line Package | 226-1051 | 2 |
| RN3, RN4 | Resistor Network, 100 k Ohm, $\pm 2 \%$, 17 W Resistors, 10-Pin Single In-Line Package | 226-1060 | 2 |
| RN5 | Resistor Network, $10 \mathrm{k} \mathrm{Ohm} \pm 2 \%$, 1W Resistors, 8 -Pin Single In-Line Package | 226-1051 | 1 |
| RN6, RN7 | Resistor Network, 100 k Ohm, $\pm 2 \%, 2.7 \mathrm{~W}$ Resistors, 10-Pin Single In-Line Package | 226-1060 | 2 |
| RN8 | Resistor Network, 10 k Ohm $\pm 2 \%$, 1W Resistors, 8 -Pin Single In-Line Package | 226-1051 | 1 |
| S1 thru | Switch, SPST, 4-Position, 8-Pin DIP Dual In-Line | 340-0002 | 3 |
| S3 |  |  |  |
| S4 | Switch, Miniature Toggle, DPDT, 0.4 vA Maximum at 20 V ac or dc | 340-0060 | 1 |
| S5 | Switch, Push, N.O. Momentary Contact, Miniature, 1A @ 120V Maximum | 343-6330 | 1 |
| TP1 thru <br> TP6 | Test, Jack, Right Angle PC Mounting | 417-0004 | 6 |
| TP7 thru <br> TP12 | Terminal, Turret, Double Shoulder | 413-1597 | 6 |
| U1 thru | Integrated Circuit, 4N33, Optical Isolator, NPN Photo | 229-0033 | 11 |
| U11 | Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP |  |  |
| U12 | Integrated Circuit, CD4075BE, RCA | 225-0006 | 1 |
| U13 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U14 | Integrated Circuit, MC14532B, 8-Bit Priority Encoder, CMOS, 16-Pin DIP | 228-4532 | 1 |
| U15 | Integrated Circuit, MC14076, Quad D Register, CMOS, 16-Pin DIP | 228-4076 | 1 |
| U16 | Integrated Circuit, MC14011BCP, Quad 2-Input NAND Gate, CMOS, 14-Pin DIP | 228-4011 | 1 |
| U17 | Integrated Circuit, MC14076, Quad D Register, CMOS, 16-Pin DIP | 228-4076 | 1 |
| U18 | Integrated Circuit, MC14028BCP, BCD-to-Decimal Decoder, CMOS | 228-4028 | 1 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 8 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| U19 | Integrated Circuit, CD4075BE, RCA | 225-0006 | 1 |
| U20 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U21 | Integrated Circuit, CD4075BE, RCA | 225-0006 | 1 |
| U22 | Integrated Circuit, MC14073B, Tripple 3-Input AND Gate, CMOS, 14-Pin DIP | 228-4073 | 1 |
| U23 | Integrated Circuit, MC14001, CMOS, Quad 2-Input NOR Gate, 14-Pin DIP | 228-4001 | 1 |
| U24 | Integrated Circuit, Triple 3 Input NOR Gates, CMOS, 14-Pin DIP | 220-4025 | 1 |
| U25 | Integrated Circuit, CD4069CN, Hex Inverter, CMOS, 14-Pin DIP | 228-4069 | 1 |
| U26 | Integrated Circuit, 14 Stage Counter, CMOS, 16-Pin DIP | 228-4020 | 1 |
| U27 | Integrated Circuit, MC14512B, 8 Channel Data Selector, CMOS | 228-4512 | 1 |
| U28 | Integrated Circuit, MC14532B, 8-Bit Priority Encoder, CMOS, 16-Pin DIP | 228-4532 | 1 |
| U29 | Integrated Circuit, LM3362Z-2.5, Precision Voltage Reference, $2.5 \mathrm{~V} \pm 4 \%,-0$ to $+70^{\circ} \mathrm{C}$, TO-92 Case | 229-0336 | 1 |
| U30, U31 | Integrated Circuit, MC14516B, Binary Up/Down Counter, CMOS, 16-Pin DIP | 228-4516 | 2 |
| U32, U33 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 2 |
| U34, U35 | Integrated Circuit, MC14516B, Binary Up/Down Counter, CMOS, 16-Pin DIP | 228-4516 | 2 |
| U36 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U37 | Integrated Circuit, CD4075BE, RCA | 225-0006 | 1 |
| U38 | Integrated Circuit, MC14073B, Tripple 3-Input AND Gate, CMOS, 14-Pin DIP | 228-4073 | 1 |
| U39 | Integrated Circuit, MC14051, 8-Bit Analog Multiplexer, CMOS, 16-Pin DIP | 220-4051 | 1 |
| U40 | Integrated Circuit, TLO74CN, Quad JFET-Input Operational Amplifier, 14-Pin DIP | 221-0074 | 1 |
| U41 | Integrated Circuit, MC14053B, Analog Multiplexers/Demultiplexers, CMOS MSI, 16-Pin DIP | 220-4053 | 1 |
| U42, U43 | Integrated Circuit, DAC-08CP, D-A Converter, 8-Bit, 16-Pin DIP | 220-0801 | 2 |
| U44 | Integrated Circuit, LM339AN, Quad Comparator, 14-Pin DIP | 221-0339 | 1 |
| U45 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U46 | Integrated Circuit, CD4069CN, Hex Inverter, CMOS, 14-Pin DIP | 228-4069 | 1 |
| U47 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U48, U49 | Integrated Circuit, MC14043BP, CMOS, Quad NOR Gate, 16-Pin DIP | 220-4043 | 2 |
| U50 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U51 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U52 | Integrated Circuit, MC14001, CMOS, Quad 2-Input NOR Gate, 14-Pin DIP | 228-4001 | 1 |
| U53 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 1 |
| U54 | Integrated Circuit, CD4069CN, Hex Inverter, CMOS, 14-Pin DIP | 228-4069 | 1 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 9 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| U55 | Integrated Circuit, CD4078BE, RCA | 225-0007 | 1 |
| U56 | Integrated Circuit, 4N33, Optical Isolator, NPN Photo <br> Transistor/Infared Emitting Diode Type, 1500V Isolation, <br> Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP | 229-0033 | 1 |
| U57 | Integrated Circuit, MC14538B, Dual Retriggerable, Resettable Monostable Multivibrator, CMOS, 16-Pin DIP | 228-4538 | 1 |
| U58 | Integrated Circuit, 14 Stage Counter, CMOS, 16-Pin DIP | 228-4020 | 1 |
| U59 | Integrated Circuit, MC14538B, Dual Retriggerable, Resettable Monostable Multivibrator, CMOS, 16-Pin DIP | 228-4538 | 1 |
| U60 | Integrated Circuit, MC14011BCP, Quad 2-Input NAND Gate, CMOS, |  | 228- |
| 4011 | 1 14-Pin DIP |  |  |
| U61 | Integrated Circuit, LM339AN, Quad Comparator, 14-Pin DIP | 221-0339 | 1 |
| U62 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U63, U64 | Integrated Circuit, TLO74CN, Quad JFET-Input Operational Amplifier, 14-Pin DIP | 221-0074 | 2 |
| U65, U66 | Integrated Circuit, LM339AN, Quad Comparator, 14-Pin DIP | 221-0339 | 2 |
| U67 | Integrated Circuit, MC14043BP, CMOS, Quad NOR Gate, 16-Pin DIP | 220-4043 | 1 |
| U68 | Integrated Circuit, MC14538B, Dual Retriggerable, Resettable Monostable Multivibrator, CMOS, 16-Pin DIP | 228-4538 | 1 |
| U69 | Integrated Circuit, CD4075BE, RCA | 225-0006 | 1 |
| U70 | Integrated Circuit, LM317LZ, Adjustable Positive Voltage Regulator, 1.2 to $37 \mathrm{~V} @ 0.1$ Ampere, TO-92 Case | 220-0317 | 1 |
| U71 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| XS5 | Switch Cap, Red | 343-6331 | 1 |
| XU1 thru <br> XU11 | Socket, 6-Pin DIP | 417-0600 | 11 |
| XU12, XU13 | Socket, 14-Pin DIP | 417-1404 | 2 |
| XU14, XU15 | Socket, 16-Pin DIP | 417-1604 | 2 |
| XU16 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU17, XU18 | Socket, 16-Pin DIP | 417-1604 | 2 |
| XU19 | Socket, 14-Pin DIP | 417-1404 | 1 |
| XU20 thru XU25 | Socket, 14-Pin DIP | 417-1404 | 6 |
| $\begin{aligned} & \text { XU26 thru } \\ & \text { XU31 } \end{aligned}$ | Socket, 16-Pin DIP | 417-1604 | 5 |
| XU32, XU33 | Socket, 6-Pin DIP | 417-0600 | 2 |
| XU34, XU35 | Socket, 16-Pin DIP | 417-1604 | 2 |
| $\begin{aligned} & \text { XU36 thru } \\ & \text { XU38 } \end{aligned}$ | Socket, 14-Pin DIP | 417-1404 | 3 |
| XU39 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU40 | Socket, 14-Pin DIP | 417-1404 | 1 |
| $\begin{aligned} & \text { XU41 thru } \\ & \text { XU43 } \end{aligned}$ | Socket, 16-Pin DIP | 417-1604 | 3 |
| $\begin{aligned} & \text { XU44 thru } \\ & \text { XU47 } \end{aligned}$ | Socket, 14-Pin DIP | 417-1404 | 4 |
| XU48, XU49 | Socket, 16-Pin DIP | 417-1604 | 2 |
| $\begin{aligned} & \text { XU50 thru } \\ & \text { XU52 } \end{aligned}$ | Socket, 14-Pin DIP | 417-1404 | 3 |
| XU53 | Socket, 6-Pin DIP | 417-0600 | 1 |

TABLE 3-6. ECU CONTROLLER CIRCUIT BOARD ASSEMBLY - 917-0205
(Sheet 10 of 10)

| REF. DES. |  |  |  |
| :--- | :--- | :--- | :--- |
| XU54, XU55 | Socket, 14-Pin DIP | PART NO. | QTY. |
| XU56 | Socket, 6-Pin DIP | $417-1404$ |  |
| XU57 thru | Socket, 16-Pin DIP | $417-0600$ | 2 |
| XU59 |  | $417-1604$ | 1 |
| XU60 thru | Socket, 14-Pin DIP | $417-1404$ | 3 |
| XU66 |  |  | 7 |
| XU67, XU68 | Socket, 16-Pin DIP | $417-1604$ |  |
| XU69 | Socket, 14-Pin DIP | $417-1404$ | 2 |
| XU71 | Socket, 14-Pin DIP | $417-1404$ | 1 |
| XU71 | Socket, 16-Pin DIP | $417-1604$ | 1 |
| ---- | Blank, ECU Controller Circuit Board, AM-1 | $517-0205$ | 1 |
|  |  |  | 1 |

## TABLE 3-7. ECU DISPLAY/CONTROL SWITCH CIRCUIT BOARD ASSEMBLY -917-0306-001 (Sheet 1 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C1 thru C11 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 11 |
| C12 | Capacitor, Electrolytic, 1 uF, 50V | 024-1064 | 1 |
| C13 thru $\mathrm{C} 23$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 11 |
| C24, C25 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 2 |
| C26, C27 | Capacitor, Electrolytic, $33 \mathrm{uF}, 35 \mathrm{~V}$ | 024-3335 | 2 |
| C28 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 1 |
| C29 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C30 thru C32 | Capacitor, Electrolytic, 100 uF, 35V | 020-1084 | 3 |
| C33 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C34 | Capacitor, Electrolytic, $33 \mathrm{uF}, 35 \mathrm{~V}$ | 024-3335 | 1 |
| C35 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 1 |
| C36 | Capacitor, Electrolytic, 33 uF, 35V | 024-3335 | 1 |
| C37 | Capacitor, Electrolytic, 10 uF, 50V | 023-1076 | 1 |
| C38, C39 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C40 thru C43 | Capacitor, Ceramic, $0.001 \mathrm{uF} \pm 10 \%$, 200V | 030-1033 | 4 |
| D1 thru D9 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 9 |
| D10, D11 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D12 thru D14 | Diode, Zener, 1N4733A, 5.1V $\pm 5 \%$, 1W | 200-4733 | 3 |
| D15, D16 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 2 |
| D17 thru D19 | Diode, Zener, 1N4733A, 5.1V $\pm 5 \%$, 1W | 200-4733 | 3 |
| D20, D21 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| DS1, DS2 | Indicator, LED, Yellow, 521-9176, 3V @ 30 mA Maximum | 323-9225 | 2 |
| DS7 | LED, MV57164, Red, High Efficiency 10-Segment Bar Graph Array | 320-7164 | 1 |
| DS8, DS9 | LED, MV54164, Green, High Efficiency 10-Segment Bar Graph Array | 320-4164 | 2 |
| DS10 | LED, MV57164, Red, High Efficiency 10-Segment Bar Graph Array | 320-7164 | 1 |
| DS11, DS12 | LED, MV54164, Green, High Efficiency 10-Segment Bar Graph Array | 320-4164 | 2 |
| DS13, DS14 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 2 |
| DS15, DS16 | Indicator, LED, Red, 521-9212, 1.7V @ 50 mA Maximum | 323-9217 | 2 |

TABLE 3-7. ECU DISPLAY/CONTROL SWITCH CIRCUIT BOARD - 917-0306-001
(Sheet 2 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| DS17, DS18 | Indicator, LED, Yellow, 521-9176, 3V @ 30 mA Maximum | 323-9225 | 2 |
| DS19, DS20 | Indicator, LED, Green, 521-9175, 3V @ 40 mA Maximum | 323-9224 | 2 |
| $\begin{aligned} & \text { DS22 thru } \\ & \text { DS25 } \end{aligned}$ | LED, Tri-Color Common Cathode | 320-0031 | 4 |
| J1 | Receptacle, Male, 13-Pin Dual In-Line | 417-2600 | 1 |
| J2 | Connector, AMP 1-87502-8, Header Straight Post Double Row, 40-Pin | 417-4040 | 1 |
| Q1, Q2 | Field Effect Transistor, J271, P-Channel JFET, TO-92 Case | 210-0271 | 2 |
| Q3 thru Q6 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 4 |
| Q7 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 1 |
| R1 thru R3 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| R4 | Resistor, 11.0 k Ohm $\pm 1 \%$, 1/4W | 103-1105 | 1 |
| R5, R6 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| R7 | Resistor, $11.0 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1105 | 1 |
| R8 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R9 | Resistor, $24.3 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2435 | 1 |
| R10 | Resistor, 825 Ohm $\pm 1 \%$, 1/4W | 103-8253 | 1 |
| R11 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R12 | Resistor, $22 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-2283 | 1 |
| R13 | Resistor, $22.1 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2211 | 1 |
| R14 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2216 | 1 |
| R15 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R16 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R17 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2241 | 1 |
| R18 | Resistor, $24.3 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2435 | 1 |
| R19 | Resistor, 825 Ohm $\pm 1 \%$, 1/4W | 103-8253 | 1 |
| R20 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R21 | Resistor, $22 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-2283 | 1 |
| R22 | Resistor, $22.1 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2211 | 1 |
| R23 | Resistor, $221 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2216 | 1 |
| R24 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R25 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2241 | 1 |
| R26 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R27 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R28 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R29 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R30 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R31 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R32 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R33 thru R36 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 4 |
| R37 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R38 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R39 | Resistor, $10 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%, 1 / 4 \mathrm{~W}$ | 100-1083 | 1 |
| R40 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R41 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R42 | Potentiometer, $1 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 175-1034 | 1 |
| R43 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R44 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |

TABLE 3-7. ECU DISPLAY/CONTROL SWITCH CIRCUIT BOARD - 917-0306-001
(Sheet 3 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R45 | Resistor, $10 \mathrm{Meg} \mathrm{Ohm} \pm 5 \%$, 1/4W | 100-1083 | 1 |
| R46 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R47 | Resistor, $2.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2241 | 1 |
| R48 | Potentiometer, $1 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | 175-1034 | 1 |
| R49 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R50, R51 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R52, R53 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R54, R55 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R56 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R57 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R58 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R59 thru R61 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 3 |
| R62 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R63 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R64 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R65 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R66 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R67 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R68 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R69 thru R71 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 3 |
| R72 | Resistor, $82.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8255 | 1 |
| R73 | Resistor, 15 k Ohm $\pm 5 \%$, 1/4W | 100-1551 | 1 |
| R74 | Resistor, 121 Ohm $\pm 1 \%$, 1/4W | 100-1231 | 1 |
| R75 | Resistor, 604 Ohm $\pm 1 \%$, 1/4W | 100-6031 | 1 |
| R76, R77 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 2 |
| R78 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R79 | Resistor, $82.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8255 | 1 |
| R80 | Resistor, 15 k Ohm $\pm 5 \%$, 1/4W | 100-1551 | 1 |
| R81 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R82 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R83 thru R85 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 3 |
| R86 | Resistor, $499 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4993 | 1 |
| R87 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R88 thru R90 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 3 |
| R91 | Resistor, 499 Ohm $\pm 1 \%$, 1/4W | 103-4993 | 1 |
| R92 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, $1 / 4 \mathrm{~W}$ | 103-1214 | 1 |
| R93 thru R95 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 3 |
| R96 thru R102 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 7 |
| R103 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R104, R105 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 2 |
| $\begin{aligned} & \text { R106 thru } \\ & \text { R112 } \end{aligned}$ | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 7 |
| R113 | Resistor, 174 Ohm $\pm 1 \%$, 1/4W | 100-1731 | 1 |
| R114 | Resistor, 825 Ohm $\pm 1 \%$, 1/4W | 103-8253 | 1 |
| S1, S2 | Switch, SPDT, Momentary MP Series, 2 Green, C\&K MP01R2266 CBE | 340-0130 | 2 |
| S3 | Switch, SPDT, Momentary MP Series, 1 Red, C\&K MP01R123 CBE | 340-0030 | 1 |
| S4, S5 | Switch, SPDT, Momentary MP Series, 1 Yellow, C\&K MP01R125 CBE | 340-0162 | 2 |

TABLE 3-7. ECU DISPLAY/CONTROL SWITCH CIRCUIT BOARD - 917-0306-001
(Sheet 4 of 4)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| S6 thru S10 | Switch, SPDT, Momentary MP Series, 1 Green, C\&K MP01R126 CBE | 340-0161 | 5 |
| S11 | Switch, SPDT, Momentary MP Series, 1 Red, C\&K MP01R123 CBE | 340-0030 | 1 |
| R58 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R63 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R68 | Resistor, 1.21 k Ohm $\pm 1 \%$, 1/4W | 103-1214 | 1 |
| R82 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R87 | Resistor, $1.21 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1214 | 1 |
| R92 | Resistor, 1.21 k Ohm $\pm 1 \%$, 1/4W | 103-1214 | 1 |
| U1 | Integrated Circuit, DG212CJ, QUAD SPST Switch, CMOS, 16-Pin DIP | 220-0212 | 1 |
| U2 | Amplifier, Dual OP, RC4227GNB Raytheon, 8-Pin DIP | 221-4227 | 1 |
| U3 | Integrated Circuit, TLO74CN, Quad JFET-Input Operational Amplifier, 14-Pin DIP | 221-0074 | 1 |
| U4 | Integrated Circuit, MC14584, Hex Schmitt Trigger, CMOS, 14-Pin DIP | 228-4584 | 1 |
| U5 | Integrated Circuit, MC14013BCP, Dual D-Type Flip-Flop, CMOS, 14-Pin DIP | 228-4013 | 1 |
| U6 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 1 |
| U7 | Integrated Circuit, DG212CJ, QUAD SPST Switch, CMOS, 16-Pin DIP | 220-0212 | 1 |
| U8 | Integrated Circuit, TLO74CN, Quad JFET-Input Operational Amplifier, 14-Pin DIP | 221-0074 | 1 |
| U9 thru U11 | Integrated Circuit, LM3914N, Dot/Bar Display Driver, 18-Pin DIP | 229-3914 | 3 |
| U12,U13 | Integrated Circuit, NE555N, Timer, 8-Pin DIP | 229-0555 | 2 |
| U14 | Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 V to 37 V , 1.5 Ampere, TO-220 Case | 227-0317 | 1 |
| U15 thru U17 | Integrated Circuit, LM3914N, Dot/Bar Display Driver, 18-Pin DIP | 229-3914 | 3 |
| XU1 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU2 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU3 thru XU5 | Socket, 14-Pin DIP | 417-1404 | 3 |
| XU6 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU7 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU8 | Socket, 14-Pin DIP | 417-1404 | 1 |
| $\begin{aligned} & \text { XU9 thru } \\ & \text { XU11 } \end{aligned}$ | Socket, 18-Pin DIP | 417-1804 | 3 |
| XU12, XU13 | Socket, 8-Pin DIP | 417-0804 | 2 |
| XU15 thru <br> XU17 | Socket, 18-Pin DIP | 417-1804 | 3 |
| --- | Blank, ECU Display/Control Switch Circuit Board | 517-0306-001 | 1 |

## TABLE 3-8. METER SWITCH CIRCUIT BOARD ASSEMBLY - 917-0306-005 (Sheet 1 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :---: |
|  |  |  |  |
| C501 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |

TABLE 3-8. METER SWITCH CIRCUIT BOARD ASSEMBLY - 917-0306-005
(Sheet 2 of 2)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| D501 | Diode, Zener, 1N4733A, $5.1 \mathrm{~V} \pm 5 \%, 1 \mathrm{~W}$ | $200-4733$ | 1 |
| J501 | Receptacle, 6-Pin | $417-0677$ | 1 |
| J502 | Socket, 4-Pin | $418-0255$ | 1 |
| R501 | Potentiometer, 500 Ohm, $1 / 2 \mathrm{~W}$ | $178-5030$ | 1 |
| R503 | Potentiometer, $2 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | $178-2044$ | 1 |
| R504 | Resistor, 3.01 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-3014$ | 1 |
| R505 | Potentiometer, 500 Ohm, $1 / 2 \mathrm{~W}$ | $178-5030$ | 1 |
| R506 | Potentiometer, $2 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | $178-2044$ | 1 |
| R507 | Resistor, 3.01 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-3014$ | 1 |
| R508 | Resistor, 2.74 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-2744$ | 1 |
| R509, R510 | Resistor, 1.62 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | $103-1624$ | 2 |
| R511 | Potentiometer, $50 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 1 / 2 \mathrm{~W}$ | $178-5054$ | 1 |
| S501, S502 | Switch, Rotary, 3 Position 2 Pole | $340-0134$ | 2 |
| ---- | Blank, Meter Switch Circuit Board | $517-0306-005$ | 1 |

TABLE 3-9. ECU EXTENDER CIRCUIT BOARD ASSEMBLY - 917-0208

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| ---- | Connector, Female, 80-Pin, Dual In-Line, PCB Mount | $417-0188$ | 1 |
| ---- | Header, Right Angle, 50-Pin | $417-0152$ | 1 |
| --- | ECU Extender Card Support, AM XMTR | $471-0849$ | 1 |
| ---- | Header, Right Angle, 80-Pin | $417-8001$ | 1 |
| ---- | Receptacle, 50-Pin Dual In-line | $417-0147$ | 1 |
| --- | Blank, ECU Extender Circuit Board, AM-1 | $517-0208$ | 1 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| C1, C2 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 2 |
| C3, C4 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | $041-1031$ | 2 |
| C5 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C6 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | $042-5021$ | 1 |
| C7 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | $041-1031$ | 1 |
| C8 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | $040-1022$ | 1 |
| C9 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C10 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | $042-5021$ | 1 |
| C11 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | $041-1031$ | 1 |
| C12 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | $040-1022$ | 1 |
| C13 | Capacitor, Monolythic $\mathrm{Ceramic}, 0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | $003-1066$ | 1 |
| C14 | Capacitor, Mica, $330 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | $042-3322$ | 1 |

# TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209 

(Sheet 2 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C15 thru C18 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 4 |
| C19, C20 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 2 |
| C21 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C22 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C23 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C24 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%$, 500V | 040-1022 | 1 |
| C25 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C26 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C27 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C28 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C29 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C30 | Capacitor, Mica, $330 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3322 | 1 |
| C31 thru | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 4 |
| C34 |  |  |  |
| C35, C36 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 2 |
| C37 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C38 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C39 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C40 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%$, 500 V | 040-1022 | 1 |
| C41 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C42 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C43 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C44 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%$, 500V | 040-1022 | 1 |
| C45 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C46 | Capacitor, Mica, $330 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3322 | 1 |
| C47 thru | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 4 |
| C50 |  |  |  |
| C51, C52 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 2 |
| C53 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C54 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C55 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C56 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C57 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C58 | Capacitor, Mica, $500 \mathrm{pF} \pm 1 \%, 500 \mathrm{~V}$ | 042-5021 | 1 |
| C59 | Capacitor, Mica, $1000 \mathrm{pF} \pm 1 \%, 100 \mathrm{~V}$ | 041-1031 | 1 |
| C60 | Capacitor, Silvered Mica, $100 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-1022 | 1 |
| C61 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C62 | Capacitor, Mica, $330 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3322 | 1 |
| $\begin{aligned} & \text { C63 thru } \\ & \text { C80 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 18 |
| C81, C82 | Capacitor, Electrolytic, 100 uF, 50V | 020-1085 | 2 |
| C83, C84 | Capacitor, Mylar Film, $0.47 \mathrm{uF} \pm 2 \%, 100 \mathrm{~V}$ | 030-4753 | 2 |
| C85 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C86, C87 | Capacitor, Mylar Film, $0.47 \mathrm{uF} \pm 2 \%, 100 \mathrm{~V}$ | 030-4753 | 2 |
| $\begin{aligned} & \text { C88 thru } \\ & \text { C90 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 3 |
| C91 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 1 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 3 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| C92 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |
| C93 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| C94 | Capacitor, Electrolytic, 22 uF, 50V | 024-2274 | 1 |
| C95 thru | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 4 |
| C98 |  |  |  |
| C99 thru | Capacitor, Monolythic Ceramic, $0.0047 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-4723 | 4 |
| C102 |  |  |  |
| C103, C104 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 2 |
| C105 | Capacitor, Ceramic Disc, 3.3 pF, 1000V | 000-3302 | 1 |
| C106, C107 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 2 |
| C108 | Capacitor, Mica, $620 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 040-6223 | 1 |
| C109 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3312 | 1 |
| C110 | Capacitor, Mica, $180 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-1822 | 1 |
| C111 | Capacitor, Mica, $620 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 040-6223 | 1 |
| C112 | Capacitor, Mica, $220 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-2223 | 1 |
| C113 | Capacitor, Monolythic Ceramic, $0.0015 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1523 | 1 |
| C114 | Capacitor, Monolythic Ceramic, . $0027 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-2723 | 1 |
| C115 | Capacitor, Mica, $750 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-7522 | 1 |
| C116 | Capacitor, Mica, $560 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 040-5623 | 1 |
| C117 | Capacitor, Monolythic Ceramic, $0.0015 \mathrm{uF} \pm 5 \%, 100 \mathrm{~V}$ | 003-1523 | 1 |
| C118 | Capacitor, Mica, $820 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 042-8222 | 1 |
| C119 | Capacitor, Mica, $270 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 041-2722 | 1 |
| C120 | Capacitor, Mica, $180 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-1822 | 1 |
| C121 | Capacitor, Mica, $620 \mathrm{pF} \pm 5 \%, 300 \mathrm{~V}$ | 040-6223 | 1 |
| $\begin{aligned} & \text { C122 thru } \\ & \text { C128 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 7 |
| C129, C130 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 2 |
| $\begin{aligned} & \text { C131 thru } \\ & \text { C133 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 3 |
| C134 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3312 | 1 |
| C135, C136 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| C137 | Capacitor, Electrolytic, 10 uF, 25V, Non-Polarized | 023-1075 | 1 |
| $\begin{aligned} & \text { C138 thru } \\ & \text { C144 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 1 |
| C145 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 1 |
| C146, C147 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 2 |
| $\begin{aligned} & \text { C148 thru } \\ & \text { C151 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $470 \mathrm{pF} \pm 5 \%$, 200V | 003-4713 | 4 |
| $\begin{aligned} & \text { C152 thru } \\ & \text { C164 } \end{aligned}$ | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%, 50 \mathrm{~V}$ | 003-1066 | 13 |
| $\begin{aligned} & \text { C165 thru } \\ & \text { C168 } \end{aligned}$ | Capacitor, Mylar Film, $0.01 \mathrm{uF} \pm 10 \%$, 200V | 030-1043 | 4 |
| C169, C170 | Capacitor, Mica, $180 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-1822 | 2 |
| C171, C172 | Capacitor, Electrolytic, $10 \mathrm{uF}, 25 \mathrm{~V}$, Non-Polarized | 023-1075 | 2 |
| C173, C174 | Capacitor, Mica, $33 \mathrm{pF} \pm 5 \%, 500 \mathrm{~V}$ | 042-3312 | 2 |
| C175 | Capacitor, Monolythic Ceramic, $0.1 \mathrm{uF} \pm 10 \%$, 50 V | 003-1066 | 1 |
| D1, D2 | Diode, 1N4148, Silicon, 75V @ 0.3 Amperes | 203-4148 | 2 |
| D3, D4 | Diode, 1N4737, Zener, $7.5 \mathrm{~V} \pm 10 \%$, 1W | 200-4737 | 2 |
| D5 thru D9 | Diode, 1N4005, Silicon, 600V @ 1 Ampere | 203-4005 | 5 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 4 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { DS1 thru } \\ & \text { DS3 } \end{aligned}$ | Indicator, LED, Green, 521-9270, 3V @ 20 mA Maximum | 323-9224 | 6 |
| $\begin{aligned} & \text { DS4 thru } \\ & \text { DS6 } \end{aligned}$ | Indicator, LED, Yellow, 521-9271, 3V @ 20 mA Maximum | 323-9225 | 3 |
| E1 thru E4 | Terminal, Turret, Double Shoulder | 413-1597 | 4 |
| J1 thru J4 | Connector, Header, Right Angle, 8-Pin | 417-0807 | 4 |
| J5 thru J7 | Receptacle, Male, 3-Pin In-line | 417-0003 | 3 |
| L1 thru L3 | Coil, Toroid, $22 \mathrm{uH} \pm 10 \%$, 34 Turns of No. 30 Enameled Copper Wire on B.E. No. 360-0023 Form | 360-0049 | 3 |
| L4 | Shielded Adjustable Coil, 64-163 uH, 155 mA Maximum, 9.98 Ohms DC Resistance | 360-0077 | 1 |
| L5, L6 | Shielded Adjustable Coil, 26-71 uH, 185 mA Maximum, 6.97 Ohms DC Resistance | 360-0062 | 2 |
| L7 | Shielded Adjustable Coil, 12-29 uH, 225 mA Maximum, 4.72 Ohms DC Resistance | 360-0078 | 1 |
| P5 thru P7 | Jumper, Programmable, 2-Pin | 340-0004 | 3 |
| P1A, P1B | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P2A, P2B | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P3A, P3B | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P4A, P4B | Jumper, Programmable, 2-Pin | 340-0004 | 2 |
| P201 | Receptacle, 50-Pin Dual In-line | 417-0147 | 1 |
| Q1, Q2 | Transistor, 2N3904, NPN, Silicon, TO-92 Case | 211-3904 | 2 |
| Q3 thru Q14 | Transistor, 2N7000, FET, N-Channel, TO-92 Case | 210-7000 | 12 |
| R1 | Potentiometer, 5 k Ohm $\pm 10 \%$, 1W | 179-5043 | 1 |
| R2 | Resistor, $8.25 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8254 | 1 |
| R3 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R4 | Resistor, $6.04 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-6044 | 1 |
| R5 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R6 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R7 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R8 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R9 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1062 | 1 |
| R10 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 178-5001 | 1 |
| R11 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R12 | Resistor, 4.75 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4741 | 1 |
| R13 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R14 | Resistor, $51.1 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R15 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R16 | Resistor, 4.75 k Ohm $\pm 1 \%$, 1/4W | 103-4741 | 1 |
| R17 thru R19 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| $\begin{aligned} & \text { R20 thru } \\ & \text { R22 } \end{aligned}$ | Resistor, $4.99 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-5041 | 3 |
| R23, R24 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 5 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R25 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R26 | Potentiometer, 10 k Ohm $\pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R27 | Potentiometer, $5 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, 1W | 179-5043 | 1 |
| R28 | Resistor, $8.25 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8254 | 1 |
| R29 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R30 | Resistor, 6.04 K OHM, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-6044 | 1 |
| R31 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R32 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R33 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R34 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R35 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R36 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 178-5001 | 1 |
| R37 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R38 | Resistor, 4.75 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4741 | 1 |
| R39 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R40 | Resistor, $51.1 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R41 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R42 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R43 thru | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| R45 |  |  |  |
| $\begin{aligned} & \text { R46 thru } \\ & \text { R48 } \end{aligned}$ | Resistor, $4.99 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-5041 | 3 |
| R49, R50 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R51 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R52 | Potentiometer, 10 k Ohm $\pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R53 | Potentiometer, 5 k Ohm $\pm 10 \%$, 1W | 179-5043 | 1 |
| R54 | Resistor, $8.25 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8254 | 1 |
| R55 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R56 | Resistor, $6.04 \mathrm{~K} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-6044 | 1 |
| R57 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R58 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R59, R60 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 2 |
| R60 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R61 | Resistor, $100 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R62 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 178-5001 | 1 |
| R63 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R64 | Resistor, 4.75 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4741 | 1 |
| R65 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R67 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R68 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| $\begin{aligned} & \text { R69 thru } \\ & \text { R71 } \end{aligned}$ | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| $\begin{aligned} & \text { R72 thru } \\ & \text { R74 } \end{aligned}$ | Resistor, $4.99 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-5041 | 3 |
| R75, R76 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R77 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R78 | Potentiometer, 10 k Ohm $\pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R79 | Potentiometer, $5 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, 1W | 179-5043 | 1 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 6 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R80 | Resistor, $8.25 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8254 | 1 |
| R81 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R82 | Resistor, $6.04 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-6044 | 1 |
| R83 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R84 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R85 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R86 | Resistor, $51.1 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R87 | Resistor, 100 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1062 | 1 |
| R88 | Potentiometer, $500 \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 178-5001 | 1 |
| R89 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R90 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4741 | 1 |
| R91 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R92 | Resistor, 51.1 Ohm $\pm 1 \%$, 1/4W | 103-5112 | 1 |
| R93 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R94 | Resistor, 4.75 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4741 | 1 |
| $\begin{aligned} & \text { R95 thru } \\ & \text { R97 } \end{aligned}$ | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 3 |
| $\begin{aligned} & \text { R98 thru } \\ & \text { R100 } \end{aligned}$ | Resistor, $4.99 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-5041 | 3 |
| R101, R102 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R103 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R104 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%, 11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| $\begin{aligned} & \text { R105 thru } \\ & \text { R109 } \end{aligned}$ | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 5 |
| R110 | Resistor, 178 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1761 | 1 |
| R111 | Resistor Network, 10-10 k Ohm 0.5\% Resistors, 0.7W Total Dissipation, 16-Pin DIP | 226-0392 | 1 |
| R112 | Resistor, 1.15 k Ohm $\pm 1 \%$, 1/4W | 103-1156 | 1 |
| R113 | Resistor, $6.04 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-6044 | 1 |
| R114 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R115 | Resistor, 442 Ohm $\pm 1 \%$, 1/4W | 103-4423 | 1 |
| R116 | Resistor, 100 Ohm $\pm 1 \%$, 1/4W | 100-1031 | 1 |
| R117 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R118 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R119 | Resistor, 499 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4996 | 1 |
| $\begin{aligned} & \text { R120 thru } \\ & \text { R126 } \end{aligned}$ | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 7 |
| R127 | Resistor, $178 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1761 | 1 |
| R128 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2495 | 1 |
| R129, R130 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R131 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R132 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R133 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R134 | Resistor, $82.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8255 | 1 |
| R135 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R136 | Resistor, 205 k Ohm, $\pm 1 \%$, 1/4W | 103-2056 | 1 |
| R137 | Resistor, $71.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-7155 | 1 |
| R138 | Resistor, 909 Ohm $\pm 1 \%$, 1/4W | 103-9031 | 1 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 7 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R139 | Resistor, $178 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1761 | 1 |
| R140, R141 | Resistor, 10 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 2 |
| R142 | Resistor, $5.23 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5251 | 1 |
| R143 | Resistor, $5.49 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5494 | 1 |
| R144 | Resistor, $100 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1031 | 1 |
| R145 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R146, R147 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R148 thru <br> R151 | Resistor, 100 Ohm $\pm 1 \%$, 1/4W | 100-1031 | 4 |
| R152, R153 | Resistor, 22.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2212 | 2 |
| R154, R155 | Resistor, 2 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-2041 | 2 |
| R156 | Resistor, 88.7 Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-8872 | 1 |
| R157, R158 | Resistor, 182 Ohm $\pm 1 \%$, 1/4W | 103-1823 | 2 |
| R159 | Resistor, 442 Ohm $\pm 1 \%$, 1/4W | 103-4423 | 1 |
| R160 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R161 | Resistor, $182 \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-1823 | 1 |
| R162, R163 | Resistor, $221 \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2213 | 2 |
| R164 | Resistor, $182 \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1823 | 1 |
| R165, R166 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 2 |
| R167 | Resistor, 182 Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1823 | 1 |
| R168 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 1 |
| R169 | Resistor, $5.23 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5251 | 1 |
| $\begin{aligned} & \text { R170 thru } \\ & \text { R172 } \end{aligned}$ | Resistor, 442 Ohm, $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-4423 | 3 |
| R173 | Resistor, $240 \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2431 | 1 |
| R174 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R175 | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 1 |
| R176 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R177 | Resistor, 22.1 Ohm $\pm 1 \%$, 1/4W | 103-2212 | 1 |
| R178 | Resistor, 3.01 k Ohm $\pm 1 \%$, 1/4W | 103-3014 | 1 |
| R179 | Resistor, 22.1 Ohm $\pm 1 \%$, 1/4W | 103-2212 | 1 |
| R180 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R181, R182 | Resistor, $1.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-1504 | 2 |
| $\begin{aligned} & \text { R183 thru } \\ & \text { R188 } \end{aligned}$ | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 6 |
| R189 | Resistor, $4.75 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4741 | 1 |
| R190 | Resistor, $3.01 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-3014 | 1 |
| R191 | Resistor, $2 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-2041 | 1 |
| R192 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R193 | Potentiometer, $10 \mathrm{k} \mathrm{Ohm} \pm 10 \%$, $11 / 4 \mathrm{~W}$ | 179-1053 | 1 |
| R194 | Resistor, $24.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-2495 | 1 |
| R195 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 2 |
| R196 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| $\begin{aligned} & \text { R197 thru } \\ & \text { R200 } \end{aligned}$ | Resistor, 49.9 k Ohm $\pm 1 \%$, 1/4W | 103-4951 | 4 |
| R201, R202 | Resistor, 240 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2431 | 2 |
| R203 | Resistor, $82.5 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-8255 | 1 |
| R204 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 8 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| R205 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R206 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R207 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R208 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R209 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R210 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R211 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R212 | Resistor, 3.3 Meg Ohm $\pm 5 \%$, 1/4W | 100-3373 | 1 |
| R213 | Resistor, $49.9 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 103-4951 | 1 |
| R214 | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R215 | Resistor, $2 \mathrm{k} \mathrm{Ohm} \pm 1 \%$, 1/4W | 100-2041 | 1 |
| R216 | Resistor, $1 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 1 |
| R217 | Resistor, $10 \mathrm{k} \mathrm{Ohm} \pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1051 | 1 |
| R218 thru | Resistor, 240 Ohm $\pm 1 \%$, 1/4W | 103-2431 | 4 |
| R221 |  |  |  |
| $\begin{aligned} & \text { R222 thru } \\ & \text { R225 } \end{aligned}$ | Resistor, 1 k Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 100-1041 | 4 |
| R226 | Resistor, $5.23 \mathrm{k} \mathrm{Ohm}, \pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5251 | 1 |
| R227 | Resistor, 51.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-5112 | 1 |
| R228 | Resistor, 22.1 Ohm $\pm 1 \%, 1 / 4 \mathrm{~W}$ | 103-2212 | 1 |
| S1 | Switch, Toggle, SPDT, 5A @ 125V ac \& 28 V dc | 348-0123 | 1 |
| S2 thru S4 | Switch, SPST, 4-Position, 8-Pin DIP Dual In-Line | 340-0002 | 3 |
| S5 | Switch, Push, N.O. Momentary Contact, Miniature, 1A @ 120V Maximum | 343-6330 | 1 |
| T1 | Transformer, RF DRIVE | 370-0046 | 1 |
| TP1 thru TP10 | Terminal, Turret, Double Shoulder | 413-1597 | 10 |
| U1 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 1 |
| U2, U3 | Integrated Circuit, 2150A, Voltage Controlled Amplifier, 8-Pin DIP | 220-2150 | 2 |
| U4 thru U7 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 4 |
| U8, U9 | Integrated Circuit, 2150A, Voltage Controlled Amplifier, 8-Pin DIP | 220-2150 | 2 |
| U10 thru U12 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 3 |
| U13, U14 | Integrated Circuit, 2150A, Voltage Controlled Amplifier, 8-Pin DIP | 220-2150 | 2 |
| U15 thru U18 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 4 |
| U19, U20 | Integrated Circuit, 2150A, Voltage Controlled Amplifier, 8-Pin DIP | 220-2150 | 2 |
| U21, U22 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 2 |
| U23 | Integrated Circuit, DG212CJ, QUAD SPST Switch, CMOS, 16-Pin DIP | 220-0212 | 1 |
| U24 thru U27 | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 4 |
| U28 | Integrated Circuit, DG212CJ, QUAD SPST Switch, CMOS, 16-Pin DIP | 220-0212 | 1 |
| $\begin{aligned} & \text { U29 thru } \\ & \text { U31 } \end{aligned}$ | Integrated Circuit, TL072CP, Dual JFET-Input Operational Amplifier, 8-Pin DIP | 221-0072 | 3 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 9 of 10)

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :---: | :---: | :---: | :---: |
| U32 | Integrated Circuit, LM317LZ, Adjustable Positive Voltage Regulator, 1.2 to 37 V @ 0.1 Ampere, TO-92 Case | 220-0317 | 1 |
| U33 | Integrated Circuit, 74HC4022, Octal Counter/Divider, CMOS, 16-Pin DIP | 221-4022 | 1 |
| U34 | Integrated Circuit, 74 HC 4002 N , Dual 4 Input NOR Gate 14-Pin DIP | 221-4002 | 1 |
| U35 | Integrated Circuit, 74HC74N, Dual D-Type Flip Flop, 14-Pin DIP | 221-7474 | 1 |
| U36 | Integrated Circuit, DG-271, 201HS, CMOS SPST Analog Switch 16-Pin DIP | 220-0017 | 1 |
| U37 | Integrated Circuit, NE5539N, UHF Operational Amplifier, 14-Pin DIP | 220-5539 | 1 |
| U38 | Integrated Circuit, CA3183E, Five Transistor Array, NPN, 16-Pin DIP | 220-3183 | 1 |
| U39 | Integrated Circuit, MC10116P, Triple Differential Amplifier, 16-Pin DIP | 220-0116 | 1 |
| $\begin{aligned} & \text { U40 } \\ & 4132 \end{aligned}$ | Integrated Circuit, 74 HC 132 N, Quad NAND Gate, Schmitt Trigger, 1 |  | 221- |
|  | 14-Pin DIP |  |  |
| U41 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U42 | Integrated Circuit, MC14584, Hex Schmitt Trigger, CMOS, 14-Pin DIP | 228-4584 | 1 |
| U43 | Integrated Circuit, MC14093B, Quad 2-Input NAND Schmitt Trigger CMOS, 14-Pin DIP | 220-4093 | 1 |
| U44 | Integrated Circuit, MC14013BCP, Dual D-Type Flip-Flop, CMOS, 14-Pin DIP | 228-4013 | 1 |
| U45 thru | Integrated Circuit, 4N33, Optical Isolator, NPN Photo | 229-0033 | 4 |
| U48 | Transistor/Infared Emitting Diode Type, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP |  |  |
| U49 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U50 | Integrated Circuit, MC14532B, CMOS, 8-Bit Priority Encoder | 228-4532 | 1 |
| U51 | Integrated Circuit, MC14013BCP, Dual D-Type Flip-Flop, CMOS, 14-Pin DIP | 228-4013 | 1 |
| U52 | Integrated Circuit, CD4071B, OR Gate, CMOS, 14-Pin DIP | 225-0005 | 1 |
| U53 | Integrated Circuit, CD4017B, 10-Output Counter/Divider, CMOS, 16-Pin DIP | 220-4017 | 1 |
| U54 | Integrated Circuit, CD4081B, Quad 2-Input AND Gate, CMOS, 14-Pin DIP | 225-0008 | 1 |
| U55 | Integrated Circuit, MC14584, Hex Schmitt Trigger, CMOS, 14-Pin DIP | 228-4584 | 1 |
| XU1 | Socket, 8-Pin DIP | 417-0804 | 1 |
| XU4 thru XU7 | Socket, 8-Pin DIP | 417-0804 | 4 |
| $\begin{aligned} & \text { XU10 thru } \\ & \text { XU12 } \end{aligned}$ | Socket, 8-Pin DIP | 417-0804 | 3 |
| XU15 thru XU18 | Socket, 8-Pin DIP | 417-0804 | 4 |
| XU21, XU22 | Socket, 8-Pin DIP | 417-0804 | 2 |
| XU23 | Socket, 16-Pin DIP | 417-1604 | 1 |
| XU24 thru <br> XU27 | Socket, 8-Pin DIP | 417-0804 | 4 |

TABLE 3-10. STEREO CIRCUIT BOARD ASSEMBLY - 917-0209
(Sheet 10 of 10)

| REF. DES. |  |  |  |
| :--- | :--- | :--- | :--- |
|  | DESCRIPTION | PART NO. | QTY. |
| XU28 | Socket, 16-Pin DIP | $417-1604$ |  |
| XU29 thru | Socket, 8-Pin DIP | $417-0804$ | 1 |
| XU31 |  |  | 3 |
| XU33 | Socket, 16-Pin DIP | $417-1604$ |  |
| XU34, XU35 | Socket, 14-Pin DIP | $417-1404$ | 1 |
| XU36 | Socket, 16-Pin DIP | $417-1604$ | 2 |
| XU37 | Socket, 14-Pin DIP | $417-1404$ | 1 |
| XU38, XU39 | Socket, 16-Pin DIP | $417-1604$ | 1 |
| XU40 thru | Socket, 14-Pin DIP | $417-1404$ | 2 |
| XU44 |  |  | 5 |
| XU45 thru | Socket, 6-Pin DIP | $417-0600$ | 4 |
| XU48 |  |  | $417-1404$ |
| XU49 | Socket, 14-Pin DIP | $417-1604$ | 1 |
| XU50 | Socket, 16-Pin DIP | $417-1404$ | 1 |
| XU51, XU52 | Socket, 14-Pin DIP | $417-1604$ | 2 |
| XU53 | Socket, 16-Pin DIP | $417-1404$ | 1 |
| XU54, XU55 | Socket, 14-Pin DIP | $407-0074$ | 2 |
| ---- | Socket/Spacer, LED | $343-6331$ | 1 |
| ---- | Switch Cap, Red | $517-0209$ | 1 |
| ---- | Blank, Stereo Circuit Board, AM1, AM5 |  | 1 |

TABLE 3-11. ECU HARNESS ASSEMBLY - 947-0153

| REF. DES. | DESCRIPTION | PART NO. | QTY. |
| :--- | :--- | :--- | :--- |
| P1 | Housing, SL-156, 3 Position | $417-0306$ |  |
| P1 | Plug, Ribbon Cable, 26-Pin Dual In-line | $418-2600$ | 1 |
| P2 | Plug, 40-Pin, Dual In-line | $417-0118$ | 1 |
| P2 | Housing, SL-156, 6 Position | $417-0606$ | 1 |
| P3 | Plug, Ribbon Cable, 26-Pin Dual In-line | $418-2600$ | 1 |
| P7 | Connector Housing, 6-Pin | $418-0670$ | 1 |
| P8 | Plug, 40-Pin, Dual In-line | $417-0118$ | 1 |
| P10 | Plug, Ribbon Cable, 26-Pin Dual In-line | $418-2600$ | 1 |
| P502 | Plug, Housing, 4-Pin | $418-0240$ | 1 |
| P801 | Plug, Ribbon Cable, 26-Pin Dual In-line | $418-2600$ | 1 |
| ---- | Pins, Connector | $417-0053$ | 1 |
|  |  |  | 10 |

## SECTION IV ECU ASSEMBLY DRAWINGS

## 4-1. INTRODUCTION.

4-2. This section provides assembly drawings, wiring diagrams, and schematic diagrams as listed below for the Broadcast Electronics ECU assembly.

| FIGURE | TITLE | NUMBER |
| :---: | :---: | :---: |
| 4-1 | SCHEMATIC DIAGRAM, ECU CONTROLLER CIRCUIT BOARD | SB917-0205 |
| 4-2 | ASSEMBLY DIAGRAM, ECU CONTROLLER CIRCUIT BOARD | AC917-0205 |
| 4-3 | COMPONENT LOCATOR, ECU CONTROLLER BOARD |  |
| 4-4 | SCHEMATIC DIAGRAM, ECU MOTHERBOARD | SB917-0301 |
| 4-5 | ASSEMBLY DIAGRAM, ECU MOTHERBOARD | AC917-0301 |
| 4-6 | SCHEMATIC DIAGRAM, EXCITER CIRCUIT BOARD | SB917-0300 |
| 4-7 | ASSEMBLY DIAGRAM, EXCITER CIRCUIT BOARD | AC917-0300 |
| 4-8 | COMPONENT LOCATOR, ECU EXCITER BOARD | ---------- |
| 4-9 | SCHEMATIC DIAGRAM, STEREO CIRCUIT BOARD | SD917-0209 |
| 4-10 | ASSEMBLY DIAGRAM, STEREO CIRCUIT BOARD | AC917-0209 |
| 4-11 | COMPONENT LOCATOR, ECU STEREO BOARD |  |
| 4-12 | SCHEMATIC DIAGRAM, ECU DISPLAY/CONTROL SWITCH CIRCUIT BOARDS | SB917-0306-001 |
| 4-13 | SCHEMATIC DIAGRAM, ECU METER SWITCH CIRCUIT BOARD | SB917-0306-005 |
| 4-14 | REFER TO PART I, SECTION VII FOR THE ECU DISPLAY CIRCUIT BOARD ASSEMBLY-002/-003/-004/-005 | AD917-0306-001/ |

/-006/-007/-009/-014







| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | C1 | C60 | B3 | C119 | B2 | D49 | B3 | Q31 | B1 |
| C2 | C1 | C61 | B3 | C120 | C3 | D50 | C1 | Q32 | B1 |
| C3 | C2 | C62 | B3 | C121 | B2 | DS1 | B3 | Q33 | B1 |
| C4 | C2 | C63 | B3 | C122 | B2 | DS2 | C3 | Q34 | B1 |
| C5 | C2 | C64 | B2 | C123 | B2 | DS3 | C3 | Q35 | C2 |
| C6 | C2 | C65 | B2 | C124 | B2 | E10 | B3 | Q36 | C1 |
| C7 | C2 | C66 | B2 | C125 | B2 | J1 | C2 | Q37 | C1 |
| C8 | C2 | C67 | B2 | C126 | B2 | J2 | B3 | Q38 | C2 |
| C9 | C2 | C68 | B2 | C127 | B2 | J3 | B3 | Q39 | C2 |
| C10 | C2 | C69 | B2 | C128 | B3 | J4 | B1 | Q40 | C1 |
| C11 | C2 | C70 | B2 | C129 | B2 | J5 | B1-B2 | Q41 | C1 |
| C12 | C2 | C71 | C2 | D1 | C1 | J6 | B1-B2 | Q42 | C2 |
| C13 | C2 | C72 | B2 | D2 | C1 | J7 | B1 | Q43 | C2 |
| C14 | C2 | C73 | B2 | D3 | C1 | J8 | C3 | Q44 | C2 |
| C15 | C3 | C74 | B2 | D4 | C1 | J9 | C3 | Q45 | C1-C2 |
| C16 | C2 | C75 | C1 | D5 | C1 | J10 | C3 | Q46 | C1 |
| C17 | C2 | C76 | C1 | D6 | C1 | J11 | B2 | Q47 | B1 |
| C18 | C3 | C77 | C2 | D7 | C2 | J12 | C2 | Q48 | C3 |
| C19 | C3 | C78 | C2 | D8 | C2 | P1 | C2 | Q49 | B2 |
| C20 | C3 | C79 | C2 | D9 | C2 | P2 | B3 | Q50 | C3 |
| C21 | C3 | C80 | C2 | D10 | C2 | P3 | B3 | Q51 | B1 |
| C22 | C2 | C81 | B1-C1 | D11 | C2 | P6 | B1 | Q52 | B2 |
| C23 | C3 | C82 | B1-C1 | D12 | C2 | P8 | C3 | Q53 | B3 |
| C24 | C2 | C83 | B2-C2 | D13 | C1 | P9 | C3 | Q54 | B3 |
| C25 | C3 | C84 | B2-C2 | D14 | C1 | P10 | C3 | Q55 | B2 |
| C26 | C3 | C85 | B2-C2 | D15 | C2 | P11 | B2 | Q56 | B2 |
| C27 | C3 | C86 | B1 | D16 | C2 | P12 | C2 | Q57 | B3 |
| C28 | C3 | C87 | B1 | D17 | C2 | P301 | C1 | Q58 | B3 |
| C29 | C3 | C88 | B3 | D18 | B1 | P302 | B1-C1 | R1 | C2 |
| C30 | C3 | C89 | B3 | D19 | A1 | Q1 | C1 | R2 | C3 |
| C31 | C3 | C90 | B3 | D20 | B1 | Q2 | C1 | R3 | C3 |
| C32 | C3 | C91 | B3 | D21 | A1 | Q3 | C1-C2 | R4 | C3 |
| C33 | C3 | C92 | B3 | D22 | B1 | Q4 | C1-C2 | R5 | C3 |
| C34 | B3 | C93 | A2 | D23 | B1-B2 | Q5 | C2 | R6 | C3 |
| C35 | C3 | C94 | B3 | D24 | B3 | Q6 | C2 | R7 | C3 |
| C36 | C3 | C95 | B3 | D25 | B1 | Q7 | C2 | R8 | C3 |
| C37 | B3 | C96 | B3 | D26 | B1 | Q8 | C1 | R9 | B3 |
| C38 | B3 | C97 | B3 | D27 | B1 | Q9 | C1 | R10 | C3 |
| C39 | B3 | C98 | B2 | D28 | B2 | Q10 | C1 | R11 | B3 |
| C40 | B2 | C99 | B2-B3 | D29 | B3 | Q11 | C1 | R12 | B3 |
| C41 | C2 | C100 | B2 | D30 | B2 | Q12 | C1 | R13 | B3 |
| C42 | B2 | C101 | B2-B3 | D31 | B2 | Q13 | B1 | R14 | B2 |
| C43 | B2 | C102 | B2 | D32 | C2 | Q14 | C2 | R15 | C3 |
| C44 | B2 | C103 | A2-B2 | D33 | B2 | Q15 | B1 | R16 | C3 |
| C45 | B2 | C104 | B3 | D34 | B2 | Q16 | C1 | R17 | C3 |
| C46 | B2 | C105 | B2 | D35 | B3 | Q17 | C2 | R18 | C3 |
| C47 | B1 | C106 | B1 | D36 | B3 | Q18 | C2 | R19 | C3 |
| C48 | B3 | C107 | B1 | D37 | A2 | Q19 | C1 | R20 | C3 |
| C49 | B3 | C108 | B2 | D38 | B3 | Q20 | C1-C2 | R21 | C3 |
| C50 | B1 | C109 | B2 | D39 | B3 | Q21 | B1 | R22 | C3 |
| C51 | C1 | C110 | B2 | D40 | B3 | Q22 | B1 | R23 | B3 |
| C52 | C1 | C111 | B2 | D41 | B2 | Q23 | C1 | R24 | B3 |
| C53 | B3 | C112 | B2 | D42 | B2 | Q24 | C2 | R25 | B3 |
| C54 | B3 | C113 | B2 | D43 | B2 | Q25 | B1 | R26 | B3-C3 |
| C55 | B2 | C114 | B2 | D44 | B3 | Q26 | B1 | R27 | B3 |
| C56 | B2 | C115 | A2 | D45 | B3 | Q27 | B1 | R28 | B3 |
| C57 | C2 | C116 | B2 | D46 | B2 | Q28 | B1 | R29 | B3 |
| C58 | B2 | C117 | B3 | D47 | C3 | Q29 | B1 | R30 | B3-C3 |
| C59 | B2 | C118 | B2 | D48 | B3 | Q30 | B1 | R31 | B3-C3 |


| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R32 | C3 | R91 | B2 | R150 | B3 | TP3 | B3 | U51 | B2 |
| R33 | C3 | R92 | B2 | R151 | B3 | TP4 | B3 | U52 | B2 |
| R34 | C3 | R93 | B2 | R152 | A3-B3 | TP5 | B3 | U53 | B1 |
| R35 | C3 | R94 | B2 | R153 | B3 | TP6 | B3 | U54 | B1 |
| R36 | C3 | R95 | B2 | R154 | B3 | TP7 | B1 | U55 | B2 |
| R37 | C1 | R96 | C2 | R155 | B3 | TP8 | C2 | U56 | B1-B2 |
| R38 | C1 | R97 | B2 | R156 | B3 | TP9 | C3 | U57 | B2 |
| R39 | B3 | R98 | B2 | R157 | B3 | TP10 | C3 | U58 | B1 |
| R40 | B3 | R99 | B2-B3 | R158 | B3 | TP11 | C3 | U59 | B2 |
| R41 | C1 | R100 | B2 | R159 | B2-B3 | U1 | C1 | U60 | B2 |
| R42 | B3 | R101 | B3 | R160 | C2 | U2 | C1 | U61 | B3 |
| R43 | B3 | R102 | B3 | R161 | B2 | U3 | C1-C2 | U62 | B2 |
| R44 | B3 | R103 | B2-B3 | R162 | C2 | U4 | C2 | U63 | B3 |
| R45 | B3 | R104 | C3 | R163 | B3 | U5 | C2 | U64 | B3 |
| R46 | B2 | R105 | B2-B3 | R164 | B3 | U6 | C2 | U65 | B2 |
| R47 | B3 | R106 | B3 | R165 | B3 | U7 | B1-C1 | U66 | B2 |
| R48 | B2 | R107 | B2 | R166 | B1 | U8 | B1-C1 | U67 | B2 |
| R49 | B3 | R108 | C3 | R167 | B1 | U9 | B2-C2 | U68 | B2 |
| R50 | B2 | R109 | B3 | R168 | B2 | U10 | B2-C2 | U69 | B2 |
| R51 | B3 | R110 | C1 | R169 | B2 | U11 | B2-C2 | U70 | C3 |
| R52 | B2-B3 | R111 | C1 | R170 | B2 | U12 | C2 | U71 | B3 |
| R53 | B2 | R112 | C2 | R171 | B2 | U13 | C2 |  |  |
| R54 | B2 | R113 | C2 | R172 | B3 | U14 | C1 |  |  |
| R55 | C3 | R114 | C2 | R173 | B2 | U15 | C1 |  |  |
| R56 | B3 | R115 | C2 | R174 | B2 | U16 | C2 |  |  |
| R57 | B3 | R116 | C1 | R175 | B2 | U17 | C2 |  |  |
| R58 | B3 | R117 | C1 | R176 | B2 | U18 | C2 |  |  |
| R59 | B3 | R118 | C2 | R177 | B2 | U19 | C2 |  |  |
| R60 | B3 | R119 | C2 | R178 | A2 | U20 | C2 |  |  |
| R61 | B3 | R120 | C2 | R179 | B2 | U21 | C2 |  |  |
| R62 | B2 | R121 | B1 | R180 | B2 | U22 | C3 |  |  |
| R63 | B3 | R122 | B1 | R181 | C2 | U23 | C2 |  |  |
| R64 | B3 | R123 | C3 | R182 | B2 | U24 | C2 |  |  |
| R65 | C3 | R124 | C3 | R183 | B3 | U25 | C2 |  |  |
| R66 | C3 | R125 | B2 | R184 | C3 | U26 | C2 |  |  |
| R67 | B3 | R126 | C1 | R185 | C3 | U27 | C2 |  |  |
| R68 | B2 | R127 | C1 | R186 | C3 | U28 | C2 |  |  |
| R69 | B2 | R128 | C1 | R187 | B3 | U29 | B2 |  |  |
| R70 | B3 | R129 | C1 | R188 | C1 | U30 | C3 |  |  |
| R71 | B3 | R130 | C1 | R189 | B2-B3 | U31 | C3 |  |  |
| R72 | B3 | R131 | B2 | R190 | B2 | U32 | B1 |  |  |
| R73 | B2 | R132 | B2 | R191 | B2 | U33 | B1 |  |  |
| R74 | B2 | R133 | B2 | R192 | B2 | U34 | C3 |  |  |
| R75 | B2 | R134 | B2 | R193 | B1 | U35 | C3 |  |  |
| R76 | B2 | R135 | B3 | RN1 | C1 | U36 | B2-C2 |  |  |
| R77 | B2 | R136 | B3 | RN2 | C2 | U37 | B2-C2 |  |  |
| R78 | B2 | R137 | B3 | RN3 | C2 | U38 | B3-C3 |  |  |
| R79 | C3 | R138 | B3 | RN4 | C2 | U39 | B3 |  |  |
| R80 | C3 | R139 | B2 | RN5 | B1 | U40 | B3-C3 |  |  |
| R81 | B2 | R140 | C2 | RN6 | A2 | U41 | B3 |  |  |
| R82 | B2 | R141 | B3 | RN7 | B2 | U42 | C3 |  |  |
| R83 | B2 | R142 | B3 | RN8 | B1 | U43 | C3 |  |  |
| R84 | B2 | R143 | B3 | S1 | C2 | U44 | B3 |  |  |
| R85 | C3 | R144 | B3 | S2 | C2 | U45 | B2 |  |  |
| R86 | B2 | R145 | B3 | S3 | C2 | U46 | B2-C2 |  |  |
| R87 | B2 | R146 | B3 | S4 | C3 | U47 | B2 |  |  |
| R88 | B2 | R147 | B3 | S5 | B3 | U48 | B2-C2 |  |  |
| R89 | B2 | R148 | B2 | TP1 | B3 | U49 | B2 |  |  |
| R90 | B2 | R149 | B2-B3 | TP2 | B3 | U50 | B2 |  |  |

FIGURE 4-3. COMPONENT LOCATOR, ECU CONTROLLER BOARD









| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | B3 | C62 | B2 | C121 | C2 | D23 | C2 | P12B | B3 |
| C2 | B3 | C63 | B4 | C122 | C2 | D24 | C3 | P13A | B3 |
| C3 | B3 | C64 | B3-B4 | C123 | C2 | D25 | C2 | P13B | B3 |
| C4 | B3 | C65 | B3 | C124 | C2 | D26 | C2 | P101 | B2-C2 |
| C5 | B3 | C66 | B3 | C125 | C2 | D27 | C2 | Q1 | B2 |
| C6 | B3 | C67 | B3 | C126 | C2 | D30 | C3 | Q2 | C4 |
| C7 | B3 | C68 | B2 | C127 | C3 | D31 | C3 | Q3 | C2 |
| C8 | B3 | C69 | A2-B2 | C128 | C3 | D32 | C3 | Q4 | C2 |
| C9 | B3 | C70 | B2 | C129 | C3 | D33 | C3 | Q5 | C3 |
| C10 | B3 | C71 | B2 | C130 | B3 | D34 | C3 | Q6 | C3 |
| C11 | B3 | C72 | B2 | C131 | C3 | D35 | C3 | Q7 | B3-C3 |
| C12 | B3 | C73 | B3-B4 | C132 | C3 | D36 | C3 | Q8 | B3 |
| C14 | B3 | C74 | B3-B4 | C133 | C3 | D37 | C3 | Q9 | B3-C3 |
| C15 | B3 | C75 | B3 | C134 | C3 | D38 | C2 | Q10 | C3 |
| C16 | B3 | C76 | B3 | C135 | C3 | D39 | B2 | Q11 | B3 |
| C17 | B3 | C77 | B3 | C136 | C3 | D40 | C2 | Q12 | B3 |
| C18 | B3 | C78 | B3 | C137 | B3 | D41 | B2 | Q13 | B2-C2 |
| C19 | B3 | C79 | B3 | C138 | B3 | D42 | C2 | Q14 | B2 |
| C20 | A3 | C80 | B3 | C139 | B3 | D43 | B2 | Q15 | B2-C2 |
| C21 | B3 | C81 | C3 | C140 | C2 | D44 | C2 | Q16 | B2 |
| C22 | B3 | C82 | B3 | C141 | C2 | D45 | B2 | Q17 | B2-C2 |
| C23 | B3 | C83 | B3 | C142 | C2 | DS1 | C4 | Q18 | B2 |
| C24 | B3 | C84 | B3-C3 | C143 | C3 | DS2 | C4 | Q19 | B2-C2 |
| C25 | B3 | C85 | B3 | C144 | C3 | DS3 | C4 | Q20 | B2 |
| C26 | B3 | C86 | B3 | C145 | C3 | DS4 | C4 | R1 | B3 |
| C27 | B3 | C87 | B3 | C146 | C3 | E1 | B3 | R2 | B3 |
| C29 | B3 | C88 | B2 | C147 | B2 | E2 | B3 | R3 | B3 |
| C30 | B3 | C89 | B2 | C148 | B2 | E3 | B3 | R4 | B3 |
| C31 | C2 | C90 | B3 | C149 | B2 | E4 | B3 | R5 | B3 |
| C32 | C2 | C91 | B2 | C150 | B2 | E5 | B2 | R8 | B3 |
| C33 | C2 | C92 | C2 | C151 | B2 | E6 | B2 | R9 | B3 |
| C34 | B2 | C93 | C2 | C152 | B2 | E7 | C2 | R10 | B3 |
| C35 | B2 | C94 | C2-C3 | C153 | B2 | E8 | B2 | R11 | B3 |
| C36 | B2 | C95 | C3 | C154 | B2 | E9 | B2 | R12 | B3 |
| C37 | B2 | C96 | C2 | C155 | C2 | E10 | B2 | R14 | B3 |
| C38 | B3 | C97 | C2 | C156 | C3 | J2 | B3 | R15 | B2 |
| C39 | B3 | C98 | C2 | C157 | C3 | J3 | B3 | R16 | B3 |
| C40 | B3 | C99 | C2 | D1 | B3 | J4 | B3 | R17 | B3 |
| C41 | A3 | C100 | C2 | D2 | B3 | J5 | C3 | R18 | B3 |
| C42 | B3 | C101 | C2 | D3 | C3 | J6 | C2 | R19 | B3 |
| C43 | B3 | C102 | C2 | D4 | B2 | J7 | C2 | R20 | B3 |
| C44 | B3-A3 | C103 | C2 | D5 | B2 | J8 | C2 | R23 | B3 |
| C45 | B3 | C104 | C2 | D6 | B2 | J9 | C2 | R24 | B3 |
| C46 | A3 | C105 | C2 | D7 | B2 | J10 | C2 | R25 | B3 |
| C47 | B3 | C106 | C2 | D8 | B2 | J11 | C2 | R26 | B3 |
| C48 | B3 | C107 | C3 | D9 | B2 | J12 | B3 | R27 | B3 |
| C49 | A3 | C108 | C3 | D10 | B2 | J13 | B3 | R29 | B3 |
| C50 | B3 | C109 | C3 | D11 | B2 | L1 | C2 | R30 | B2 |
| C51 | B3-B4 | C110 | C3 | D12 | B2 | L2 | B2 | R31 | C3-C4 |
| C52 | A3 | C111 | C3 | D13 | B2 | L3 | B2 | R32 | C3-C4 |
| C53 | B3 | C112 | C3 | D14 | B2 | L4 | C2 | R33 | C3-C4 |
| C54 | B2 | C113 | C3 | D15 | B2 | P2 | B3 | R34 | B3 |
| C55 | B2 | C114 | C3 | D16 | B2 | P3 | B3 | R35 | B3 |
| C56 | B2 | C115 | C3 | D17 | B2 | P4 | B3 | R36 | B3 |
| C57 | B2 | C116 | C3 | D18 | B2 | P5 | C3 | R37 | B3 |
| C58 | B2 | C117 | C3 | D19 | B2 | P6A | C2 | R38 | B3 |
| C59 | B2 | C118 | C2 | D20 | B2 | P6B | C2 | R39 | B3 |
| C60 | B2 | C119 | C3 | D21 | B2 | P7 | C2 | R40 | B3 |
| C61 | B2 | C120 | C2 | D22 | C2 | P12A | B3 | R41 | B4 |

FIGURE 4-8. COMPONENT LOCATOR, ECU EXCITER BOARD
(Sheet 1 of 2)

| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R42 | B3 | R101 | B3 | R160 | C3 | U7 | B3 |  |  |
| R43 | B3 | R102 | B3-B4 | R161 | C3 | U8 | B3 |  |  |
| R44 | B3 | R103 | B3 | R162 | B3 | U9 | B3 |  |  |
| R45 | B3 | R104 | B4 | R163 | C3 | U10 | B2 |  |  |
| R46 | A3 | R105 | C3-C4 | R164 | C3 | U11 | B2 |  |  |
| R47 | A3 | R106 | C3-C4 | R165 | C3 | U12 | B2 |  |  |
| R48 | B3 | R107 | C3 | R166 | B3 | U13 | B4 |  |  |
| R49 | B3 | R108 | C3-B3 | R167 | B3 | U14 | B3 |  |  |
| R50 | B3 | R109 | C3-B3 | R168 | B3 | U15 | B3 |  |  |
| R51 | B3 | R110 | C3-B3 | R169 | C4 | U16 | B3 |  |  |
| R52 | C3 | R111 | C3-B3 | R170 | C4 | U17 | B3-C3 |  |  |
| R53 | C3 | R112 | B2 | R171 | C3-C4 | U18 | B3-C3 |  |  |
| R54 | C3 | R113 | B2 | R172 | B2-C2 | U19 | B2 |  |  |
| R55 | B2 | R114 | B2 | R173 | B2 | U20 | B2 |  |  |
| R56 | B2 | R115 | B2 | R174 | B2-C2 | U21 | B2 |  |  |
| R57 | B2 | R116 | B2 | R175 | B2 | U22 | B2 |  |  |
| R58 | B2 | R117 | B2 | R176 | B2-C2 | U23 | B2 |  |  |
| R59 | B2 | R118 | B2 | R177 | B2 | U24 | C2 |  |  |
| R60 | B2 | R119 | C2 | R178 | B2-C2 | U25 | C3 |  |  |
| R61 | B2 | R120 | C2 | R179 | B2 | U26 | C2 |  |  |
| R62 | B2 | R121 | C2-C3 | R180 | C3 | U27 | C3 |  |  |
| R63 | B2 | R122 | C2 | R181 | B4 | U28 | C3 |  |  |
| R64 | B2 | R123 | C2 | R182 | C3 | U29 | C2 |  |  |
| R65 | B2 | R124 | C2 | R183 | C3 | U30 | C2 |  |  |
| R66 | B2 | R125 | C2 | R184 | C3 | U31 | C2 |  |  |
| R67 | A2-B2 | R126 | C2 | R185 | B2 | U32 | C2 |  |  |
| R68 | B2 | R127 | C2 | R186 | C3 | U33 | C3 |  |  |
| R69 | B2 | R128 | C2 | R187 | C3 | U34 | C3 |  |  |
| R70 | B4 | R129 | C2 | R188 | C3 | U35 | C3 |  |  |
| R71 | B4 | R130 | C2 | R189 | B4 | U36 | C3 |  |  |
| R72 | B3 | R131 | C2 | R190 | B3 | U37 | C3 |  |  |
| R73 | B3 | R132 | C2 | R191 | B4 | U38 | B3-C3 |  |  |
| R74 | B3 | R133 | C3 | R192 | B3 | U39 | C3 |  |  |
| R75 | B4 | R134 | C3 | R193 | B2 | U40 | B3-C3 |  |  |
| R76 | B4-A4 | R135 | C3 | R194 | B3 | U41 | C3 |  |  |
| R77 | A3-A4 | R136 | C3 | S1 | B2 | U42 | C2 |  |  |
| R78 | B3 | R137 | C3 | S2 | C3 | Y1 | C3 |  |  |
| R79 | B3 | R138 | C3 | T1 | B2 |  |  |  |  |
| R80 | B3 | R139 | C3 | TP1 | C3 |  |  |  |  |
| R81 | B2 | R140 | C3 | TP2 | C3 |  |  |  |  |
| R82 | A2 | R141 | C3 | TP3 | C3 |  |  |  |  |
| R83 | B2 | R142 | C3 | TP4 | C3 |  |  |  |  |
| R84 | B2 | R143 | C3-C4 | TP5 | B2 |  |  |  |  |
| R85 | B2 | R144 | C2 | TP6 | B2 |  |  |  |  |
| R86 | B3 | R145 | C2 | TP7 | C2 |  |  |  |  |
| R87 | B3 | R146 | C2 | TP8 | C2 |  |  |  |  |
| R88 | B3 | R147 | C2 | TP9 | C3 |  |  |  |  |
| R89 | B3 | R148 | C2 | TP10 | C3 |  |  |  |  |
| R90 | B3 | R149 | C2 | TP11 | B2 |  |  |  |  |
| R91 | B3 | R150 | C2 | TP12 | B3 |  |  |  |  |
| R92 | B3 | R151 | C2 | TP13 | B4 |  |  |  |  |
| R93 | B3 | R152 | C2 | TP14 | C3 |  |  |  |  |
| R94 | B2 | R153 | C2 | TP15 | C3 |  |  |  |  |
| R95 | C3 | R154 | C2 | U1 | B3 |  |  |  |  |
| R96 | C3 | R155 | C2 | U2 | B3 |  |  |  |  |
| R97 | C3 | R156 | C3 | U3 | B3 |  |  |  |  |
| R98 | B3 | R157 | C3 | U4 | B3 |  |  |  |  |
| R99 | B3 | R158 | C3 | U5 | B3 |  |  |  |  |
| R100 | B3 | R159 | C3 | U6 | B3 |  |  |  |  |

FIGURE 4-8. COMPONENT LOCATOR, ECU EXCITER BOARD
(Sheet 2 of 2)

ELECTRONICS INC


LeFT Hise freauency Eavelizer $\qquad$
$\qquad$ Bus broup delay $\qquad$ 1 4uS group pelay $\qquad$ $\downarrow$ - - GuS Fine delay


$\qquad$ L_ sus sroup delay $1\llcorner$ $\qquad$ L - bus fine delay

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|  | $\begin{aligned} & \text { MATEAIFL } \\ & \text { SEE B/M } \\ & \text { 917-D209 } \end{aligned}$ |  |  |  |
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| matis |  | monam- | $\left.\right\|_{\text {sane }}$ note |  |







| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | C2 | C60 | B3 | C119 | B1 | D3 | B2 | R3 | C2 |
| C2 | C2 | C61 | B3 | C120 | B1 | D4 | B2 | R4 | C2 |
| C3 | C2 | C62 | B3 | C121 | B1 | D5 | C2 | R5 | C2 |
| C4 | C3 | C63 | B3 | C122 | B1 | D6 | C1 | R6 | C3 |
| C5 | C3 | C64 | B2 | C123 | B1 | D7 | C1 | R7 | C2 |
| C6 | C3 | C65 | B2 | C124 | B2 | D8 | C1 | R8 | C2 |
| C7 | C3 | C66 | C2 | C125 | B1 | D9 | C1 | R9 | C2 |
| C8 | C3 | C67 | C2 | C126 | B2 | DS1 | C3 | R10 | C3 |
| C9 | C3 | C68 | C2 | C127 | B2 | DS2 | B3 | R11 | C3 |
| C10 | C3 | C69 | C2 | C128 | C2 | DS3 | C3 | R12 | C2 |
| C11 | C3 | C70 | C2 | C129 | C1-C2 | DS4 | C3 | R13 | C2 |
| C12 | C3 | C71 | B2 | C130 | C2 | DS5 | C3 | R14 | C3 |
| C13 | C3 | C72 | B2 | C131 | C2 | DS6 | C3 | R15 | C3 |
| C14 | C3 | C73 | B2 | C132 | B1 | E1 | C1 | R16 | C3 |
| C15 | C3 | C74 | B2 | C133 | C1 | E2 | C1 | R17 | C3 |
| C16 | C3 | C75 | B2 | C134 | C1 | E3 | C1 | R18 | C3 |
| C17 | C2 | C76 | B2 | C135 | C1 | E4 | C1 | R19 | C3 |
| C18 | B2 | C77 | B2 | C136 | B1-C1 | J1 | C3 | R20 | C3 |
| C19 | B2 | C78 | B2 | C137 | C1 | J2 | B3 | R21 | C3 |
| C20 | C3 | C79 | C2 | C138 | C1 | J3 | B3 | R22 | C3 |
| C21 | B3 | C80 | B2 | C139 | C2 | J4 | B3 | R23 | C3 |
| C22 | B3 | C81 | B2 | C140 | C2 | J5 | B2 | R24 | C3 |
| C23 | B3 | C82 | B2 | C141 | C2 | J6 | C2 | R25 | C3 |
| C24 | B2 | C83 | C2-D2 | C142 | C2 | J7 | C2 | R26 | C3 |
| C25 | C3 | C84 | C2-D2 | C143 | C2 | L1 | C1 | R27 | C3 |
| C26 | C3 | C85 | C3 | C144 | C2 | L2 | C1 | R28 | C2 |
| C27 | C3 | C86 | C3-D3 | C145 | C2 | L3 | C1 | R29 | C2 |
| C28 | C3 | C87 | C3-D3 | C146 | C2 | L4 | B2 | R30 | C2 |
| C29 | B3 | C88 | D3 | C147 | C2 | L5 | B2 | R31 | C2 |
| C30 | B3 | C89 | C2 | C148 | C2 | L6 | B2 | R32 | C3-B3 |
| C31 | C3 | C90 | C2 | C149 | C2 | L7 | B2 | R33 | C2 |
| C32 | C2 | C91 | C2 | C150 | C2 | P1A | C3 | R34 | C2 |
| C33 | B2 | C92 | C1 | C151 | C2 | P1B | C3 | R35 | C2 |
| C34 | B2 | C93 | C1 | C152 | C2 | P2A | B3 | R36 | C3 |
| C35 | B2 | C94 | C1 | C153 | C2 | P2B | B3 | R37 | C3 |
| C36 | B3 | C95 | C1 | C154 | C2 | P3A | B3 | R38 | C2 |
| C37 | B3 | C96 | B2 | C155 | C2 | P3B | B3 | R39 | C2 |
| C38 | B3 | C97 | B2 | C156 | C3 | P4A | B3 | R40 | C3 |
| C39 | B3 | C98 | B2 | C157 | C2 | P4B | B3 | R41 | C3 |
| C40 | B3 | C99 | B2 | C158 | C2 | P5 | B2 | R42 | C3 |
| C41 | B3 | C100 | B2 | C159 | C2 | P6 | C2 | R43 | B3-C3 |
| C42 | B3 | C101 | B2 | C160 | C2-C3 | P7 | C2 | R44 | B3 |
| C43 | B3 | C102 | B2 | C161 | D1 | P201 | C1-D1 | R45 | B3 |
| C44 | B3 | C103 | B2 | C162 | D1 | Q1 | B1 | R46 | C3 |
| C45 | B3 | C104 | B2 | C163 | D1-D2 | Q2 | B2 | R47 | C3 |
| C46 | B3 | C105 | B2 | C164 | D2 | Q3 | B3 | R48 | C3 |
| C47 | B3 | C106 | B2 | C165 | C2 | Q4 | C3 | R49 | B3 |
| C48 | B3 | C107 | B2 | C166 | C2 | Q5 | C3 | R50 | B3 |
| C49 | B2 | C108 | B1 | C167 | C2 | Q6 | C3 | R51 | B3 |
| C50 | B2 | C109 | B1 | C168 | C2 | Q7 | C3 | R52 | B3 |
| C51 | B2 | C110 | B1 | C169 | B2 | Q8 | C3 | R53 | B3 |
| C52 | B3 | C111 | B1 | C170 | B2 | Q9 | D1 | R54 | B2 |
| C53 | B3 | C112 | B1 | C171 | B1 | Q10 | D1 | R55 | B2 |
| C54 | B3 | C113 | B1 | C172 | B1 | Q11 | D1-D2 | R56 | B2 |
| C55 | B3 | C114 | B1 | C173 | B1 | Q12 | D2 | R57 | B2 |
| C56 | B2 | C115 | B1 | C174 | B2 | Q13 | D1 | R58 | B3 |
| C57 | B3 | C116 | B1 | C175 | B1 | Q14 | D1 | R59 | B2 |
| C58 | B3 | C117 | B1 | D1 | B2 | R1 | C3 | R60 | B2 |
| C59 | B3 | C118 | B1 | D2 | B2 | R2 | C2 | R61 | B2 |

FIGURE 4-11. COMPONENT LOCATOR, ECU STEREO BOARD
(Sheet 1 of 2)

| REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE | REF | ZONE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R62 | B3 | R121 | B2 | R180 | B2-C2 | TP5 | B2 | U54 | C2 |
| R63 | B3 | R122 | B2 | R181 | B2-C2 | TP6 | C1 | U55 | C2 |
| R64 | B2 | R123 | B2 | R182 | B2-C2 | TP7 | B2 |  |  |
| R65 | B2 | R124 | B2 | R183 | C2 | TP8 | B2 |  |  |
| R66 | B3 | R125 | B2 | R184 | C2 | TP9 | B2 |  |  |
| R67 | B3 | R126 | B2 | R185 | C2 | TP10 | B2 |  |  |
| R68 | B3 | R127 | B2 | R186 | C1 | U1 | C2 |  |  |
| R69 | B3 | R128 | B2 | R187 | C2 | U2 | C2-C3 |  |  |
| R70 | B3 | R129 | B2 | R188 | C1 | U3 | C2-C3 |  |  |
| R71 | B3 | R130 | B2 | R189 | C1 | U4 | C3 |  |  |
| R72 | B3 | R131 | B2 | R190 | B1 | U5 | C3 |  |  |
| R73 | B3 | R132 | D3 | R191 | C1 | U6 | C2-C3 |  |  |
| R74 | B3 | R133 | C3-D3 | R192 | C3 | U7 | B2-C2 |  |  |
| R75 | B3 | R134 | D3 | R193 | C3 | U8 | B2-B3 |  |  |
| R76 | B3 | R135 | D2 | R194 | C3 | U9 | C2-C3 |  |  |
| R77 | B3 | R136 | C2 | R195 | C1 | U10 | B3-C3 |  |  |
| R78 | B3 | R137 | D3 | R196 | C1 | U11 | B3-C3 |  |  |
| R79 | B3 | R138 | D3 | R197 | C2 | U12 | B2 |  |  |
| R80 | B2 | R139 | C3 | R198 | C2 | U13 | B2-B3 |  |  |
| R81 | B2 | R140 | C2 | R199 | C2 | U14 | B2-B3 |  |  |
| R82 | B2 | R141 | C2 | R200 | C2 | U15 | B3 |  |  |
| R83 | B2 | R142 | B2 | R201 | B3 | U16 | B3 |  |  |
| R84 | B3 | R143 | C2-B2 | R202 | C3 | U17 | B2-B3 |  |  |
| R85 | B2 | R144 | B2 | R203 | C2 | U18 | B2 |  |  |
| R86 | B2 | R145 | C2 | R204 | C2 | U19 | B2-B3 |  |  |
| R87 | B2 | R146 | C1 | R205 | C2 | U20 | B2-B3 |  |  |
| R88 | B3 | R147 | C1 | R206 | C2 | U21 | B3 |  |  |
| R89 | B2-B3 | R148 | B2 | R207 | C2 | U22 | B3 |  |  |
| R90 | B2 | R149 | B2 | R208 | C2 | U23 | C2 |  |  |
| R91 | B2 | R150 | B2 | R209 | C2 | U24 | C2 |  |  |
| R92 | B3 | R151 | B2 | R210 | C2 | U25 | C2 |  |  |
| R93 | B3 | R152 | B2 | R211 | C2 | U26 | B2 |  |  |
| R94 | B3 | R153 | B2 | R212 | C2 | U27 | B2 |  |  |
| R95 | B3 | R154 | B2 | R213 | C2 | U28 | B2 |  |  |
| R96 | B3 | R155 | B2 | R214 | C2 | U29 | B2 |  |  |
| R97 | B3 | R156 | B2 | R215 | C2 | U30 | C3-D3 |  |  |
| R98 | B3 | R157 | B2 | R216 | C3 | U31 | C2 |  |  |
| R99 | B3 | R158 | B2 | R217 | C3 | U32 | B2 |  |  |
| R100 | B3 | R159 | B2 | R218 | C3 | U33 | B2 |  |  |
| R101 | B3 | R160 | B2 | R219 | C3 | U34 | B2 |  |  |
| R102 | B3 | R161 | B2 | R220 | C3 | U35 | B2 |  |  |
| R103 | B3 | R162 | B2 | R221 | C3 | U36 | B2 |  |  |
| R104 | B3 | R163 | B1 | R222 | D1 | U37 | B2 |  |  |
| R105 | C2 | R164 | B1 | R223 | D1 | U38 | B1 |  |  |
| R106 | B2 | R165 | B1 | R224 | D2 | U39 | C1-C2 |  |  |
| R107 | C2 | R166 | B1 | R225 | D2 | U40 | C1 |  |  |
| R108 | C2 | R167 | B1 | R226 | B1 | U41 | C2 |  |  |
| R109 | B2 | R168 | B1 | R227 | B1 | U42 | C2 |  |  |
| R110 | C2 | R169 | B1 | R228 | C2 | U43 | C2 |  |  |
| R111 | B2 | R170 | B1 | S1 | C3-D3 | U44 | C2 |  |  |
| R112 | C2 | R171 | B1 | S2 | B1 | U45 | C1-C2 |  |  |
| R113 | B2 | R172 | B1 | S3 | B1 | U46 | C1-C2 |  |  |
| R114 | B2 | R173 | B1 | S4 | B1 | U47 | C1-C2 |  |  |
| R115 | B2 | R174 | B1-C1 | S5 | C3 | U48 | C1-C2 |  |  |
| R116 | B2 | R175 | B2 | T1 | C1 | U49 | C2 |  |  |
| R117 | C2-B2 | R176 | B2-C2 | TP1 | C1 | U50 | C2 |  |  |
| R118 | B2 | R177 | B1-C1 | TP2 | C1 | U51 | C2 |  |  |
| R119 | B2 | R178 | B2-C2 | TP3 | B2 | U52 | C2 |  |  |
| R120 | B2 | R179 | B2-C2 | TP4 | B2 | U53 | C2 |  |  |

FIGURE 4-11. COMPONENT LOCATOR, ECU STEREO BOARD
(Sheet 2 of 2)
broadcast
electronics inc





